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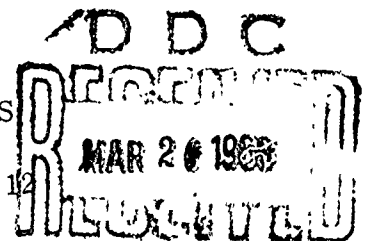
UNIVERSITY OF MARYLAND
WIND TUNNEL REPORT NO. 485

EFFECTS OF STREAMWISE GAPS, HULL
FLOW AND PROPELLER SLIPSTREAM UPON
THE AERODYNAMIC CHARACTERISTICS OF
A FAMILY OF LOW-ASPECT RATIO,
ALL-MOVEABLE CONTROL SURFACES

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ABSTRACT

Effects of faired, streamwise gaps upon the free stream characteristics of a family of low-aspect-ratio, all-moveable control surfaces are presented. The family of control surfaces consisted of three aspect ratios (1, 2, and 3) and three sweep angles (0, 11, and 22.5 degrees), each having a NACA 0015 airfoil section and a taper ratio of 0.45. Gap effects were also investigated in conjunction with simulated hull effects. Propeller slipstream effects were determined for the minimum gap condition.

TABLE OF CONTENTS

	Page
INTRODUCTION	1
DESCRIPTION OF MODELS	1
TEST PROCEDURE	2
PRESENTATION OF DATA	3
DISCUSSION OF RESULTS	4
Free Stream Gap Effects	4
Free Stream Gap Effects Upon Lift	5
Free Stream Gap Effects Upon Drag	6
Free Stream Gap Effects Upon Chordwise Center of Pressure Location	6
Free Stream Gap Effects Upon Spanwise Center of Pressure Location	7
Summary of Free Stream Gap Effects	8
Gap Effects With Simulated Hull	8
Simulated Hull Flow and Propeller Slipstream Effects	9
CONCLUSIONS AND RECOMMENDATIONS	12
ACKNOWLEDGEMENTS	13
REFERENCES	14
TABLE	15
FIGURES	16

APPENDIX A	Free Stream Characteristics for Various Gap Sizes	101
APPENDIX B	Simulated Hull Flow Characteristics for Various Gap Sizes	185
APPENDIX C	Combined Simulated Hull Flow and Propeller Slipstream Characteristics, Minimum Gap	255

INDEX OF FIGURES

Fig. No.	Title	Page
1	Basic Dimensions, AR = 1, $\Lambda = 0^\circ$	16
2	Basic Dimensions, AR = 1, $\Lambda = 11^\circ$	17
3	Basic Dimensions, AR = 1, $\Lambda = 22.5^\circ$	18
4	Basic Dimensions, AR = 2, $\Lambda = 0^\circ$	19
5	Basic Dimensions, AR = 2, $\Lambda = 11^\circ$	20
6	Basic Dimensions, AR = 2, $\Lambda = 22.5^\circ$	21
7	Basic Dimensions, AR = 3, $\Lambda = 0^\circ$	22
8	Basic Dimensions, AR = 3, $\Lambda = 11^\circ$	23
9	Basic Dimensions, AR = 3, $\Lambda = 22.5^\circ$	24
10	Fairing Details, AR = 1, $\Lambda = 0^\circ$	25
11	Fairing Details, AR = 2, $\Lambda = 22.5^\circ$	26
12	Aspect Ratio 1, $\Lambda = 11^\circ$, Control Surface Mounted on Tunnel Floor With Minimum Gap	27
13	Aspect Ratio 1, $\Lambda = 22.5^\circ$, Control Surface With 4.5 in. Gap, $\alpha = 35^\circ$	27
14	Aspect Ratio 2, $\Lambda = 0^\circ$, Control Surface With 12.0 in. Gap, $\alpha = 0^\circ$	28
15	Aspect Ratio 2, $\Lambda = 11^\circ$, Control Surface With 4.5 in. Gap, $\alpha = 30^\circ$	28
16	Turning Vanes and Screen Installed at Leading Edge of Test Section to Simulate Hull Flow Conditions	29
17	Propeller and Drive Motor Installed With Turning Vanes and Screen	29
18	Free Stream Faired Gap Effects on Lift Coefficient, Aspect Ratio 1, $\Lambda = 0^\circ$	30
19	Free Stream Faired Gap Effects on Lift Coefficient, Aspect Ratio 1, $\Lambda = 11^\circ$	31
20	Free Stream Faired Gap Effects on Lift Coefficient, Aspect Ratio 1, $\Lambda = 22.5^\circ$	32
21	Free Stream Faired Gap Effects on Lift Coefficient, Aspect Ratio 2, $\Lambda = 0^\circ$	33
22	Free Stream Faired Gap Effects on Lift Coefficient, Aspect Ratio 2, $\Lambda = 11^\circ$	34
23	Free Stream Faired Gap Effects on Lift Coefficient, Aspect Ratio 2, $\Lambda = 22.5^\circ$	35
24	Free Stream Faired Gap Effects on Lift Coefficient, Aspect Ratio 3, $\Lambda = 0^\circ$	36
25	Free Stream Faired Gap Effects on Lift Coefficient, Aspect Ratio 3, $\Lambda = 11^\circ$	37
26	Free Stream Faired Gap Effects on Lift Coefficient, Aspect Ratio 3, $\Lambda = 22.5^\circ$	38

INDEX OF FIGURES (continued)

Fig. No.	Title	Page
27	Free Stream, Faired Gap Effects on Drag Coefficient, Aspect Ratio 1, $\Lambda = 0^\circ$	39
28	Free Stream, Faired Gap Effects on Drag Coefficient, Aspect Ratio 1, $\Lambda = 11^\circ$	40
29	Free Stream, Faired Gap Effects on Drag Coefficient, Aspect Ratio 1, $\Lambda = 22.5^\circ$	41
30	Free Stream, Faired Gap Effects on Drag Coefficient, Aspect Ratio 2, $\Lambda = 0^\circ$	42
31	Free Stream, Faired Gap Effects on Drag Coefficient, Aspect Ratio 2, $\Lambda = 11^\circ$	43
32	Free Stream, Faired Gap Effects on Drag Coefficient, Aspect Ratio 2, $\Lambda = 22.5^\circ$	44
33	Free Stream, Faired Gap Effects on Drag Coefficient, Aspect Ratio 3, $\Lambda = 0^\circ$	45
34	Free Stream, Faired Gap Effects on Drag Coefficient, Aspect Ratio 3, $\Lambda = 11^\circ$	46
35	Free Stream, Faired Gap Effects on Drag Coefficient, Aspect Ratio 3, $\Lambda = 22.5^\circ$	47
36	Free Stream, Faired Gap Effects on Chordwise Center of Pressure, Aspect Ratio 1, $\Lambda = 0^\circ$	48
37	Free Stream, Faired Gap Effects on Chordwise Center of Pressure, Aspect Ratio 1, $\Lambda = 11^\circ$	49
38	Free Stream, Faired Gap Effects on Chordwise Center of Pressure, Aspect Ratio 1, $\Lambda = 22.5^\circ$	50
39	Free Stream, Faired Gap Effects on Chordwise Center of Pressure, Aspect Ratio 2, $\Lambda = 0^\circ$	51
40	Free Stream, Faired Gap Effects on Chordwise Center of Pressure, Aspect Ratio 2, $\Lambda = 11^\circ$	52
41	Free Stream, Faired Gap Effects on Chordwise Center of Pressure, Aspect Ratio 2, $\Lambda = 22.5^\circ$	53
42	Free Stream, Faired Gap Effects on Chordwise Center of Pressure, Aspect Ratio 3, $\Lambda = 0^\circ$	54
43	Free Stream, Faired Gap Effects on Chordwise Center of Pressure, Aspect Ratio 3, $\Lambda = 11^\circ$	55
44	Free Stream, Faired Gap Effects on Chordwise Center of Pressure, Aspect Ratio 3, $\Lambda = 22.5^\circ$	56
45	Free Stream, Faired Gap Effects on Spanwise Center of Pressure, Aspect Ratio 1, $\Lambda = 0^\circ$	57
46	Free Stream, Faired Gap Effects on Spanwise Center of Pressure, Aspect Ratio 1, $\Lambda = 11^\circ$	58
47	Free Stream, Faired Gap Effects on Spanwise Center of Pressure, Aspect Ratio 1, $\Lambda = 22.5^\circ$	59

INDEX OF FIGURES (continued)

Fig. No.	Title	Page
48	Free Stream, Faired Gap Effects of Spanwise Center of Pressure, Aspect Ratio 3, $\Lambda = 0^\circ$	60
49	Free Stream, Faired Gap Effects of Spanwise Center of Pressure, Aspect Ratio 3, $\Lambda = 11^\circ$	61
50	Free Stream, Faired Gap Effects of Spanwise Center of Pressure, Aspect Ratio 3, $\Lambda = 22.5^\circ$	62
51	Wake Velocity Diagram From Figure 11 of Reference 6	63
52	Wake Velocity Diagram For Simulated Hull Flow	64
53	Faired Gap Effects on Lift Coefficient For Simulated Hull Flow, Aspect Ratio 2, $\Lambda = 0^\circ$	65
54	Faired Gap Effects on Drag Coefficient For Simulated Hull Flow, Aspect Ratio 2, $\Lambda = 0^\circ$	66
55	Faired Gap Effects on Chordwise Center of Pressure For Simulated Hull Flow, Aspect Ratio 2 $\Lambda = 0^\circ$	67
56	Faired Gap Effects on Spanwise Center of Pressure For Simulated Hull Flow, Aspect Ratio 2, $\Lambda = 0^\circ$	68
57	Velocity Field at Rudder Leading Edge, From Figure 5 of Reference 7	69
58	Propeller Slipstream Velocity Survey at Rudder Leading Edge, Aspect Ratio 1	70
59	Propeller Slipstream Velocity Survey at Rudder Leading Edge, Aspect Ratio 2	71
60	Propeller Slipstream Velocity Survey at Rudder Leading Edge, Aspect Ratio 3	72
61	Comparison of Lift Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions Aspect Ratio 1, $\Lambda = 0^\circ$	73
62	Comparison of Lift Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions Aspect Ratio 1, $\Lambda = 11^\circ$	74
63	Comparison of Lift Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions Aspect Ratio 1, $\Lambda = 22.5^\circ$	75
64	Comparison of Lift Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions Aspect Ratio 2, $\Lambda = 0^\circ$	76
65	Comparison of Lift Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions Aspect Ratio 2, $\Lambda = 11^\circ$	77
66	Comparison of Lift Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions Aspect Ratio 2, $\Lambda = 22.5^\circ$	78

INDEX OF FIGURES (continued)

Fig. No.	Title	Page
67	Comparison of Lift Coefficients For free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 3, $\Lambda = 0^\circ$	79
68	Comparison of Lift Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 3, $\Lambda = 11^\circ$	80
69	Comparison of Lift Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 3, $\Lambda = 22.5^\circ$	81
70	Comparison of Drag Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 1, $\Lambda = 0^\circ$	82
71	Comparison of Drag Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 1, $\Lambda = 11^\circ$	83
72	Comparison of Drag Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 1, $\Lambda = 22.5^\circ$	84
73	Comparison of Drag Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 2, $\Lambda = 0^\circ$	85
74	Comparison of Drag Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 2, $\Lambda = 11^\circ$	86
75	Comparison of Drag Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 2, $\Lambda = 22.5^\circ$	87
76	Comparison of Drag Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 3, $\Lambda = 0^\circ$	88
77	Comparison of Drag Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 3, $\Lambda = 11^\circ$	89
78	Comparison of Drag Coefficients For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 3, $\Lambda = 22.5^\circ$	90
79	Comparison of Center of Pressure For Free Stream, Simulated Hull Flow and Propeller Slipstream Con- ditions, Aspect Ratio 1, $\Lambda = 0^\circ$	91
80	Comparison of Center of Pressure For Free Stream, Simulated Hull Flow and Propeller Slipstream Con- ditions, Aspect Ratio 1, $\Lambda = 11^\circ$	92

INDEX OF FIGURES (continued)

Fig. No.	Title	Page
81	Comparison of Center of Pressure For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 1, $\Lambda = 22.5^\circ$	93
82	Comparison of Center of Pressure For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 2, $\Lambda = 0^\circ$	94
83	Comparison of Center of Pressure For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 2, $\Lambda = 11^\circ$	95
84	Comparison of Center of Pressure For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 2, $\Lambda = 22.5^\circ$	96
85	Comparison of Center of Pressure For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 3, $\Lambda = 0^\circ$	97
86	Comparison of Center of Pressure For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 3, $\Lambda = 11^\circ$	98
87	Comparison of Center of Pressure For Free Stream, Simulated Hull Flow and Propeller Slipstream Conditions, Aspect Ratio 3, $\Lambda = 22.5^\circ$	99

NOTATION

AR	Effective aspect ratio, two times geometric aspect ratio, $2\frac{b^2}{S}$
b	Control surface span, feet
c	Chord, measured parallel to plane of root section, feet
\bar{c}	Mean geometric chord, $\frac{c_t + c_r}{2}$, feet
C_D	Drag coefficient, $\frac{D}{qS}$
C_L	Lift coefficient, $\frac{L}{qS}$
C_L	Rolling moment coefficient, $\frac{\mathcal{L}}{qSb}$
C_m	Pitching moment coefficient about the quarter chord point of the mean geometric chord, $\frac{M}{qS\bar{c}}$
C_n	Yawing moment coefficient, $\frac{N}{qS\bar{c}}$
$(CP)_{\bar{c}}$	Chordwise center of pressure measured from leading edge at mean geometric chord in per cent of the mean geometric chord,

$$(CP)_{\bar{c}} = 0.25 - \frac{C_m}{C_L \cos \alpha + C_D \sin \alpha}$$

$(CP)_s$	Spanwise center of pressure measured from plane of root section in per cent of control surface span,
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$$(CP)_s = \frac{C_L \cos \alpha - C_n \sin \alpha}{C_L \cos \alpha + C_D \sin \alpha}$$

D	Drag force, pounds
L	Lift force, pounds
\mathcal{L}	Rolling moment, foot pounds

M	Pitching moment, foot pounds
N	Yawing moment, foot pounds
q	Dynamic pressure, $1/2 \rho V^2$, pounds per square foot
RN	Reynolds number, $\frac{\rho V \bar{c}}{\mu}$
s	Gap width, inches
S	Control surface area, $\bar{c}b$, square feet
V	Free stream velocity, feet per second
V_t	Tangential component of velocity measured in the plane of the propeller, feet per second
V_r	Radial component of velocity measured in the plane of the propeller, feet per second
V_{tr}	Transverse component of velocity, vector sum of V_t and V_r , feet per second
V_x	Velocity component in streamwise direction, feet per second
α	Angle of attack, degrees
λ	Taper ratio, c_t/c_r
Λ	Sweepback angle of quarter-chord line, degrees
μ	Coefficient of viscosity of air, pound second per square foot
ρ	Mass density of air, slugs per cubic foot

SUBSCRIPTS

r	Root
t	Tip

INTRODUCTION

Considerable information on the free stream characteristics of low-aspect-ratio control surfaces is available from various wind tunnel tests (Reference 1). The most comprehensive of these tests are those reported in Reference 2. While the information obtained from the wind tunnel tests is quite valuable to the control surface designer, it is not usually directly applicable to the design problem. The tunnel tests are usually conducted in a uniform flow field with minimum clearance between the root chord of the control surface and the tunnel boundary. Whereas, an actual control surface normally operates with an appreciable gap between the root chord and the ship hull in a stream that may be disturbed by the hull effects and propeller slipstream.

In recognition of the need for additional information on gap, hull and propeller slipstream effects, a three part wind tunnel test program was undertaken. A family of nine low-aspect-ratio, all moveable control surfaces was used for test purposes. Each surface had a NACA 0015 airfoil section, square tip and a taper ratio of 0.45. Effective aspect ratios of 1, 2, and 3 and quarter chord sweep angles of 0, 11 and 22.5 degrees were employed. Faired gaps of up to 40% of the planform mean chord were tested. Using these models, the test was broken into the following three parts:

1. Free stream gap effects
2. Gap with simulated hull flow
3. Combined simulated hull flow and propeller slipstream effects for the minimum gap configurations.

Throughout this report, the "aspect ratio" referred to is the effective aspect ratio when the model is mounted on the tunnel floor. In this type of installation, the control surface is considered as a reflection plane model (with the tunnel floor as the reflection plane) having an effective aspect ratio equal to twice the geometric aspect ratio.

DESCRIPTION OF MODELS

Nine all-moveable control surface models were constructed. Each model had a 30 in. mean geometric chord, NACA 0015 airfoil section, square tip and 0.45 taper ratio. Three models each of effective

aspect ratio 1, 2 and 3 were made. For each aspect ratio, models having quarter chord sweep angles of 0, 11 and 22.5 degrees were constructed. The model planforms are presented in Figures 1 - 9. Each surface was constructed in such a manner that a support strut could be attached at the root chord at the axis of rotation. The axis of rotation was perpendicular to the mean geometric chord at the 25% mean chord point. The length of the support strut could be varied to change the gap size.

All gaps employed during the test were faired gaps. That is, a fairing piece was positioned between the root chord of the surface and the tunnel floor. The fairing piece stayed aligned at zero angle with the free stream when the control surface was rotated. The fairing pieces were constructed as extensions of the control surfaces. Figures 10 and 11 are drawings showing the details of two of the fairings while photographs of the models and fairings are presented in Figures 12-15.

TEST PROCEDURE

The control surfaces were mounted on the floor of the 7.75 foot by 11 foot test section of the wind tunnel with the support strut located on the vertical axis of the balance system. Force and moment measurements were made using the wind tunnel six-component balance system. Gap fairing pieces were mounted on the tunnel floor but not attached to the balance system so that only those aerodynamic forces and moments acting on the control surface were recorded. The free stream gap effect runs were conducted at a dynamic pressure, q , of 43.235 pounds per square foot (indicated airspeed of 130 mph). The Reynolds number based upon the mean geometric chord length was 3.04×10^6 .

Lift forces acting on the model mounted on the tunnel floor produced large rolling moments at the balance center (center line of test section). In order to keep the rolling moments from exceeding the balance limits at the desired Reynolds number, it was necessary to preload the balances. This was accomplished by placing a large static load on the balance turntable that produced a rolling moment that increased with angle of attack in the opposite direction of that caused by the model lift. Wind off static tare runs were made to obtain these corrections to the rolling moment.

Each of the nine control surfaces was tested to obtain the free stream gap effects. At least 6 gaps were tested for each surface. The gaps varied from a minimum of approximately 0.10 in. to 12 in. for the aspect-ratio 1 and 2 surfaces and up to 18 in. for the aspect ratio 3 surfaces. This corresponds to a maximum gap of 80% of the control surface span for the aspect ratio 1 surfaces and 40% of the span for the aspect ratio 2 and 3 surfaces.

After obtaining the free stream data, vanes and screen were installed at the entrance of the test section to produce a flow angularity and velocity gradient similar to that existing in actual conditions in the proximity of a ship hull. Figure 16 shows the vanes installed in the tunnel. The tunnel speed was adjusted to give the same velocity in the undisturbed flow as was used for the free stream tests. All of the control surfaces were tested for various gaps in this simulated hull flow.

To obtain slipstream effects, a 4 ft. diameter propeller was mounted between the hull simulation vanes and the control surface (Figure 17). Thus, the slipstream flow was superposed upon the simulated hull flow. For this condition, the nine control surfaces were tested only in the minimum gap position. To maintain the desired slipstream to free stream velocity ratio and not exceed the maximum propeller rpm, it was necessary to reduce the tunnel speed. This series of tests was conducted at a dynamic pressure of 18.92 pounds per square inch (indicated airspeed of 86 mph). The Reynolds number was 2.0×10^6 . To obtain a direct comparison with the free stream conditions, test runs were made for the minimum gap in the free stream at this lower value of Reynolds Number.

The angle of attack range was zero to $\pm 45^\circ$, except in a few instances where the model stalled at a slightly higher angle of attack.

PRESENTATION OF DATA

Results of the test are presented in nondimensional plotted form in Appendices A - C. These plots show lift and drag coefficients and chordwise and spanwise centers of pressure versus angle of attack. Data have been corrected for tunnel wall effects by computing the standard tunnel wall corrections for each control surface in the minimum gap configuration and applying these corrections to each run for that surface regardless of the gap size.

The effect of varying the gap size is shown in Figures 18-50. Whereas, Figures 61-87 show the effects of the hull simulation and propeller slipstream.

DISCUSSION OF RESULTS

FREE STREAM GAP EFFECTS

Due to the pressure differential across the gap on a lifting surface, air, or water in the case of ships, will leak through, thereby affecting the aerodynamic characteristics. Gap effects are treated theoretically in References 3 and 4. Theoretical results, neglecting the effects of viscosity, indicate large corrections to the pressures and velocities in the immediate vicinity of the gap. Theoretically, even small gaps result in very large losses in lift. However, in practical applications, viscous effects would alter the predicted theoretical results, especially when the gap is small.

Experimental data on gap effects suitable for control surfaces design is lacking. Due to the lack of experimental data, the author undertook an exploratory test (Reference 5) to determine experimentally the effects of a streamwise gap upon the aerodynamic characteristics of a representative all moveable control surface. The control surface used for this investigation had an effective aspect ratio of 2, a taper ratio of 0.45, quarter chord sweep of 22.5° , and a NACA 0015 airfoil section. Tests were conducted with an unfaired gap varying in size up to 4 inches or approximately 10 percent of the control surface span. Results of this study indicated that the gap effects upon the lift and drag values were considerably less than theoretical predictions, whereas, the effects upon the chordwise center of pressure shift were greater. This investigation resulted in the conclusion that it would be desirable to pursue the gap effect investigation for increased gap size and various surface geometries. The data presented in this report aid in fulfilling this need.

All gaps tested during this investigation were faired since this more nearly approximates the general condition for ship uses. The data presented in Reference 5 are for unfaired gaps.

Some of the control surfaces used in this investigation are similar to those used in the tests reported in Reference 2. The aerodynamic data for the minimum gap runs from this test should and do agree with the results presented in Reference 2. The force coefficients presented in the basic data (Appendix A) of this report are slightly lower, especially for the aspect ratio 1 surfaces. The reason the results of this

test are lower is that no correction for the boundary layer build up on the tunnel floor, at the control surface root chord, has been applied. This region of reduced velocity in the boundary layer extends approximately 2.2 in. above the tunnel floor. This reduced velocity region covers a sizeable portion of the aspect ratio 1 control surfaces which have a span of only 15 in. The effects of the boundary layer are less noticeable for the aspect ratio 2 and 3 surfaces which have larger spans. This boundary layer correction has not been applied to data presented in this report, since this is part of the gap effects which are of interest.

Free Stream Gap Effects Upon Lift

Free stream gap effects upon the control surface lift are presented in Figures 18-26. The data presented in these figures are cross plots of the lift coefficient for selected values of angle of attack, α , versus gap size. Representative angles of attack below the stall, an angle of attack close to the stall angle (approximately $C_{L \text{ max.}}$) and angles above stall, where appropriate, were selected. At low angles of attack, the gap fairing essentially eliminates any gap effects. This is evidenced in the cross plots.

A study of the cross plots reveals that the gap effects change with variation in the quarter chord sweep angle, whereas, a change in aspect ratio has little or no influence upon the gap effects. At a quarter chord sweep angle of zero degrees, the lift coefficient drops off as the gap is increased up to 1.25 in. then increases with increase in gap up to about 4 in. then decreases slowly as the gap increases to the maximum tested. The minimum lift coefficient, a little over 90% of the value obtained at minimum gap, occurs at the 1.25 in. gap. At the maximum gap, the lift coefficient is approximately 95% of the minimum gap value. For the 11 degree sweep angle, the lift coefficient decreases for small gaps, then increases slightly before dropping off at the large gap. The value of the lift coefficient does not drop below about 94% of the minimum gap value for this sweep angle. For the 22.5 degree sweep angle, the lift coefficient drops off as the gap increases up to about 3 in., then remains essentially constant. The lift coefficient at maximum gap is approximately 94% of that at minimum gap. When viewed in the light of the large lift losses expected from theoretical considerations, the observed losses are very moderate even for the most severe case.

The cross plots for the aspect ratio 1 control surfaces indicate a combination of the gap effects and an increased velocity effect, obtained by moving the control surface out of the boundary layer into the free stream as the gap increases. This velocity effect is evident for the

low angle of attack curves where the gap effects are negated by the fairings.

Lift data for angles of attack above the stall angle are faired with dashed lines to indicate the uncertainty of the values obtained in the stalled situation.

Data are presented for positive angles of attack only, since the airfoil sections are symmetrical and the results should be the same in either direction.

Free Stream Gap Effects Upon Drag

Drag coefficients cross plotted against gap size are presented in Figures 27-35 for representative angles. Generally speaking, the drag coefficients increase with increasing gap size in the small gap region (up to 2 or 3 in.) then decrease steadily as the gap approaches the maximum value. The final drag coefficient for the maximum gap condition is usually close to the minimum gap value. Overall gap effects upon the drag are small with no noticeable changes due to quarter chord sweep angle or aspect ratio.

Minimum drag coefficients ($\alpha = 0^\circ$) decrease slightly with gap size for most of the configurations. Since the gaps are faired in all cases, a change in drag would not be expected at $\alpha = 0^\circ$. This reduction in drag is probably due to a reduction in the interference drag at the intersection of the model and the tunnel floor. In actual installations, this drag would still be present but would be acting upon the fairing piece instead of the control surface.

Curves for the angles of attack greater than the stall angle of attack are faired with dashed lines to indicate the uncertainty of these values.

Free Stream Gap Effects Upon Chordwise Center of Pressure Location

Cross plots of the chordwise center of pressure locations against gap size for selected angle of attack values are presented in Figures 36-44. As was noticed for the forces, the fairing pieces eliminate gap effects in the lower angle of attack range. For the aspect ratio 1 control surfaces, the chordwise center of pressure moves aft approximately 1.5 to 2 percent as the gap is increased from the minimum value to 2.0 or 2.5 in. As the gap size increases above this value, there is very little change in the center of pressure location. For the aspect ratio 2 and 3 control surfaces, the center

of pressure moves aft as the gap size is increased (up to 1.5 to 3.0 in., depending on the quarter chord sweep angle) then moves forward with increasing gap size. The maximum rearward center of pressure shift varies with the sweep angle, decreasing with increasing quarter chord sweep. The maximum center of pressure shift is about 4 percent and occurs at a 1.5 in. gap for a sweep angle of zero degrees. The chordwise center of pressure location for the maximum gap size tested was always aft of the minimum gap size location. However, this shift did not exceed 2 percent of the chord length for any of the control surfaces tested.

Free Stream Gap Effects Upon Spanwise Center of Pressure Location

Spanwise center of pressure location cross plots are presented in Figures 45-50. Before reviewing these, it is necessary to discuss the accuracy of the spanwise center of pressure calculations. As was mentioned previously, the control surfaces were mounted on the tunnel floor. This produced large rolling moments about the balance center, which is located on the test section center line. In order to keep the rolling moment balance from reaching the limit of its travel, large weights were placed on the balance turntable which produced a static variation with angle of attack that counterbalanced the aerodynamic rolling moment. Since this variation of rolling moment with angle was large, a small error in setting the angle produced appreciable errors in the rolling moment. In percent of total rolling moment experienced, the errors were quite small, but in the low angle of attack region where the aerodynamic forces are relatively small, the error becomes appreciable. It is estimated that the error in rolling moment is ± 2.5 ft. lbs. With spanwise center of pressure defined as follows:

$$(CP)_s = \frac{C_f \cos \alpha - C_n \sin \alpha}{C_L \cos \alpha + C_D \sin \alpha}$$

it is seen that an error in rolling moment, C_f , will cause a sizeable error in $(CP)_s$ at small values of angle of attack, α , where the lift and drag values are small. At larger values of α , lift and drag become greater decreasing the effect of the error in rolling moment. It is also evident that the error will be greater for the small aspect ratio control surface since the aerodynamic forces are smaller. For the aspect ratio 1 control surfaces, the error in $(CP)_s$ is considerable throughout the whole range of angle of attack. The data are presented in the plots of the basic data in Appendix A, but due to the scatter, no cross plots are presented. The data for the high angle of attack on the aspect ratio 2 surfaces are within ± 1 percent and aspect ratio 3 data is not affected appreciably by the error in rolling moment.

A look at the spanwise center of pressure location cross plots shows that the gap effect is negligible in the data presented.

Summary of Free Stream Gap Effects

Free stream gap effects are considerably less than would be expected from theoretical considerations for the control surfaces tested. Aspect ratio appears to have no bearing upon the gap effects. There is a change in gap effects with variation in the quarter chord sweep angle, with the greatest effects occurring for zero sweep angle. Generally speaking, the maximum effects are in the region of small gaps (2 to 3 in.) with the effects diminishing as the gap increases. The fact that maximum gap effects occur in the 2 to 3 in. region (not a certain percent of span) may be a consequence of the boundary layer on the tunnel floor, which is approximately 2.20 in. thick. It is possible that a different boundary layer thickness may change the region of maximum gap effects. No attempt was made during this investigation to validate this statement.

GAP EFFECTS WITH SIMULATED HULL

For the purpose of hull simulation, it was decided to attempt to duplicate the wake velocity diagram of Figure 11 of Reference 6. This figure has been reproduced for convenience as Figure 51 in this report. Turning vanes and screens were installed in the entrance to the test section as shown in Figure 16 to produce the desired flow angularity and velocity gradient. The resulting flow distribution is presented in Figure 52. A comparison of Figures 51 and 52 shows that a reasonable simulation was obtained. A comparison of the streamwise components of velocity are presented in Table I.

With the simulated hull flow, gap effects become enmeshed with the velocity gradient effects. As the gap size is increased, the control surface moves into a higher average velocity stream. Since all force coefficients are based upon the free stream velocity, a reduced velocity near the hull results in reduced values of the coefficients. Therefore, the force coefficients increase as the gap size increases due to increased velocity over the control surface.

In the free stream investigation, it was found that gap effects on the configurations tested were relatively small. For this reason, only the data for the control surface exhibiting the greatest gap effects (aspect ratio 2, quarter chord sweep angle equal zero degrees) are presented in

the cross plots of Figures 53-56. As was noted previously in the free stream condition, gap effects at small angles of attack are negligible due to the fairing pieces.

Comparing Figures 21 and 53, the gap effects upon the lift coefficient in the small gap region, where velocity gradient effects are small, show the same characteristics for both free stream and simulated hull effects. As the gap is increased, the effects of the velocity gradient for the simulated hull flow are evidenced. The lift coefficient for the maximum gap tested is greater than that obtained for the minimum gap condition.

Comparing the drag values presented in Figures 30 and 54, shows the same relationships prevailing as mentioned for the lift coefficients. That is, gap effects are essentially the same for both conditions in the small gap region and velocity gradient effects predominate in the large gap region.

With chordwise center of pressure defined:

$$(CP)_{\bar{c}} = .25 - \frac{C_m}{C_L \cos \alpha + C_D \sin \alpha},$$

velocity effects are present in both the numerator and denominator of the second term on the right, thereby eliminating the velocity gradient effects. This is seen to be the case by comparing Figures 39 and 55. The gap effects are seen to be essentially the same for both conditions.

Figure 56 shows that the gap effects upon the spanwise center of pressure location are negligible as was the case for the free stream investigation.

From the comparisons above, it may be noted that while the hull simulation does change the magnitude of the force coefficients, it has very little influence on the gap effects. These being essentially the same as for the free stream situation.

SIMULATED HULL FLOW AND PROPELLER SLIPSTREAM EFFECTS

In an effort to gain some insight of the propeller slipstream effects on the aerodynamic characteristics of the control surface, a propeller was mounted in the test section between the hull simulation vanes and the control surface being tested (See Figure 17). It was

desired to duplicate the flow depicted in Figure 5 of Reference 7. For convenience, the information presented in Figure 5 of Reference 7 is shown in Figure 57 of this report. Several difficulties were encountered in trying to duplicate the desired flow conditions. The first and probably the most severe difficulty was that the scope of the contract did not permit the construction of a propeller and drive system which would be in the proper geometric proportion to the control surfaces. Therefore, it was necessary to use an existing propeller and drive motor (borrowed from the David Taylor Model Basin) that was larger than was desired. Also, since there was no information available on the allowable speed of this propeller, a conservative rpm limit was established for the tests. In order to obtain the desired ratio of slipstream to freestream velocity with this allowable rpm, it was necessary to reduce the tunnel velocity from that used in the preceeding portion of the test. Another problem was that with the existing velocity survey equipment, it was not possible to obtain measurements at all the desired locations. The final difficulty encountered was that the hull effects are not known for the data presented in Reference 7. For the purpose of this test, the propeller slipstream is superposed upon the simulated hull flow discussed previously. This simulated hull flow may be considerably different from that existing for the reference ship.

Results of the wake velocity surveys are presented in Figures 58-60. For each aspect ratio, the propeller was positioned so that the slipstream enveloped 60 percent of the span of the control surface. In spite of the difficulties enumerated, there is good qualitative agreement in regards to flow angularity and velocity ratios between the test conditions and those presented in Reference 7. It should be noted that it is the port side of the ship that is being simulated. In this simulation positive angle of attack ($+\alpha$) corresponds to right rudder.

Data are presented in Figures 61-87 for comparison of the free stream, simulated hull, and simulated hull with slipstream conditions. In comparing the simulated hull data with the free stream characteristics, the following may be observed:

1. The lift and drag curves for the simulated hull flow exhibit an angle shift and a reduced q , dynamic pressure, effect. Observed effects are:

Aspect Ratio	Shift in α Degrees	Effective q % Freestream q
1	3.5	75
2	2.5	83
3	2.5	87

This angle shift is a result of the average simulated flow angle, whereas the reduced q effect arises from the velocity gradient in the simulated flow. These results are what would be expected from the flow that is simulated and could be predicted with reasonable accuracy from a knowledge of the flow angularity and velocity gradient in the vicinity of the control surface.

2. After eliminating the effects of the shift in α from the chordwise center of pressure curves, it may be noted that the $CP_{\bar{c}}$ moves aft with an increase in the quarter chord sweep. There is a maximum shift of approximately 2 percent of the chord for a sweep angle of 22.5 degrees. This rearward shift of $(CP)_{\bar{c}}$ with sweep is a consequence of the velocity gradient.
3. There is a slight inboard shift of the spanwise center of pressure location for the aspect ratio 2 control surfaces as a result of the simulated hull flow and a slight outboard shift for the aspect ratio 3 surfaces. The inboard $(CP)_s$ shift for the aspect ratio 2 control surface is opposite to that expected due to the increased velocity over the outboard portion of the control surface.

Slipstream effects combined with the simulated hull flow vary with aspect ratio. The probable cause of this variation is the twist in the slipstream, since this would be different for each of the aspect ratios tested (See Figures 58-60). The following slipstream effects are noted:

1. Increased slipstream velocity overcomes the reduced velocity effects of the hull simulation.
2. Slipstream twist overcomes the effects of the hull flow angularity.
3. The lift versus angle of attack curve is extended with the stall angle of attack being from 3 to 6 degrees greater in every instance.
4. Slipstream drag values are consistently higher for negative angles and slightly less or equal to free stream values for positive angles of attack.
5. Chordwise and spanwise center of pressure locations vary considerably for the different aspect ratios tested. The results differ with angle of attack.

From these results, it is seen that the propeller slipstream has significant effects upon the control surface characteristics. These effects vary with the slipstream velocity and twist experienced by the control surface, being different for each aspect ratio.

The results show large shifts in the centers of pressure which are not readily predictable. Results presented here represent one flow condition and should be construed as only a general indication of the effects of the propeller slipstream. Since the effects are significant upon the center of pressure locations, it would have been desirable to determine the cause of these shifts to see whether or not they could be predicted. This, however, was outside of the scope of this contract.

CONCLUSIONS AND RECOMMENDATIONS

From the experimental results of this investigation, free stream gap effects are presented as cross plots for faired streamwise gaps. The results indicate that the fairing pieces eliminate any gap effects in the small angle of attack region (up to about 10°). At large angles of attack, the gap effects are found to be considerably less than those anticipated from theoretical considerations. Gap effects are greatest for those control surfaces having zero quarter chord sweep angle and occur for gaps of about 10% of the control surface span. For maximum gaps tested (up to 40% span for aspect ratio 2 and 3 surfaces and 80% span for aspect ratio 1 surfaces) lift losses are small. Nowhere do they exceed 6% of the minimum gap value. Results of this investigation indicate there is a need for more information in the following areas:

1. theoretical characteristics at infinite gap for the family of control surfaces used in this investigation for comparison with the experimental results,
2. effects of boundary layer thickness upon the gap effects,
3. physical changes in the flow over the control surface as a result of streamwise gaps.

Results of the simulated hull flow investigation indicate that the hull effects are readily predictable if the flow conditions at the control surface location are known.

For the propeller slipstream investigated, drag force and center of pressure locations vary significantly in a manner that is not readily predictable. It should be pointed out that these results are for a parti-

cular hull flow simulation and propeller-control surface geometry; hence, the effect of a given hull configuration and propeller slipstream on the control surface characteristics must be considered for each specific design. These results indicate a further need for investigation of the propeller slipstream effects to determine whether or not these effects can be predicted with reasonable accuracy or if there is an optimum position for the control surface within the slipstream.

ACKNOWLEDGEMENTS

The author wishes to express his appreciation to Mr. J. N. Fresh of the David Taylor Model Basin for his assistance in locating a propeller and drive motor for use in the slipstream investigation.

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5. Windsor, R. I., "Experimental Investigation of Streamwise Gap Effects Upon the Aerodynamic Characteristics of a Low Aspect Ratio All Movable Control Surface", University of Maryland Wind Tunnel Report No. 453, 1965.
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7. Macovsky, M. S., Duerr, R. J. and Jewell, D. A., "An Investigation of a Flow-Excited Vibration of the U. S. S. Forest Sherman (DD931)" David Taylor Model Basin Hydromechanics Laboratory Research and Development Report, Report 1188, August, 1958.

TABLE I
SIMULATED HULL FLOW
LONGITUDINAL VELOCITY COMPONENT, V_x/V

POSITION NUMBER (SEE FIG. NO. 51)	FROM FIG. 11 REFERENCE 5	FROM TEST SECTION SURVEY
101	0.785	0.876
102	0.859	0.862
103	0.965	0.871
104	0.992	1.023
105	1.025	1.027
106	1.022	0.983
107	1.019	0.944
108	1.019	1.026
109	1.019	1.025
110	0.988	1.020
111	0.974	1.025
112	0.962	1.019
113	0.903	1.018
114	0.816	0.957
201	0.826	0.864
202	0.812	0.886
203	0.918	0.880
204	0.976	0.867
205	1.020	1.028
206	1.018	1.027
207	1.015	1.017
208	1.011	1.025
209	1.009	1.025
210	0.993	1.028
211	0.973	1.024
212	0.916	0.963
213	0.813	0.879
214	0.814	0.878
301	0.795	0.823
302	0.773	0.818
303	0.861	0.893
304	0.973	0.873
305	1.030	1.023
306	1.007	1.025
307	1.002	1.031
308	1.007	1.028
309	1.010	1.030
310	1.001	1.026
311	0.975	1.027
312	0.931	0.881
313	0.819	0.883
314	0.722	0.894

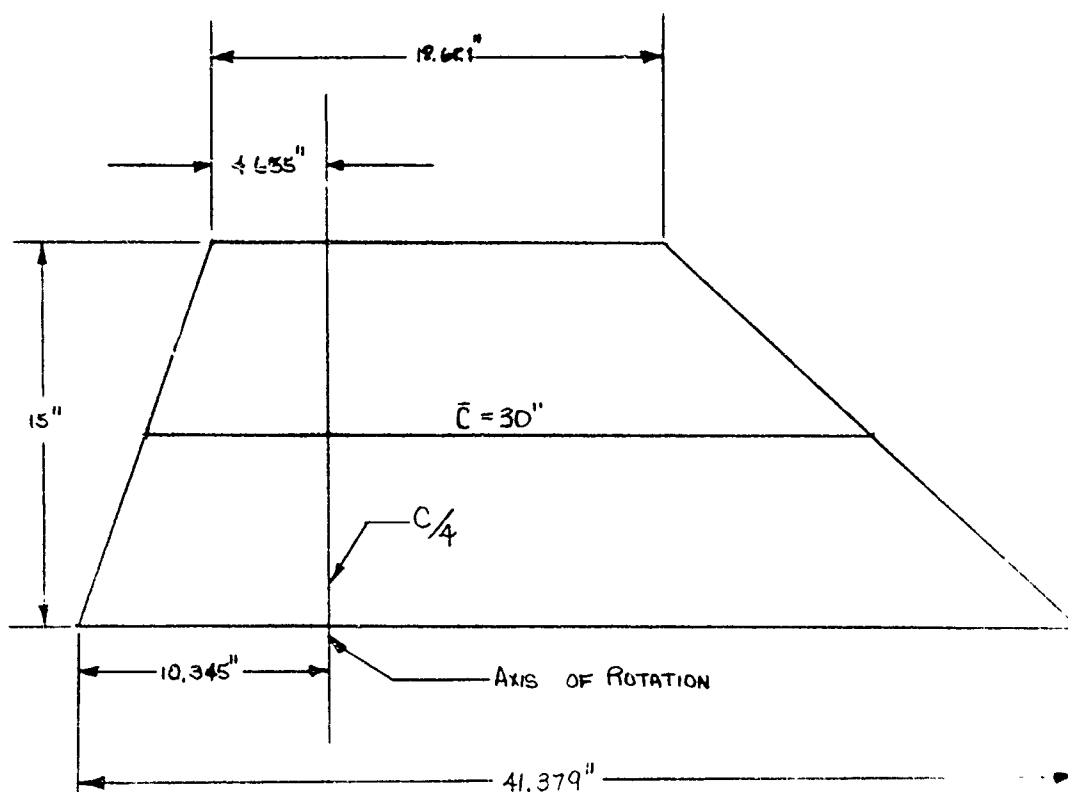


Figure No. 1
Basic Dimensions

EFFECTIVE $AR = 1$
 $\Delta = 0$

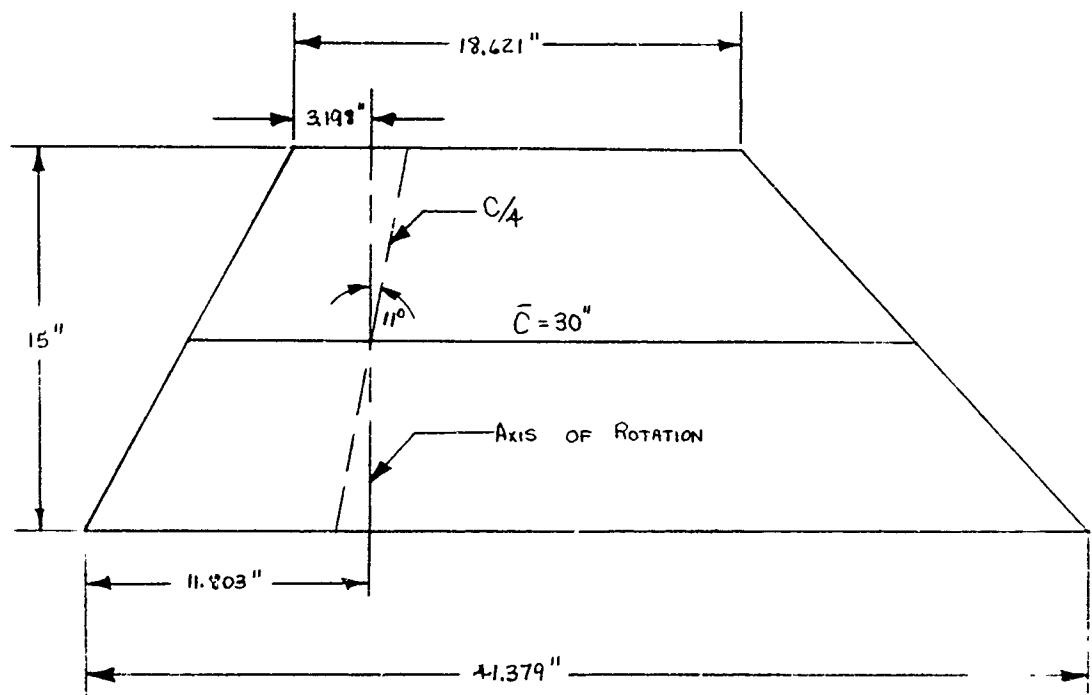


Figure No. 2
Basic Dimensions

EFFECTIVE AR = 1

$\angle = 11$

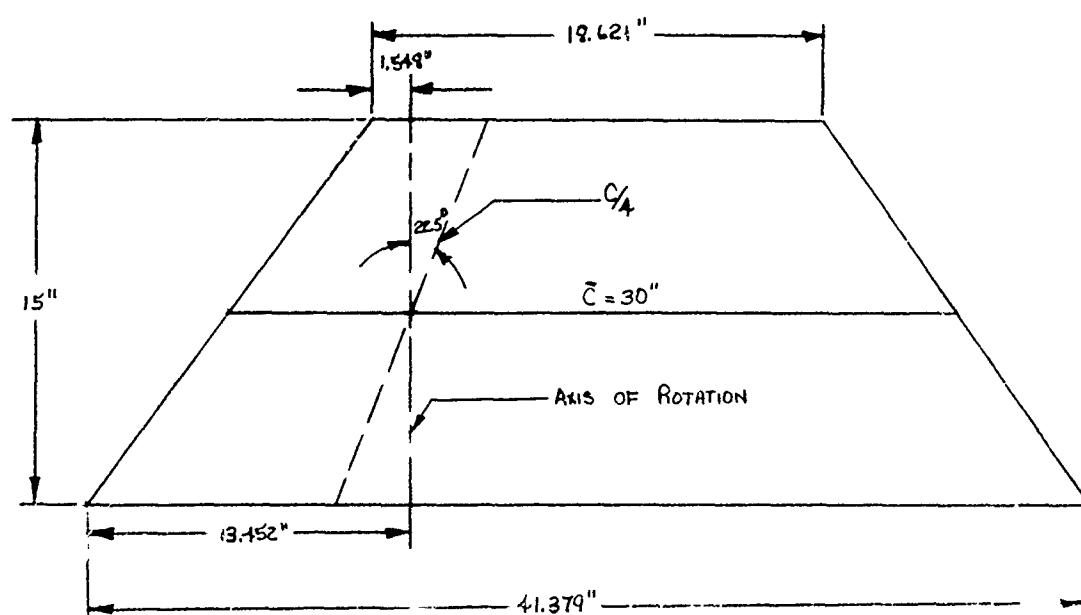


Figure No. 3
Basic Dimensions

EFFECTIVE $AR = 1$
 $\angle = 22.5$

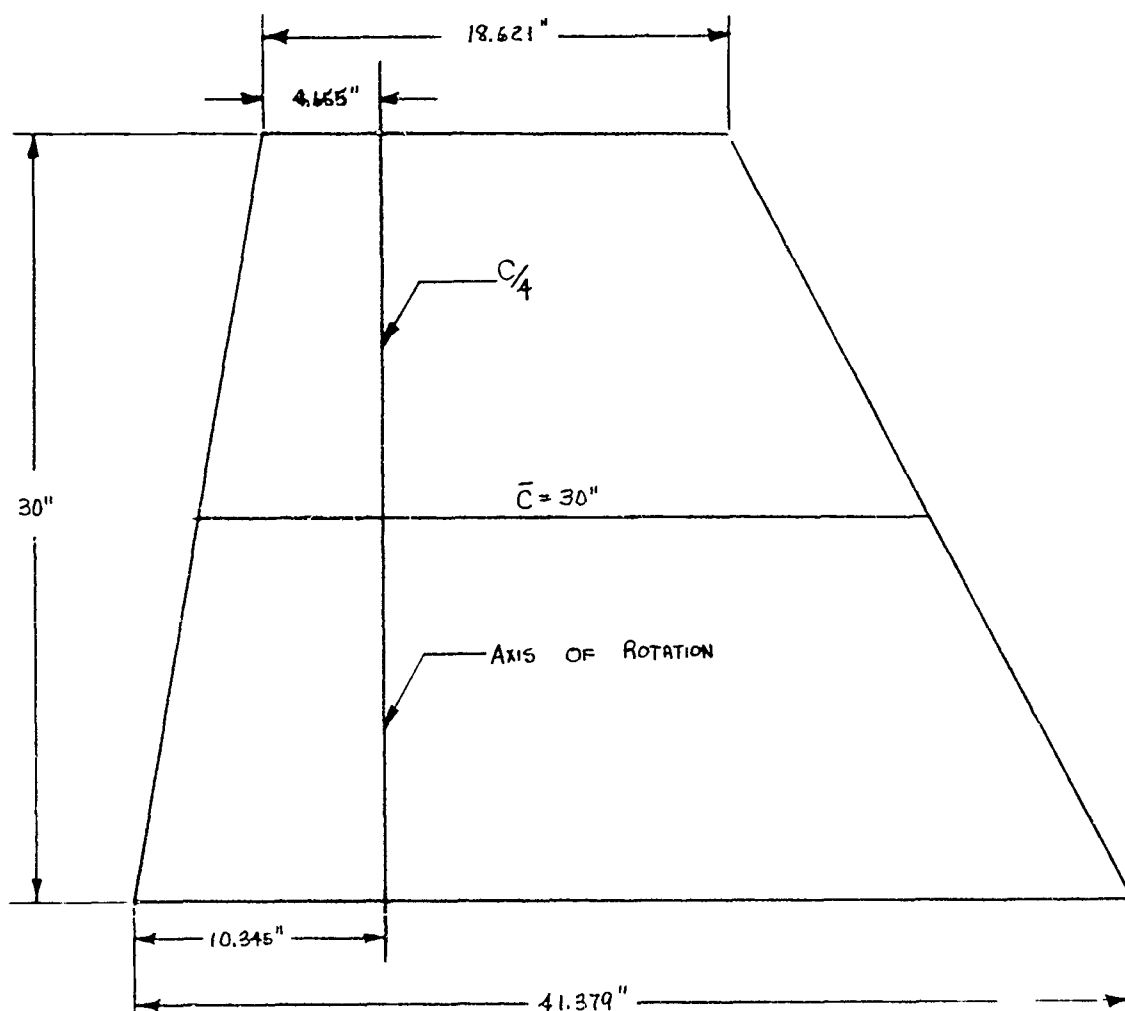


Figure No. 4
Basic Dimensions

EFFECTIVE AR = 2

$\angle = 0$

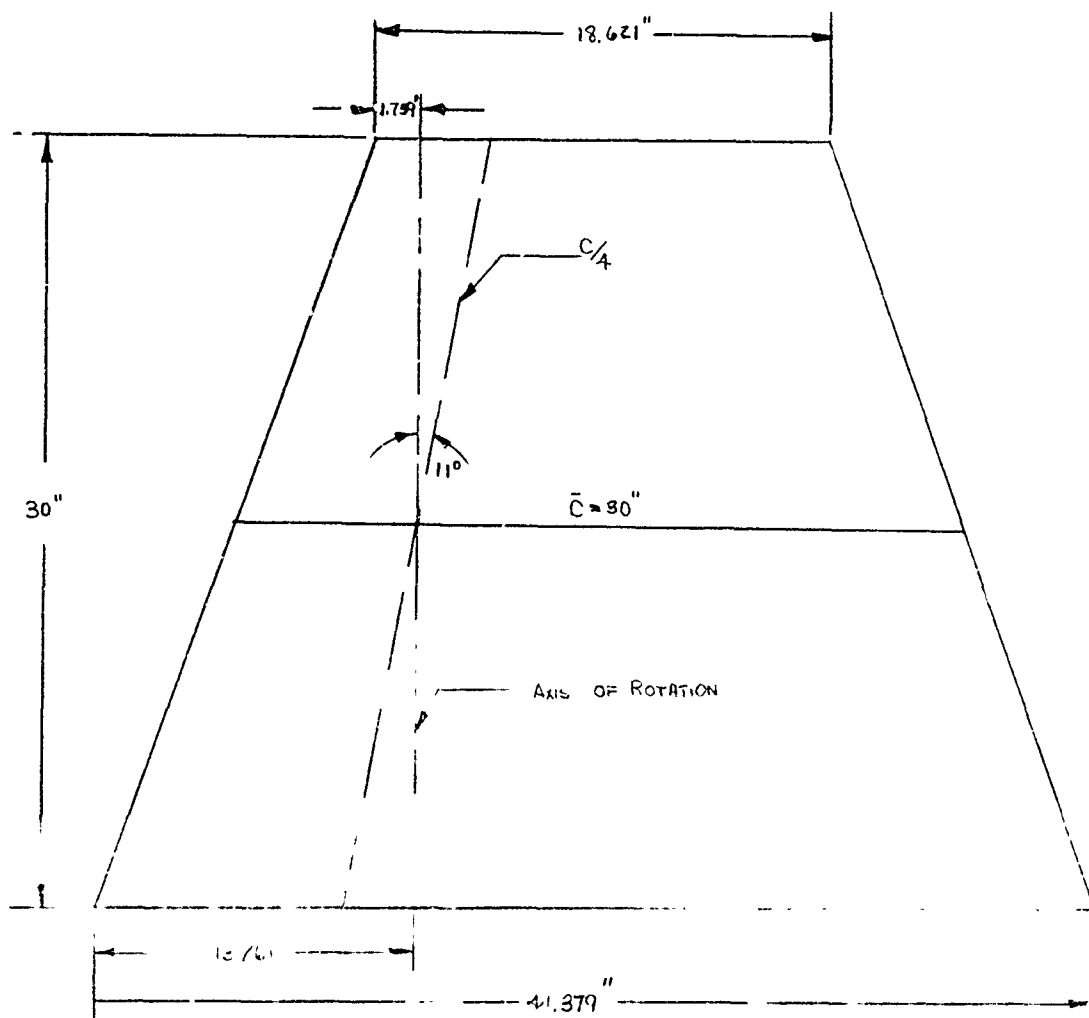


Figure No. 5
Basic Dimensions

EFFECTIVE AR = 2

$\angle = 11$

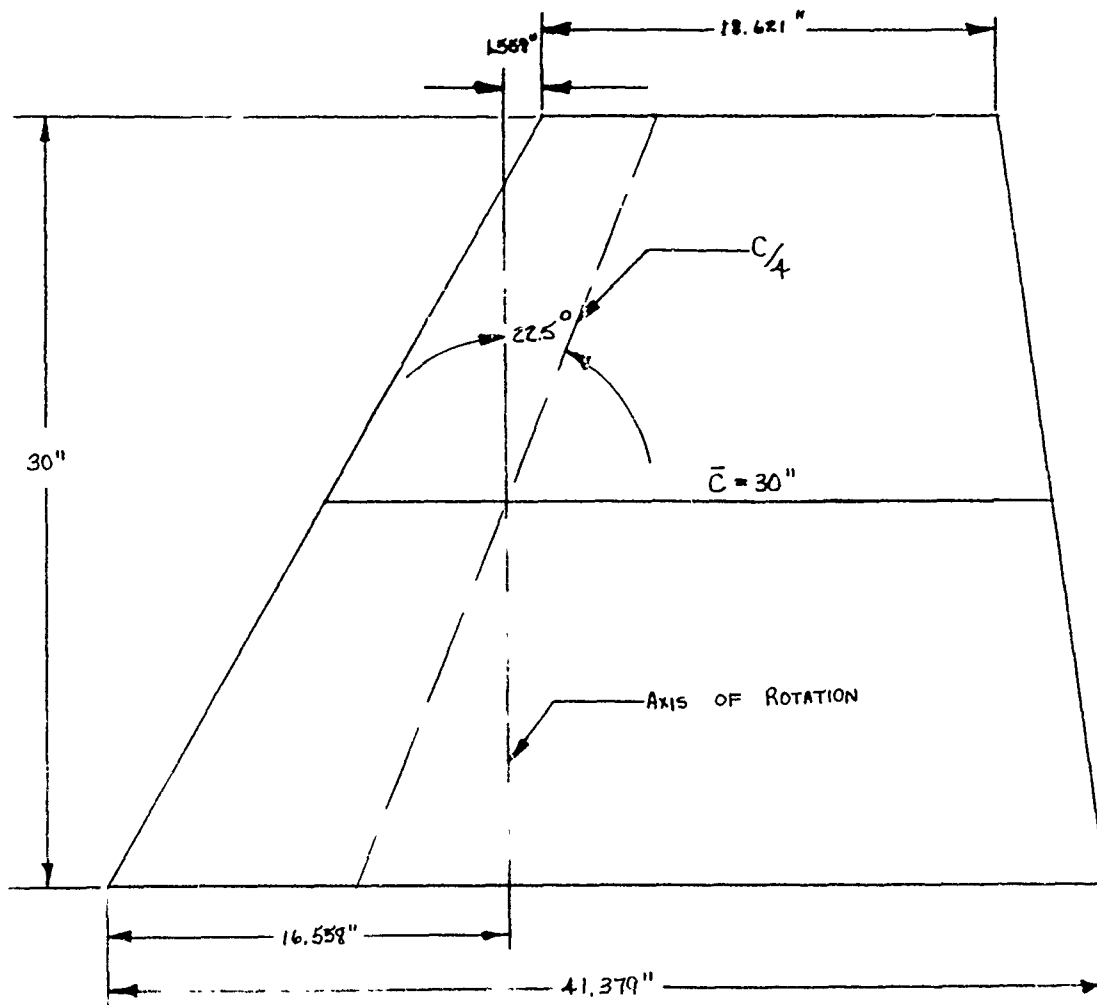


Figure No. 6
Basic Dimensions

EFFECTIVE $AR = 2$

$\angle = 22.5$

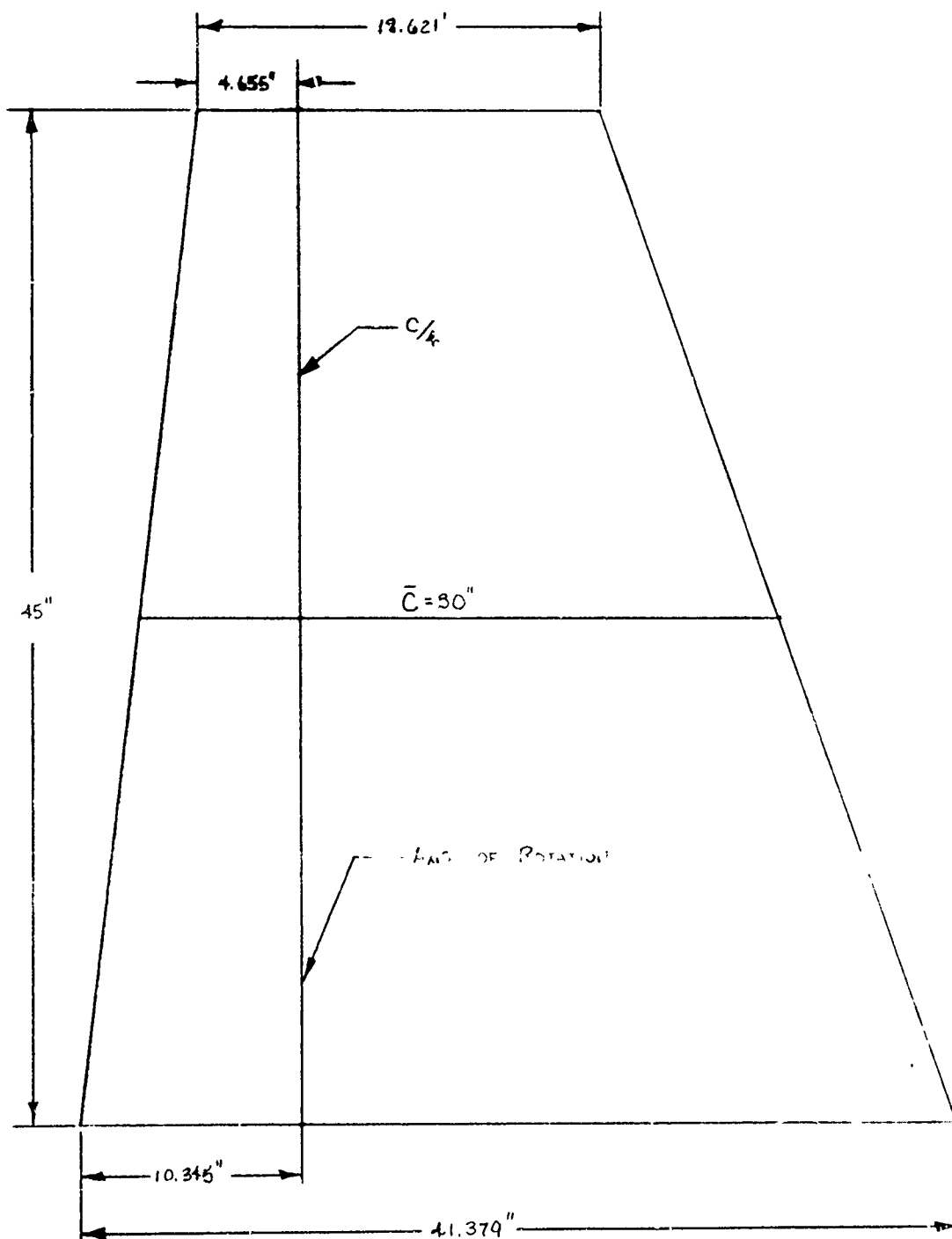


Figure No. 7
Basic Dimensions

EFFECTIVE $AR = 3$

$\mathcal{A} = 0$

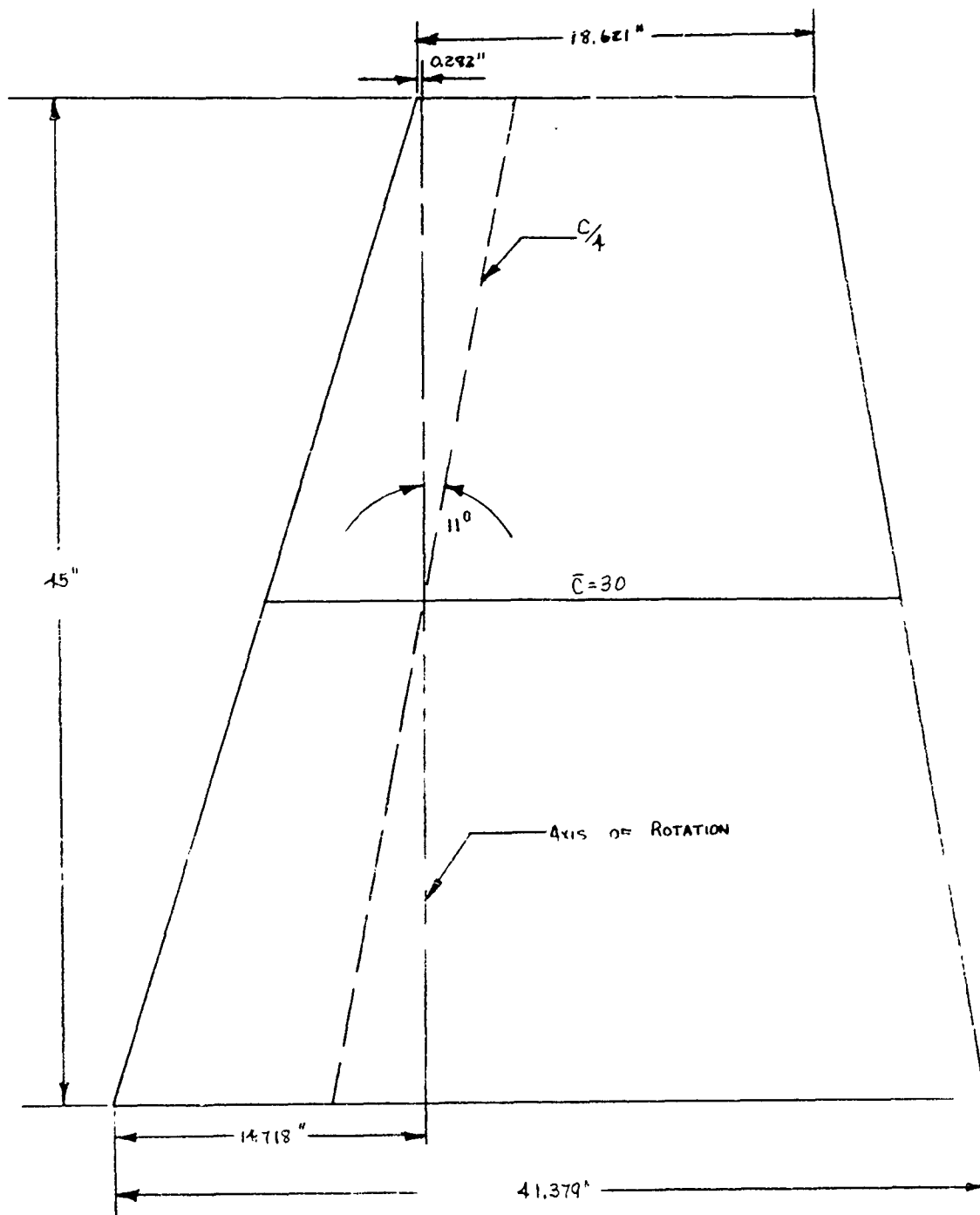


Figure No. 8
Basic Dimensions

EFFECTIVE AR = 3

$\lambda = 11$

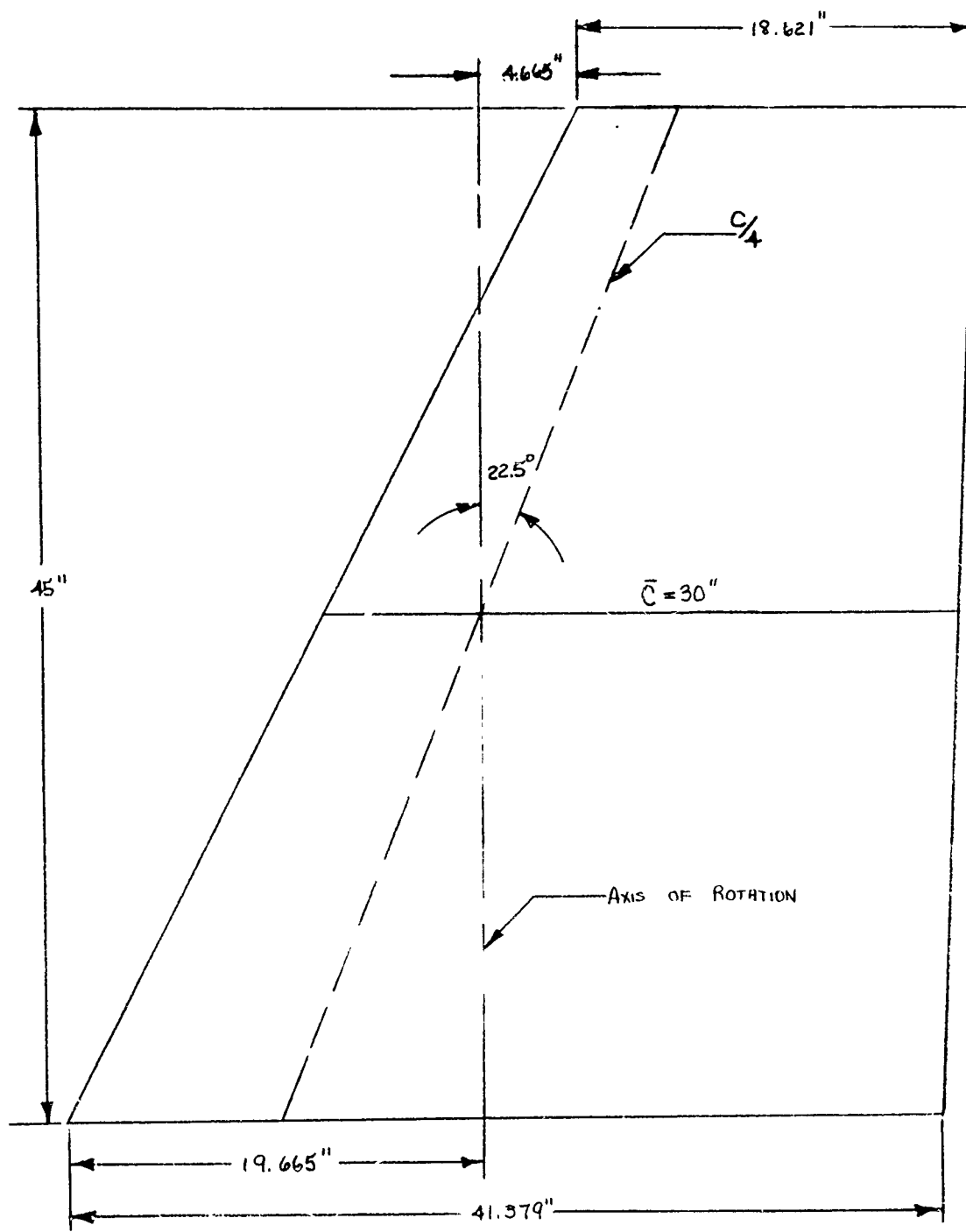


Figure No. 9
Basic Dimensions

EFFECTIVE AR = 3
 $\angle = 22.5$

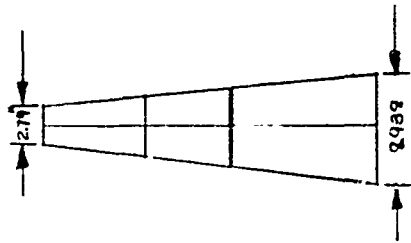
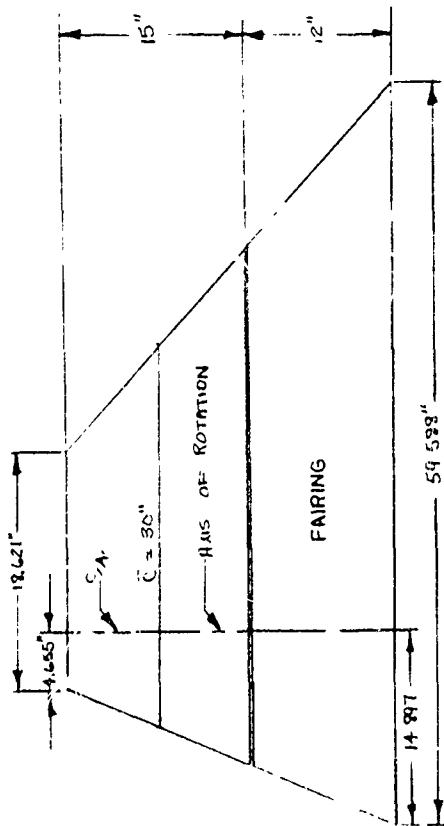


Figure No. 10
Fairing Details

EFFECTIVE AR = 1
 $\lambda = 0$

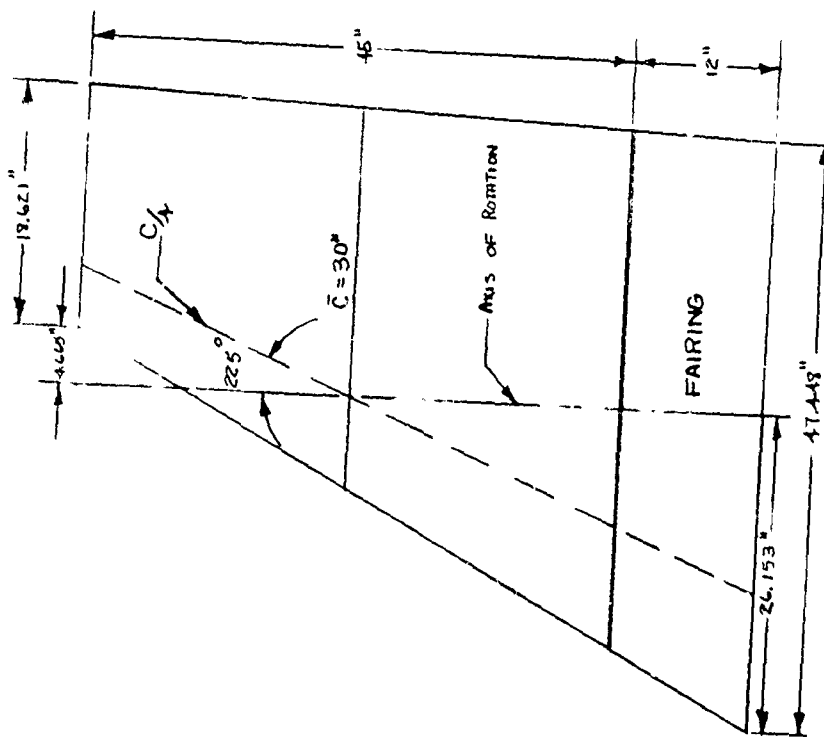


Figure No. 11
Fairing Details

EFFECTIVE $AR = 3$

$\Lambda = 22.5$

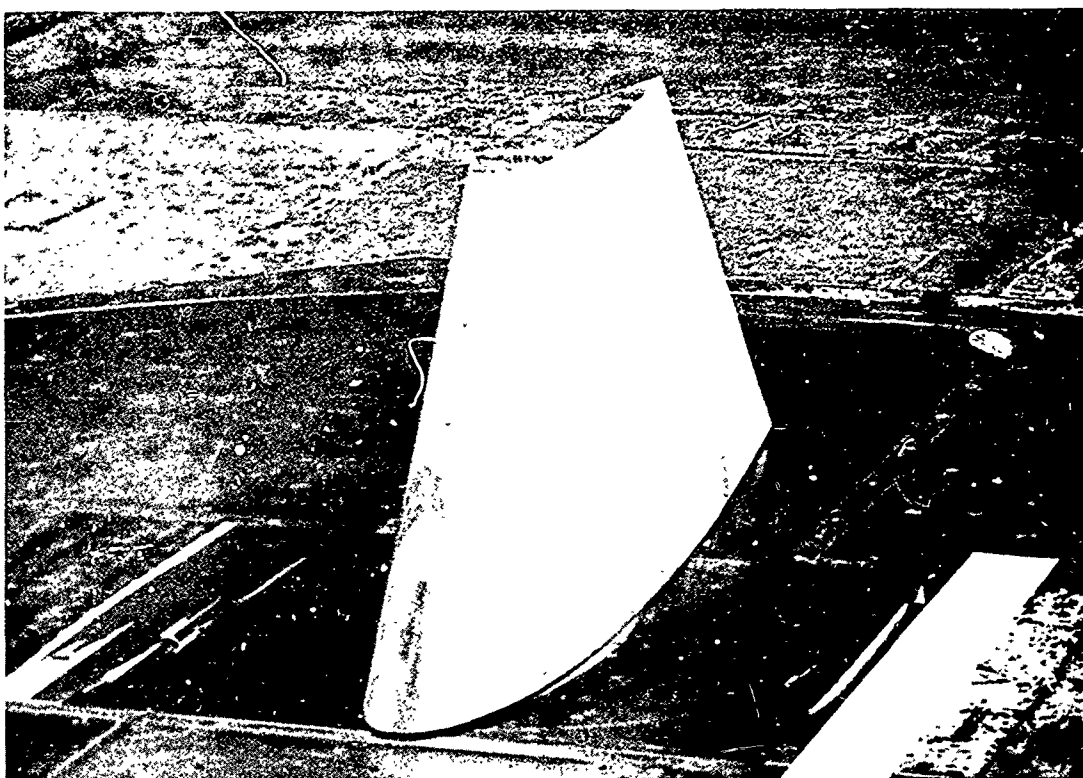


Figure No. 12. Aspect Ratio 1, $\Lambda = 11^\circ$, Control Surface Mounted on Tunnel Floor With Minimum Gap.

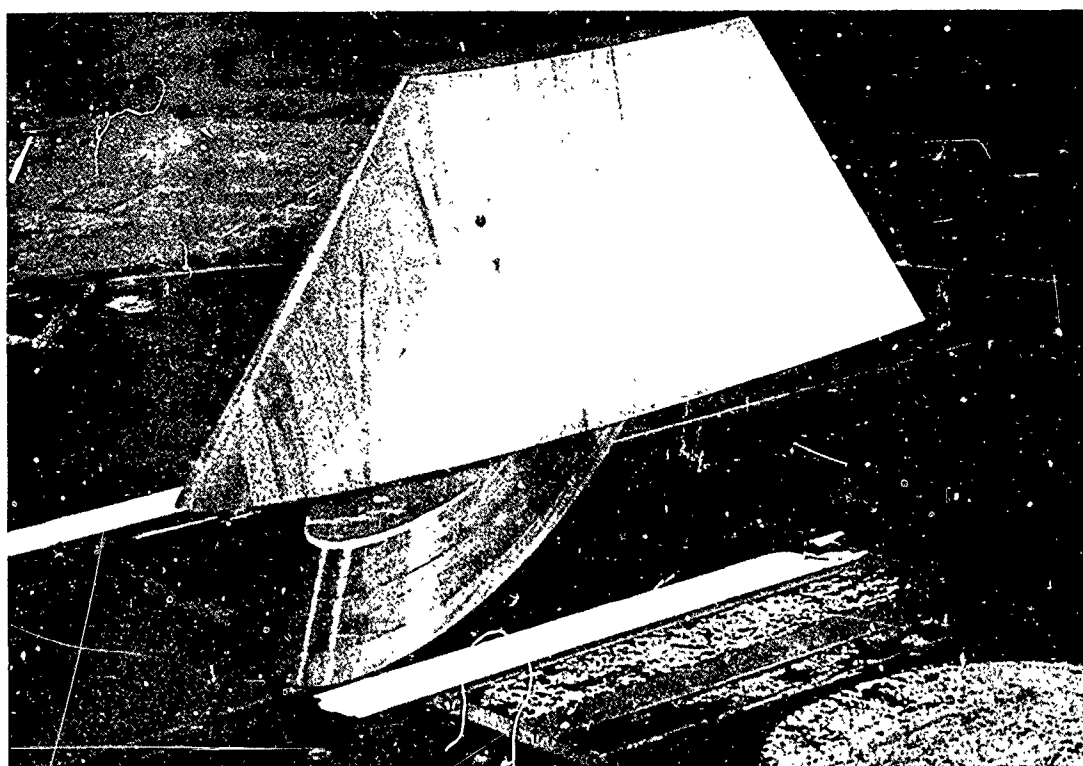


Figure No. 13. Aspect Ratio 1, $\Lambda = 22.5^\circ$, Control Surface With 4.5 inch Gap, $\alpha = 35^\circ$.

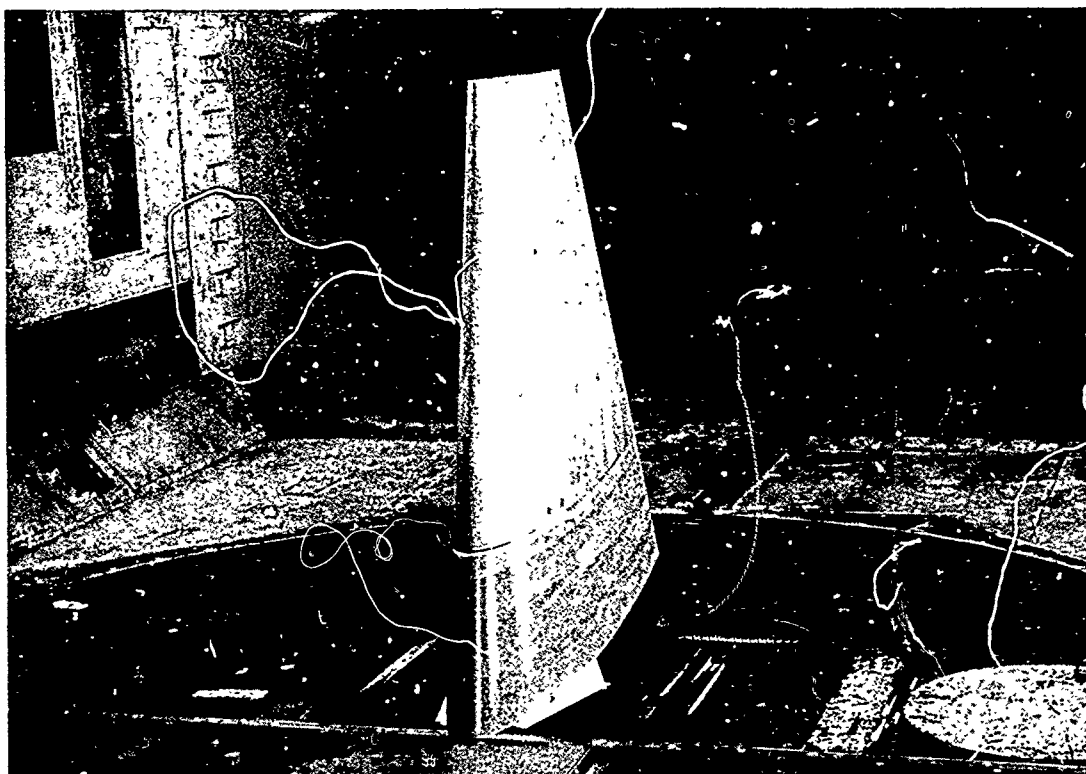


Figure No. 14. Aspect Ratio 2, $\Lambda = 0^\circ$, Control Surface With 12 inch Gap, $\alpha = 0^\circ$.

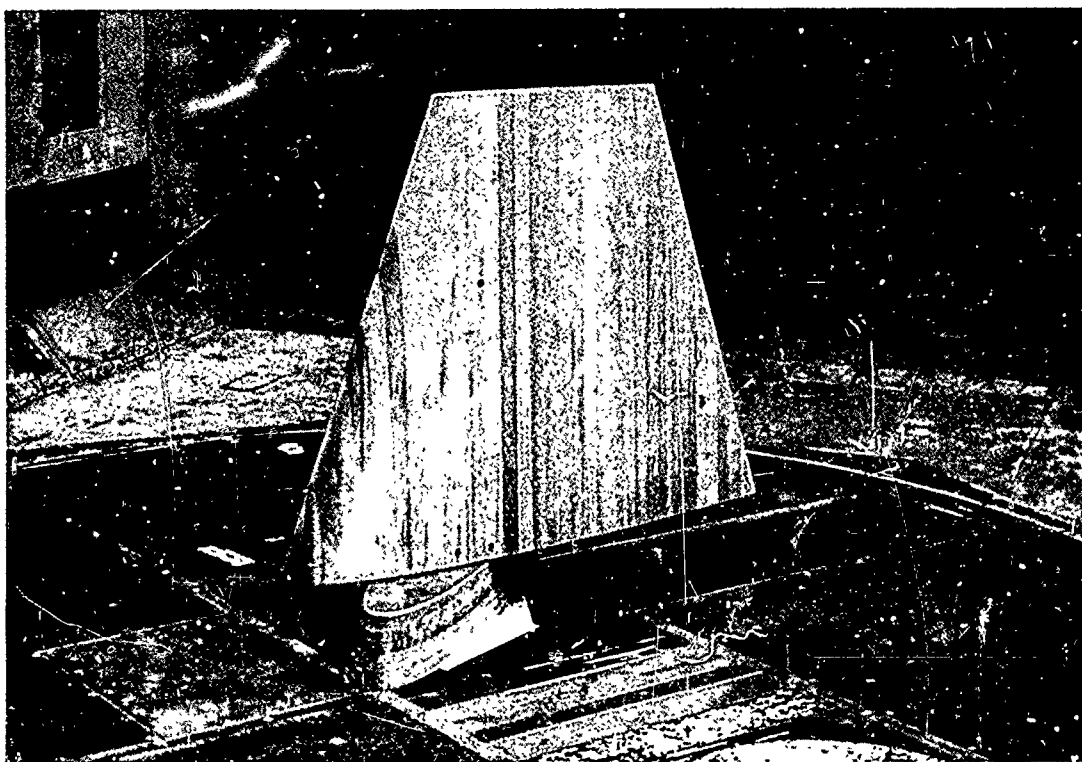


Figure No. 15. Aspect Ratio 2, $\Lambda = 11^\circ$, Control Surface With 4.5 inch Gap, $\alpha = 30^\circ$.

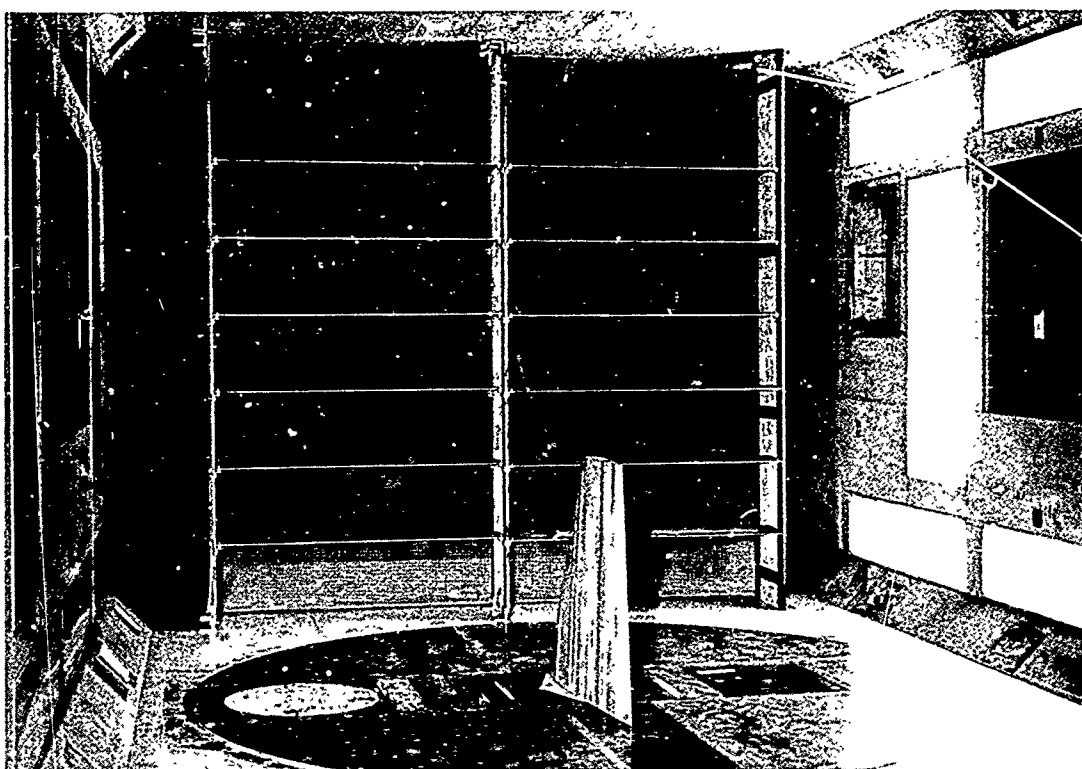


Figure No. 16. Turning Vanes and Screen Installed at Leading Edge of Test Section to Simulate Hull Flow Conditions.

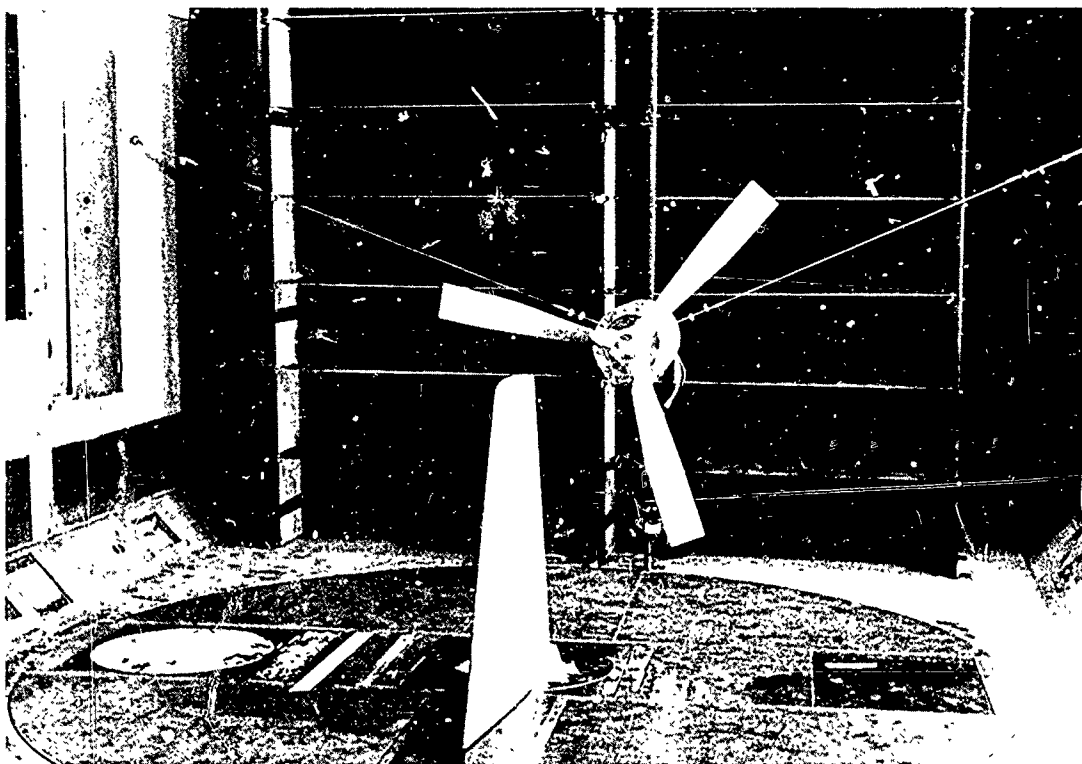
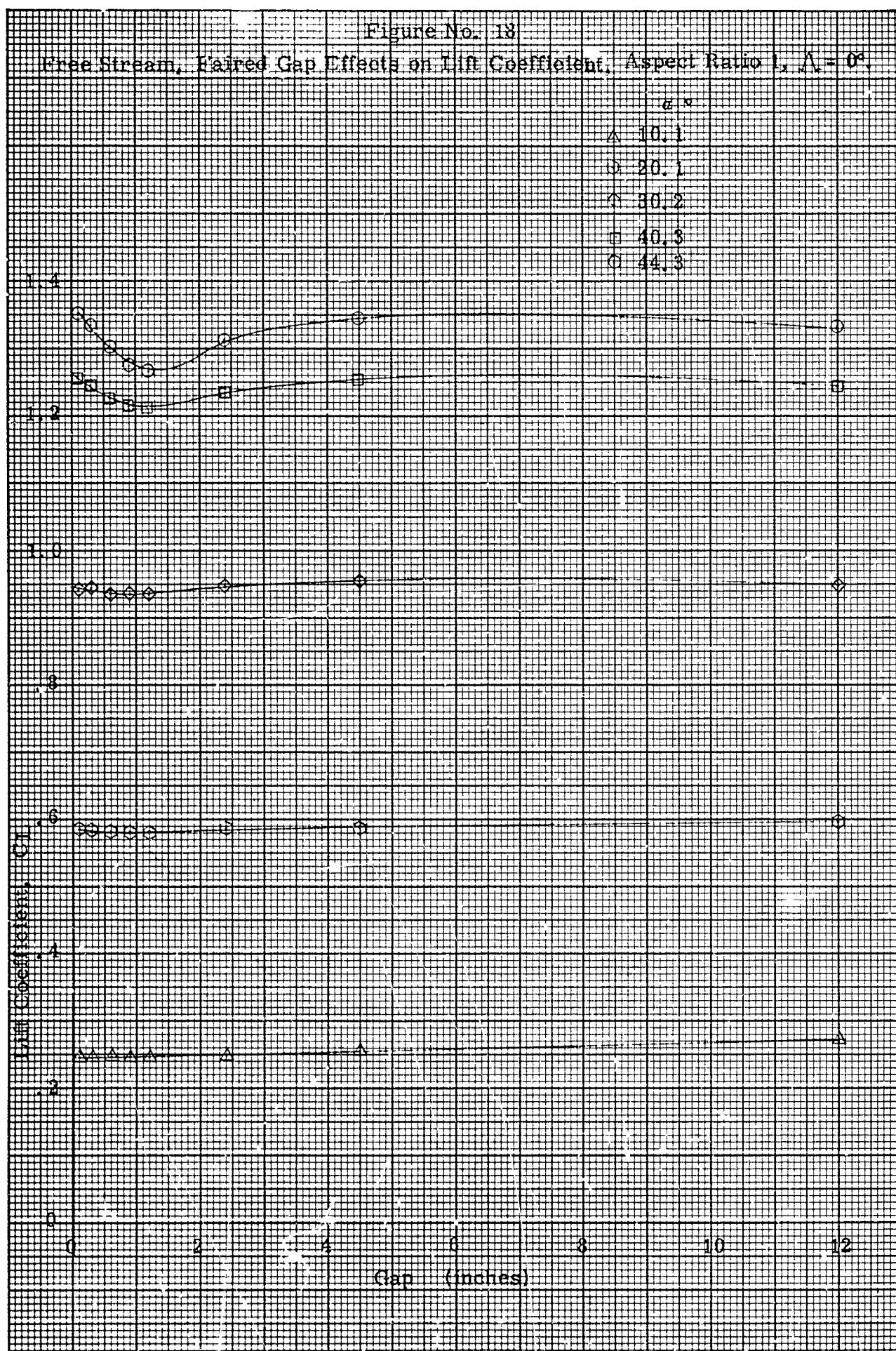
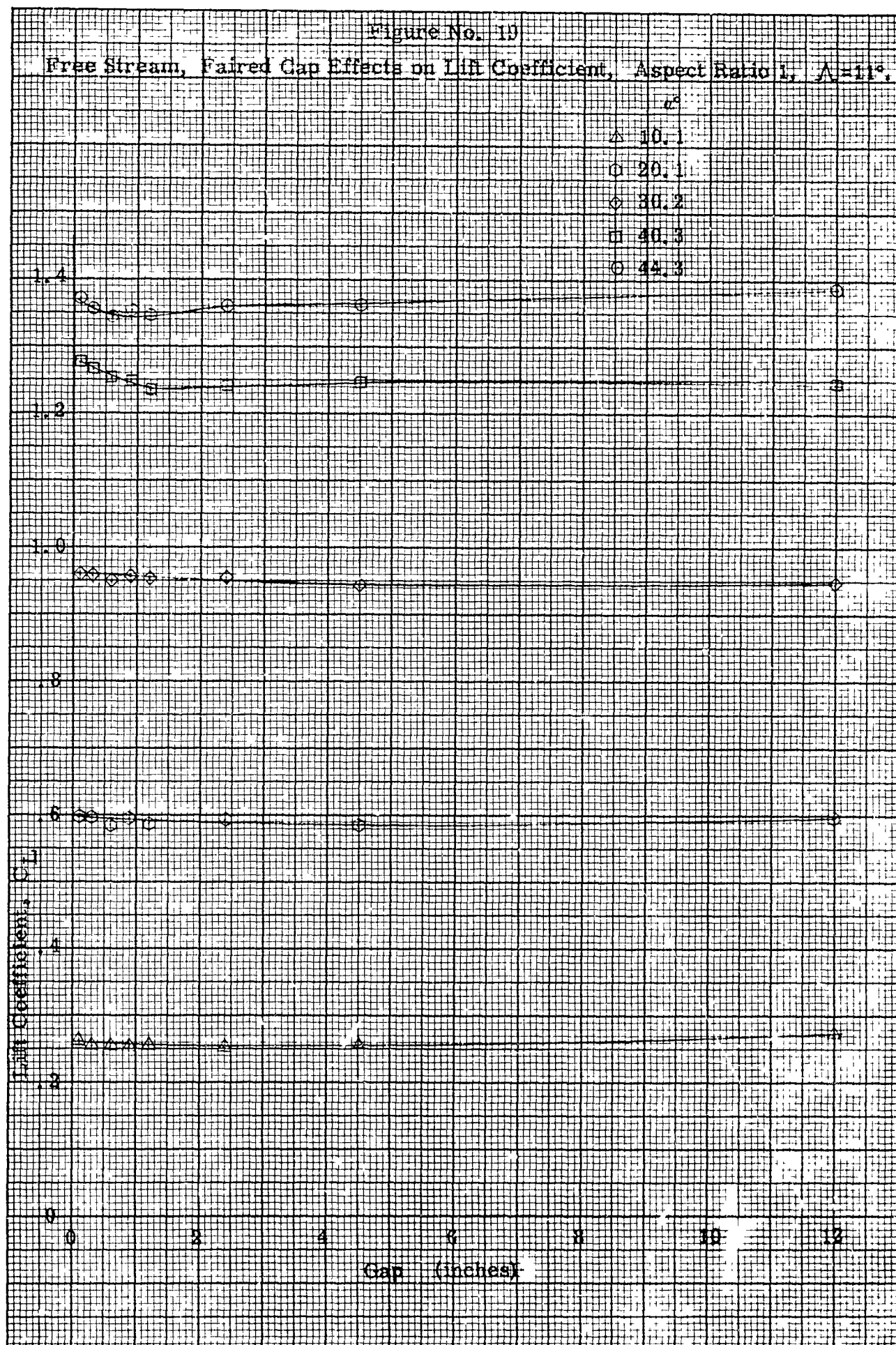
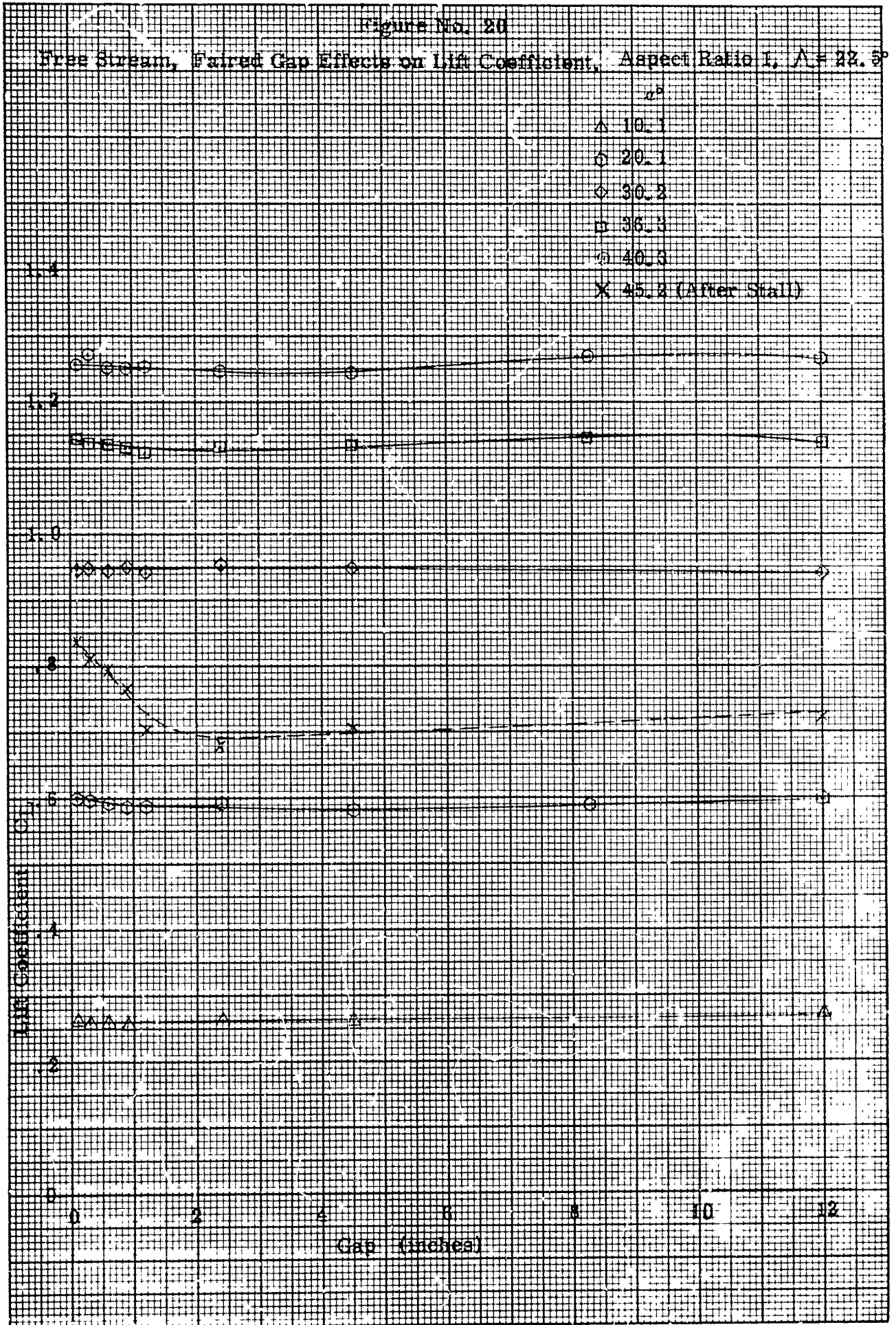
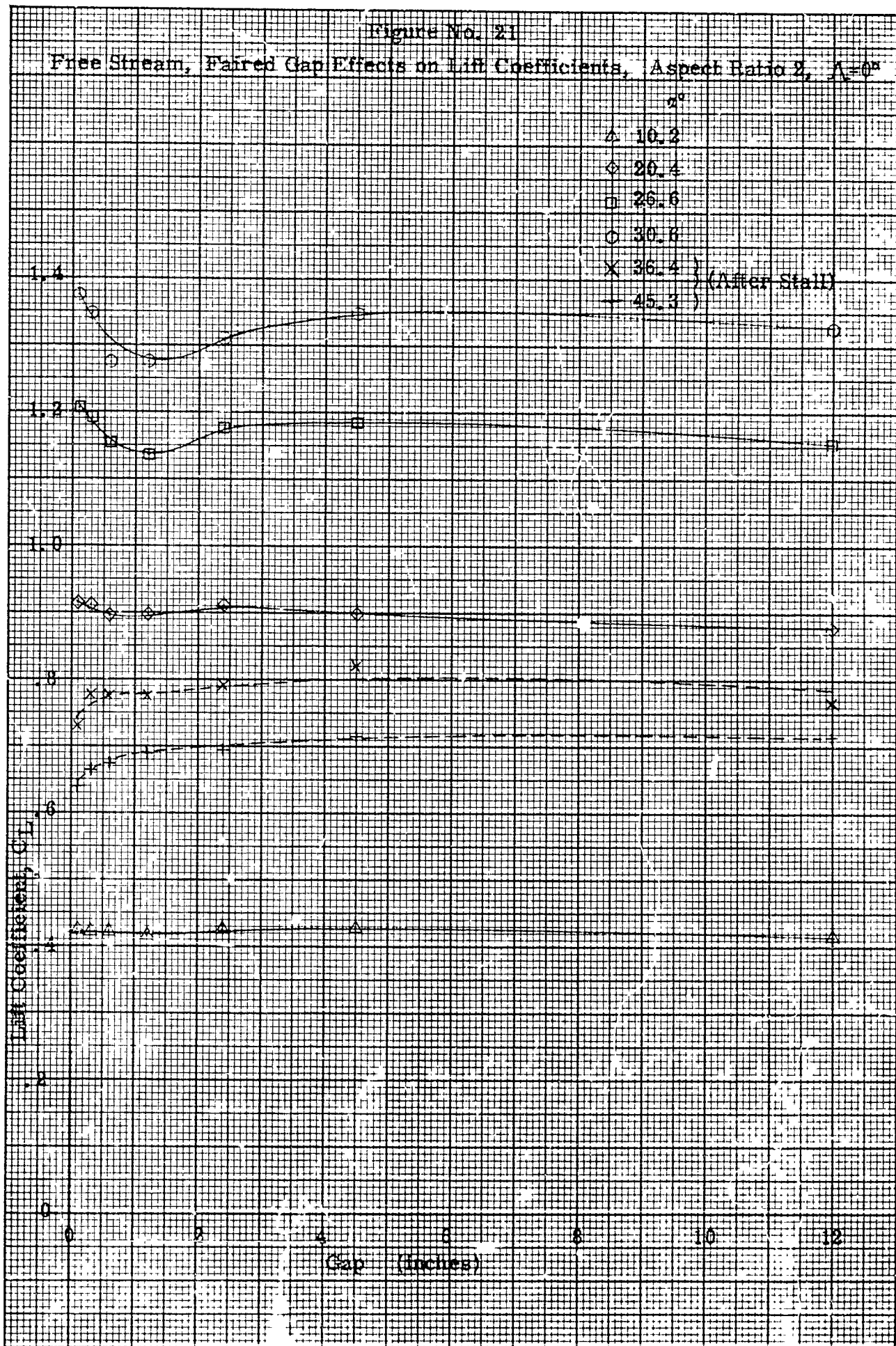


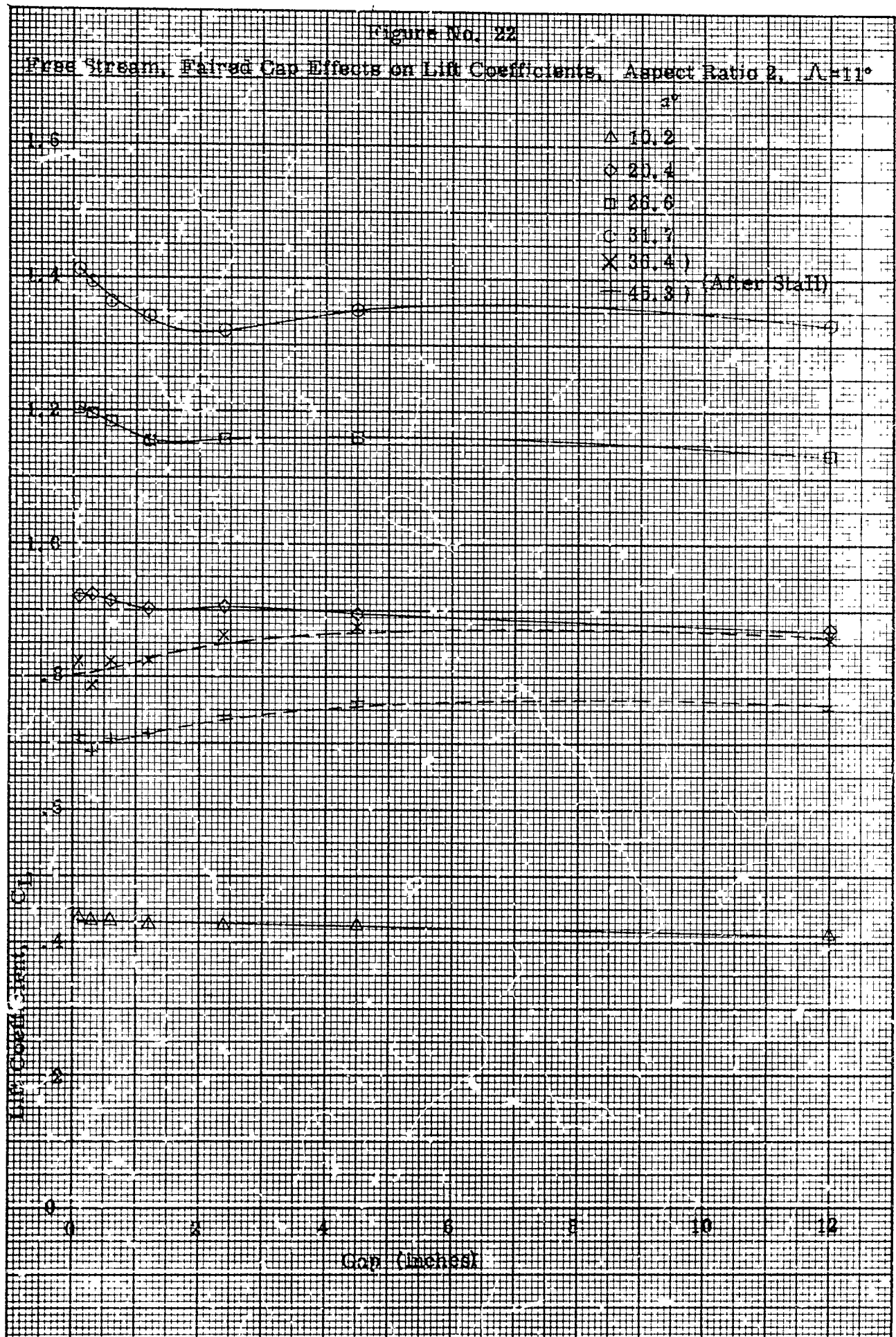
Figure No. 17. Propeller and Drive Motor Installed With Turning Vanes and Screen.

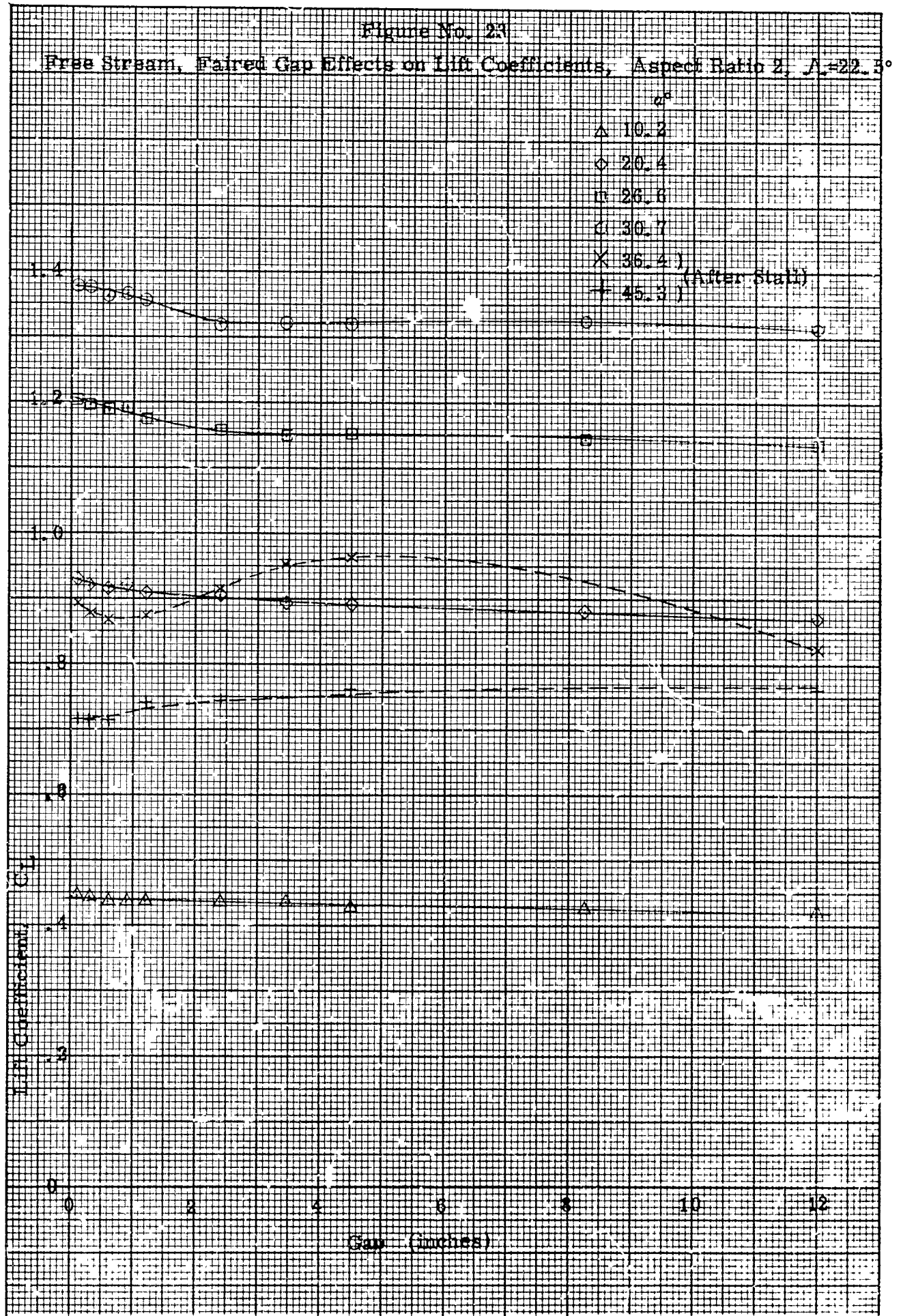




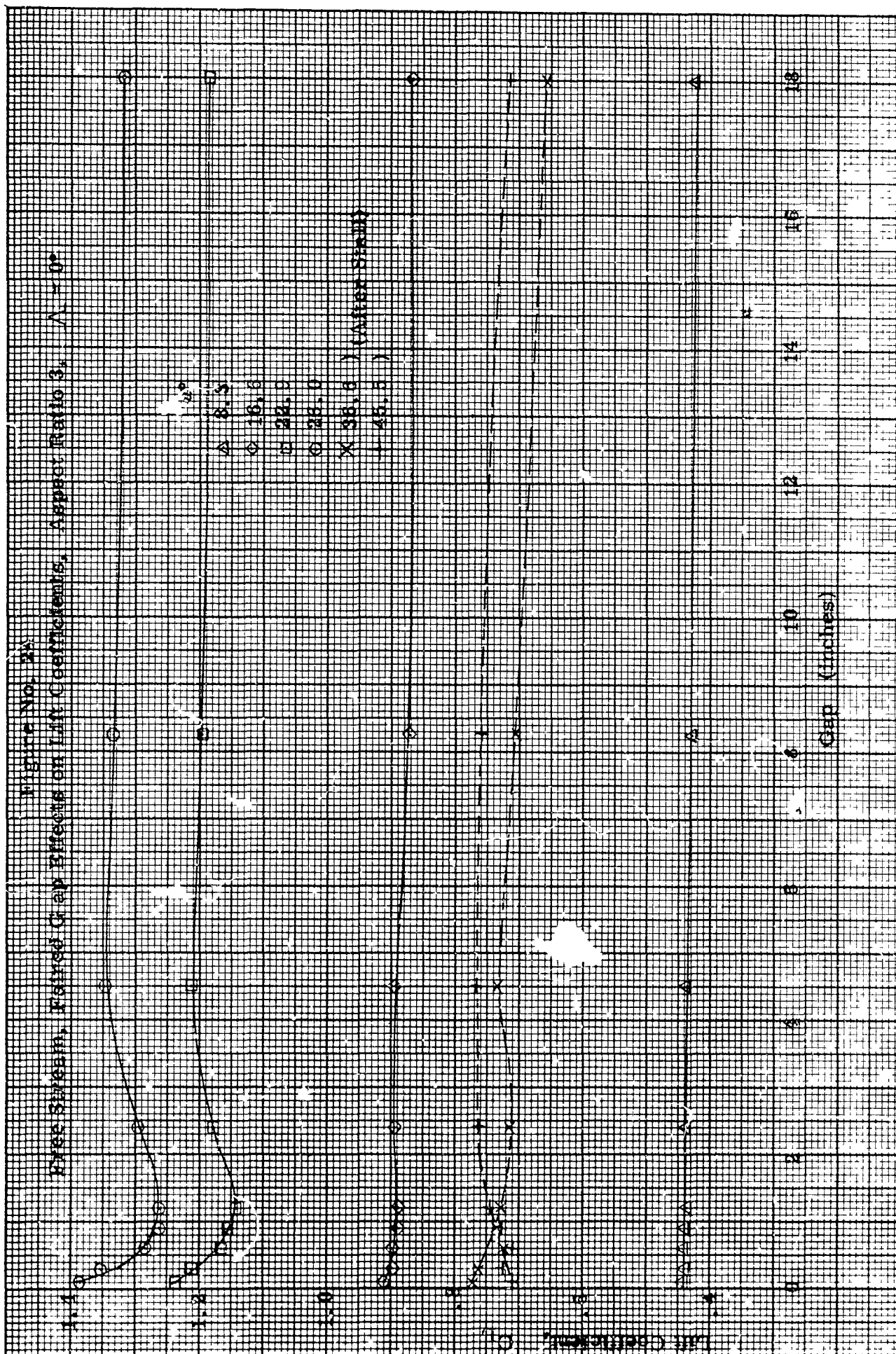


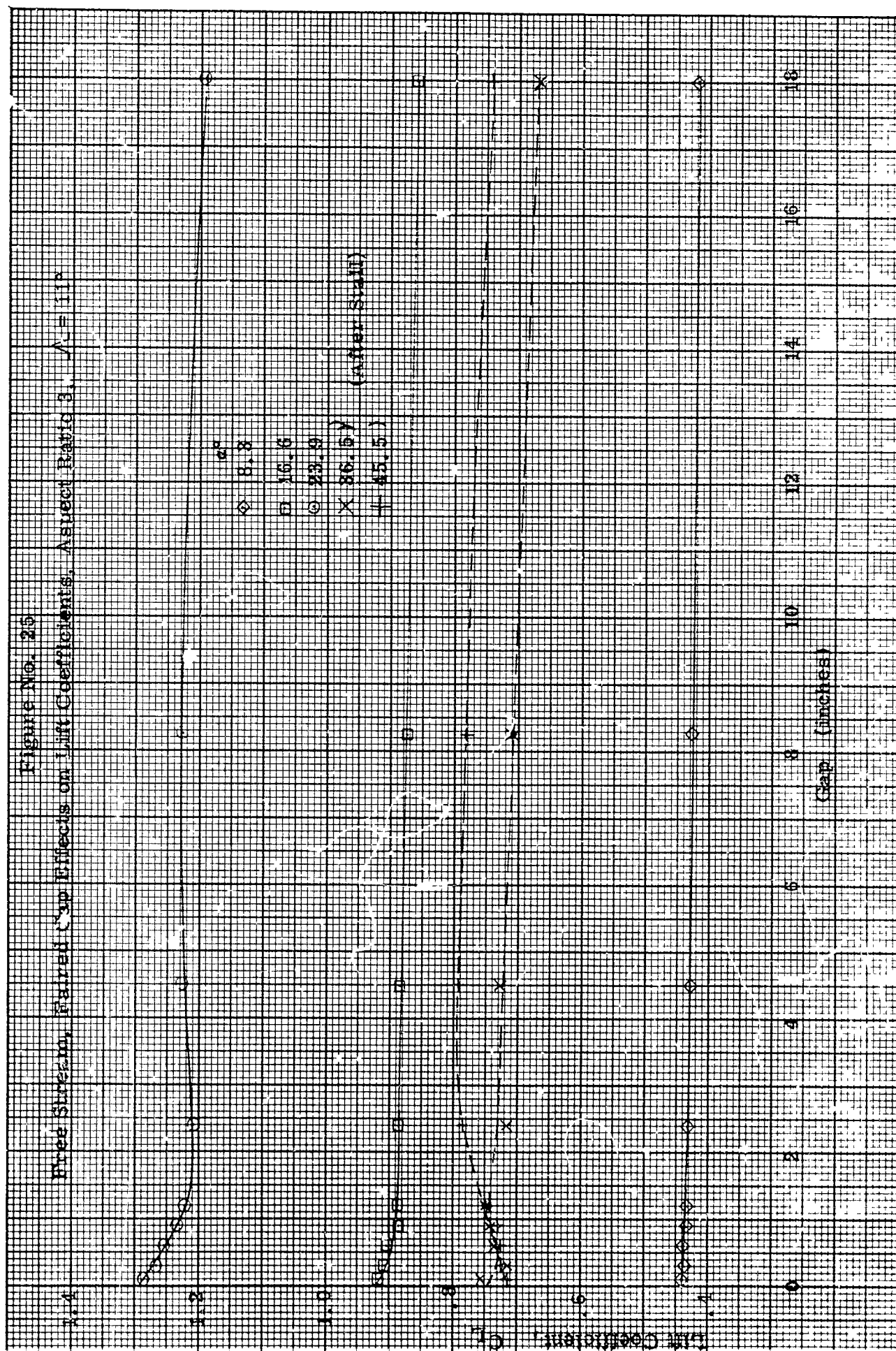


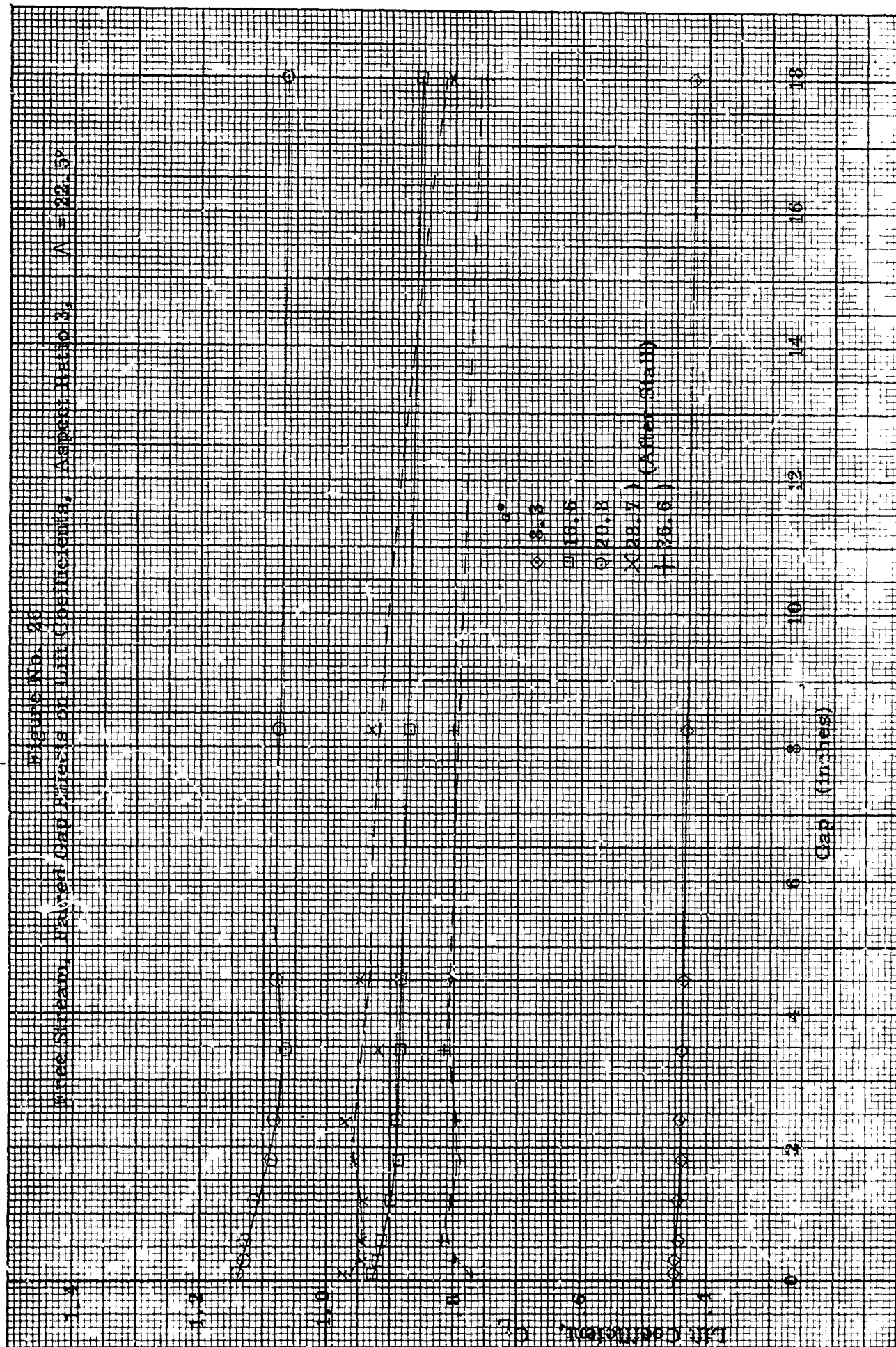


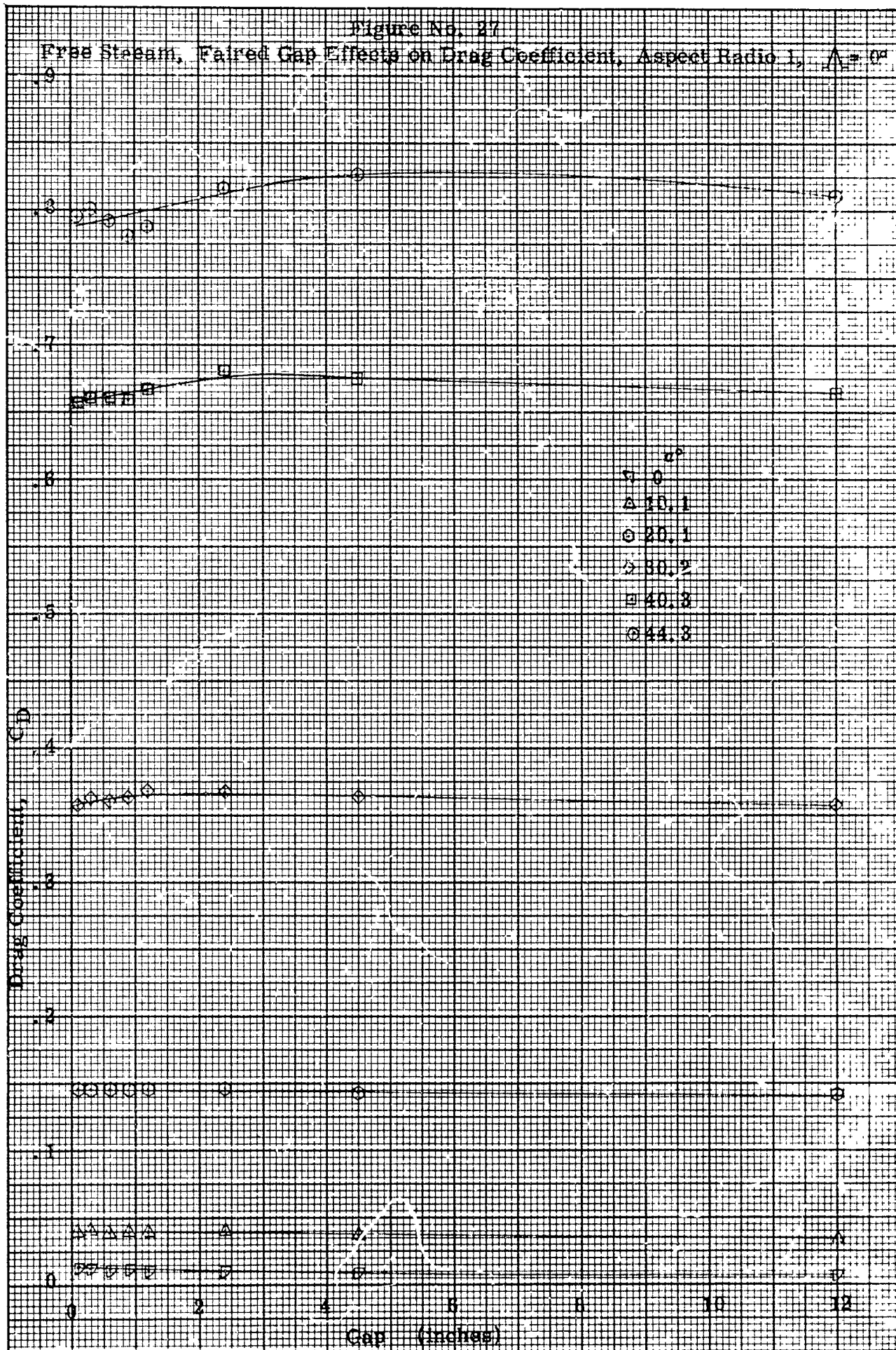


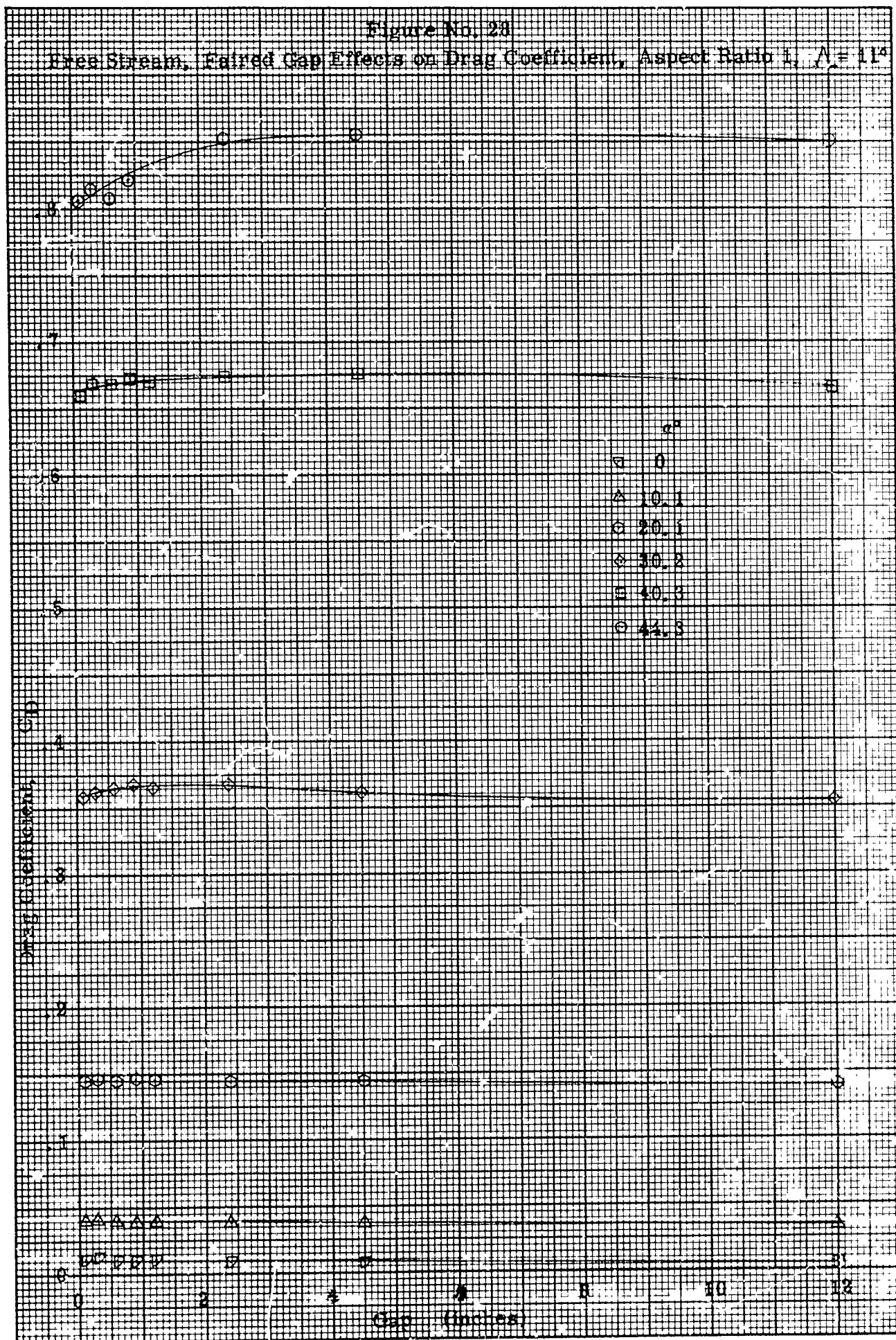
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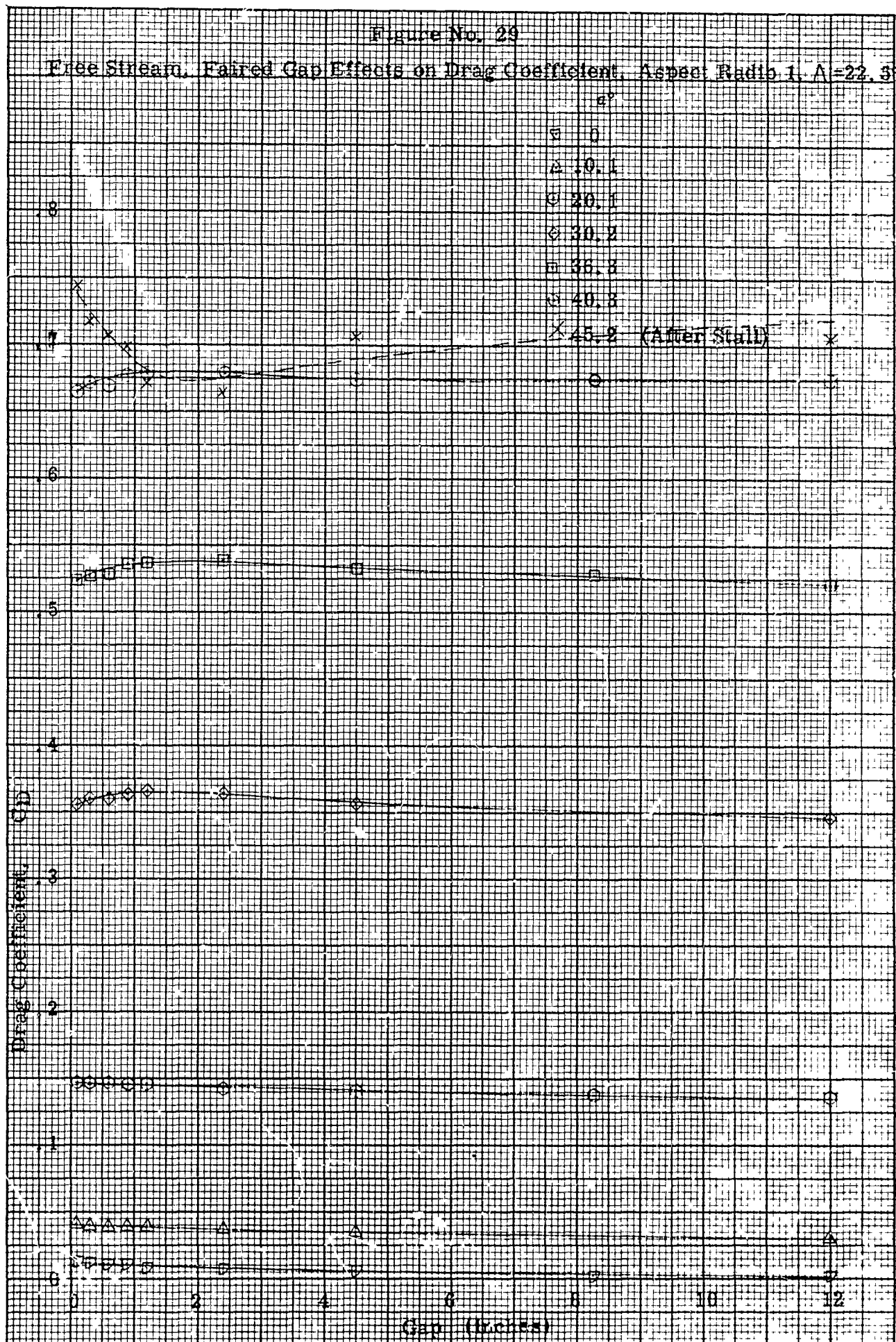


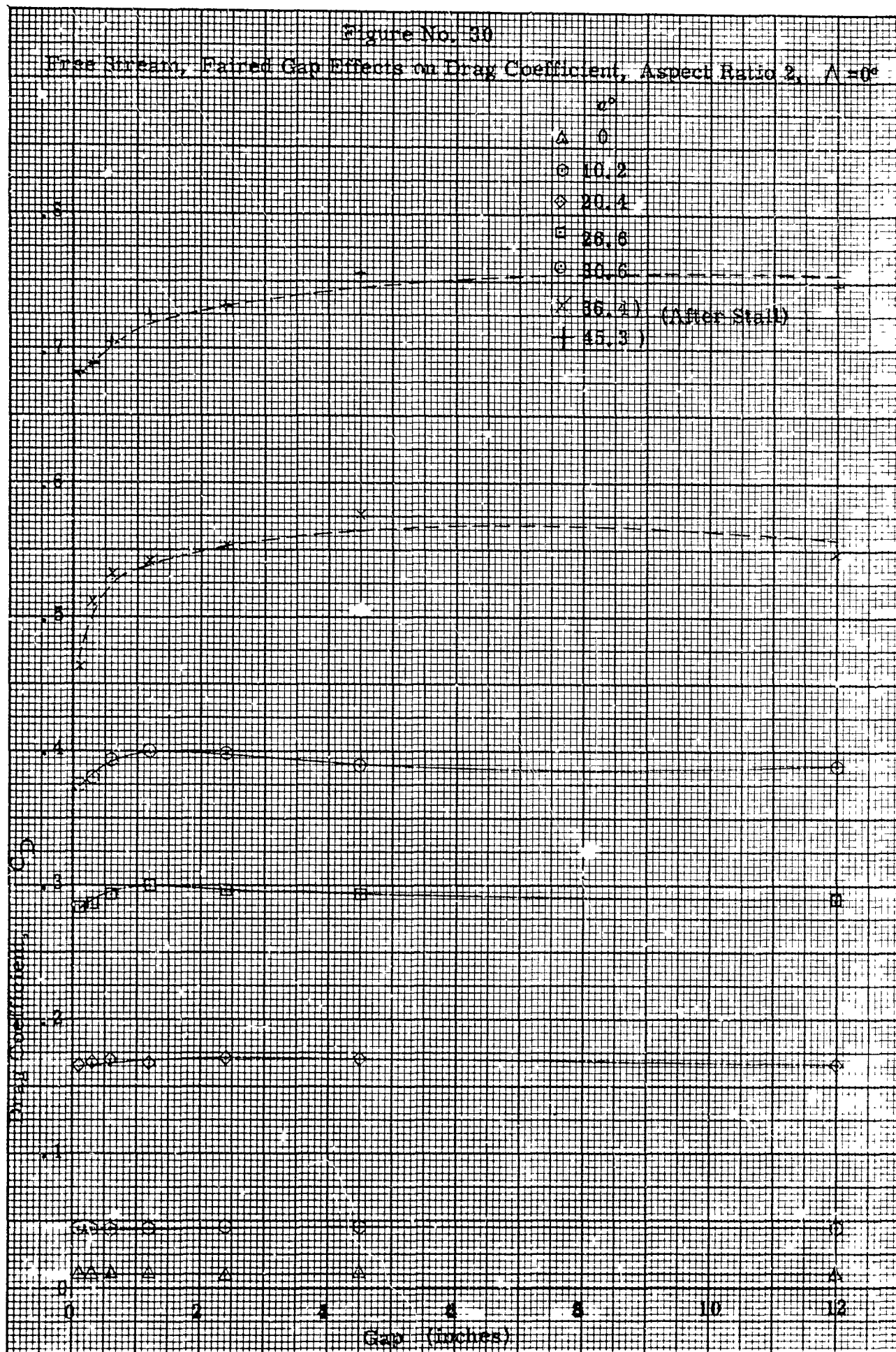




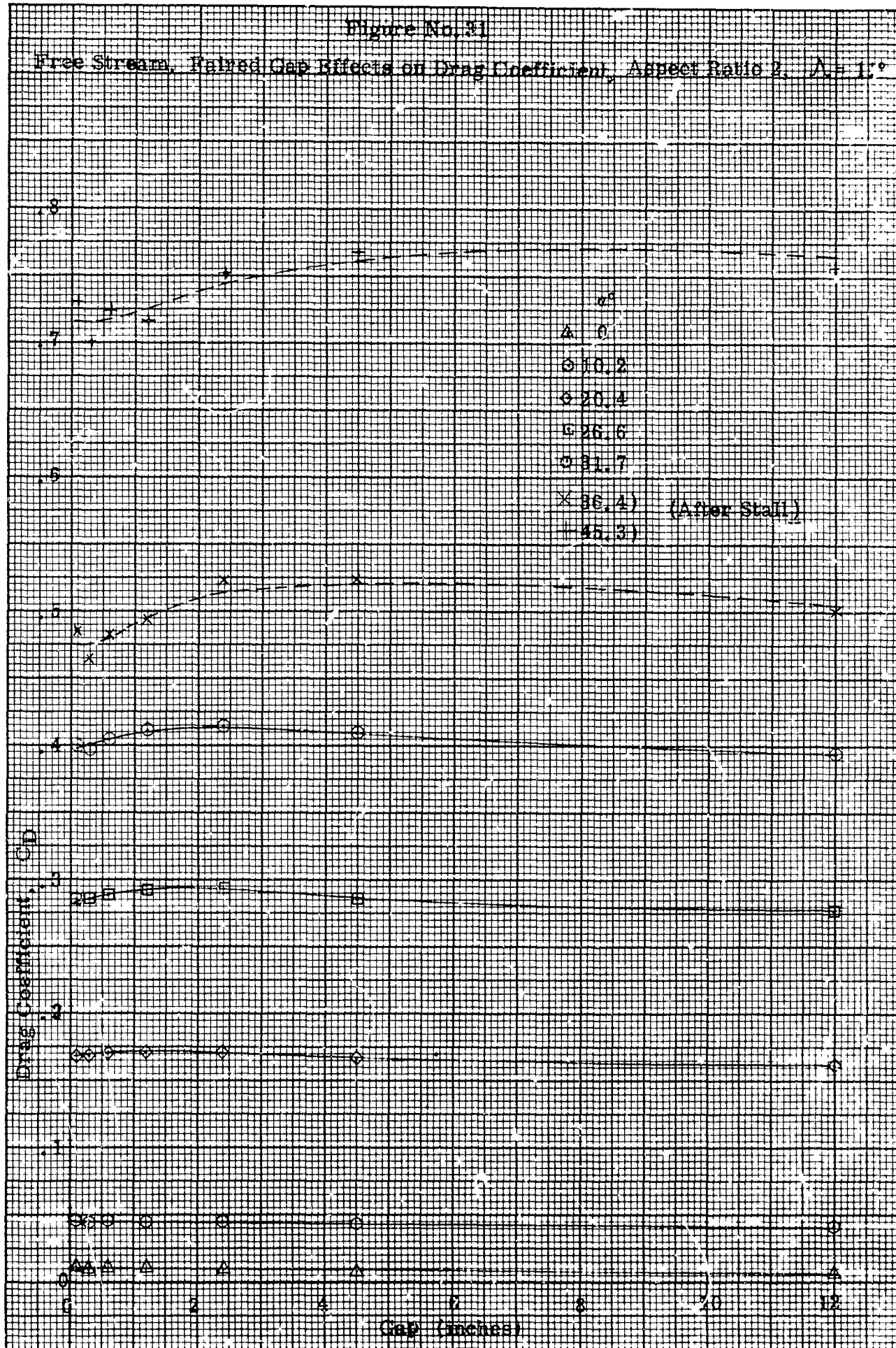




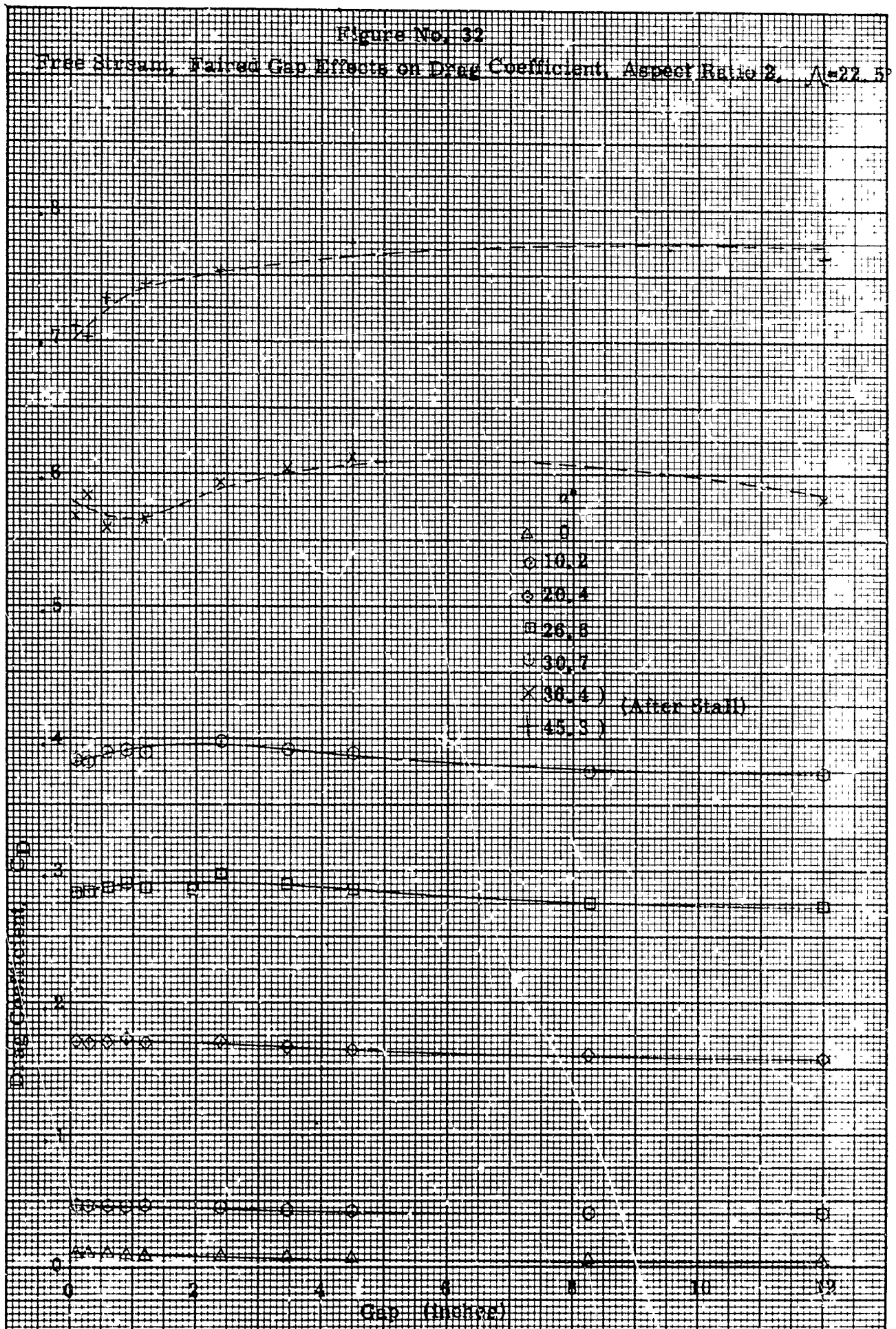


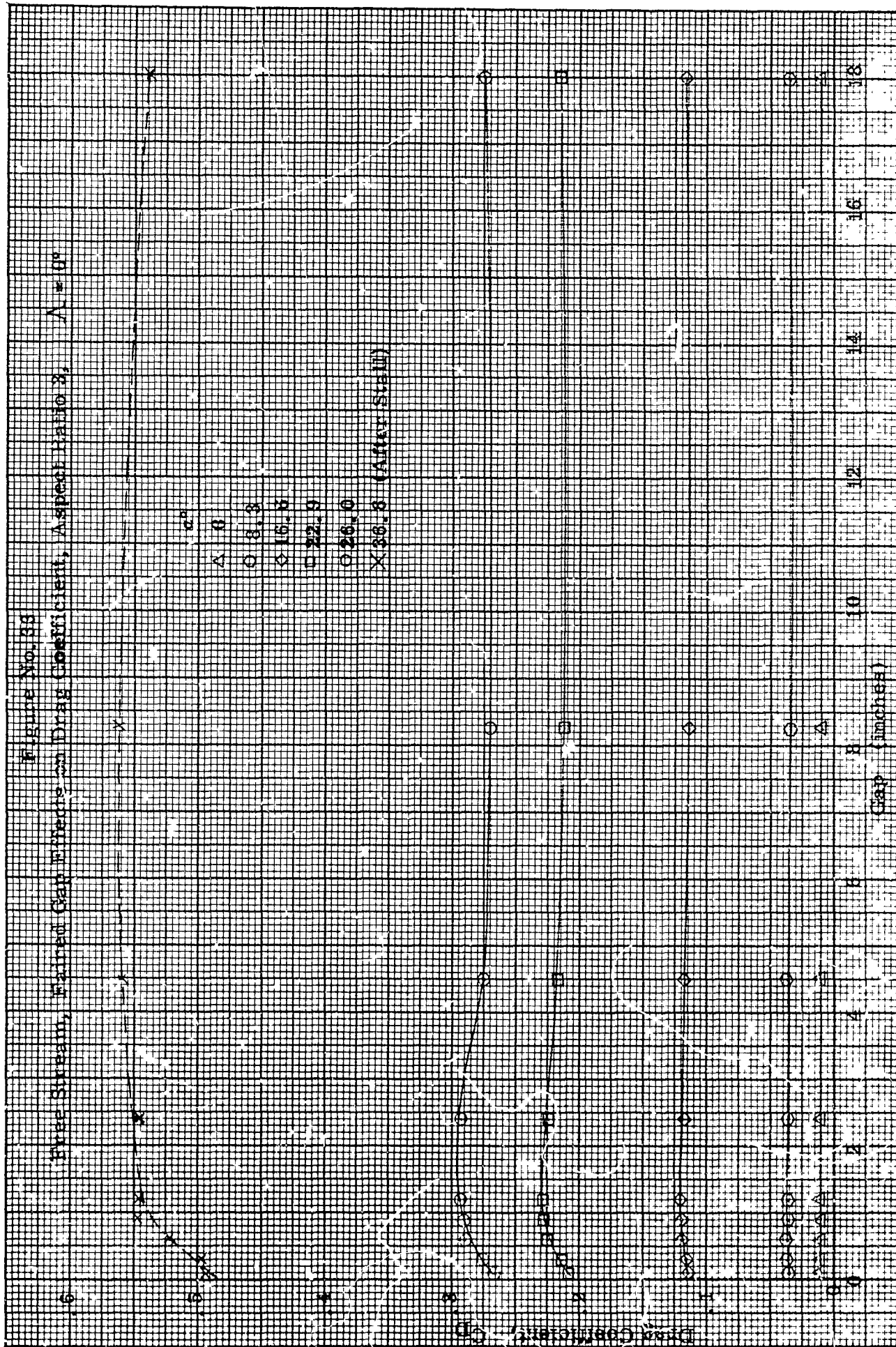


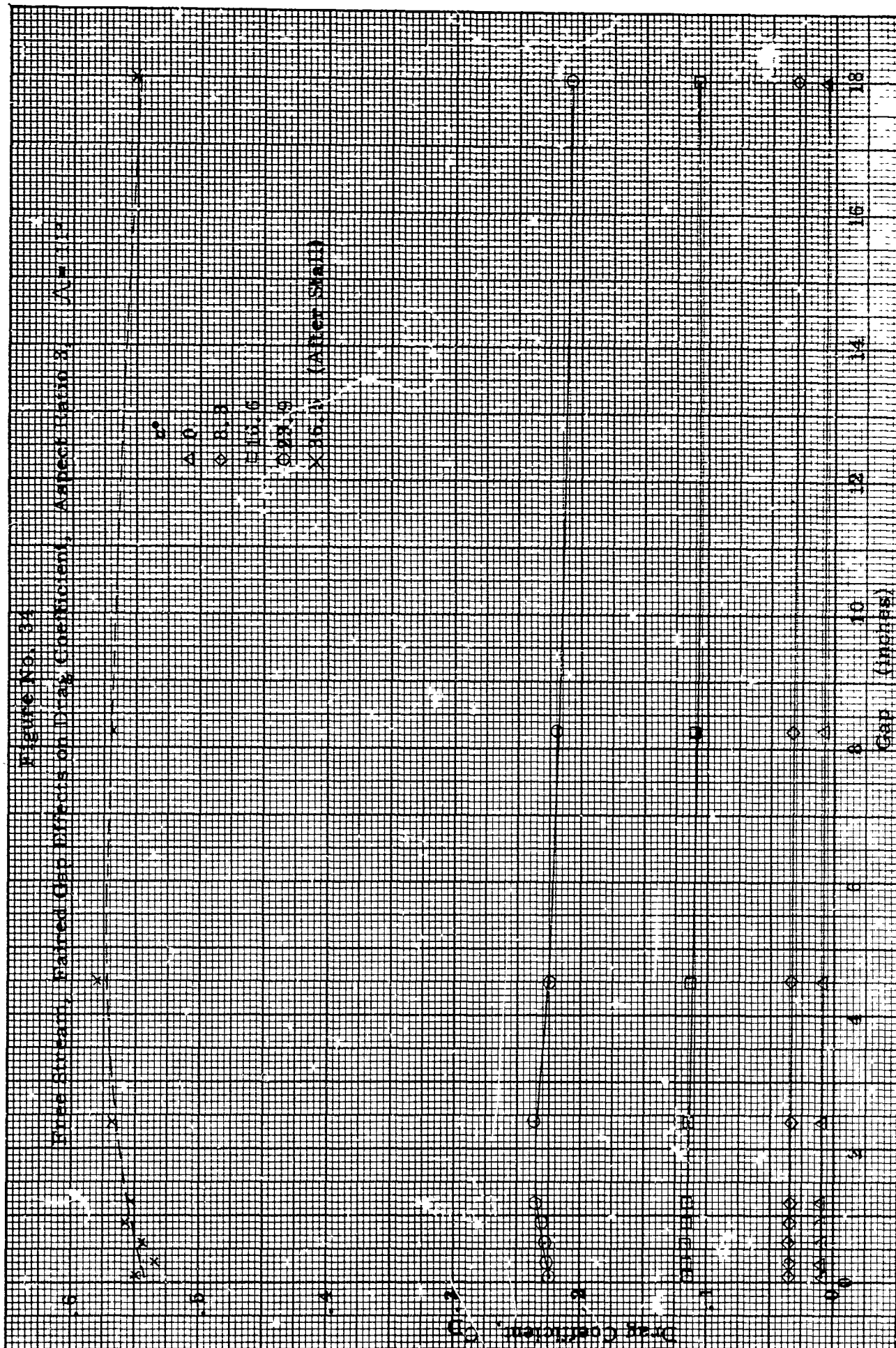
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Figure No. 36
 Free Stream, Filled Gap Effects on Chordwise Center of Pressure
 Aspect Ratio 1, $\Lambda = 0^\circ$

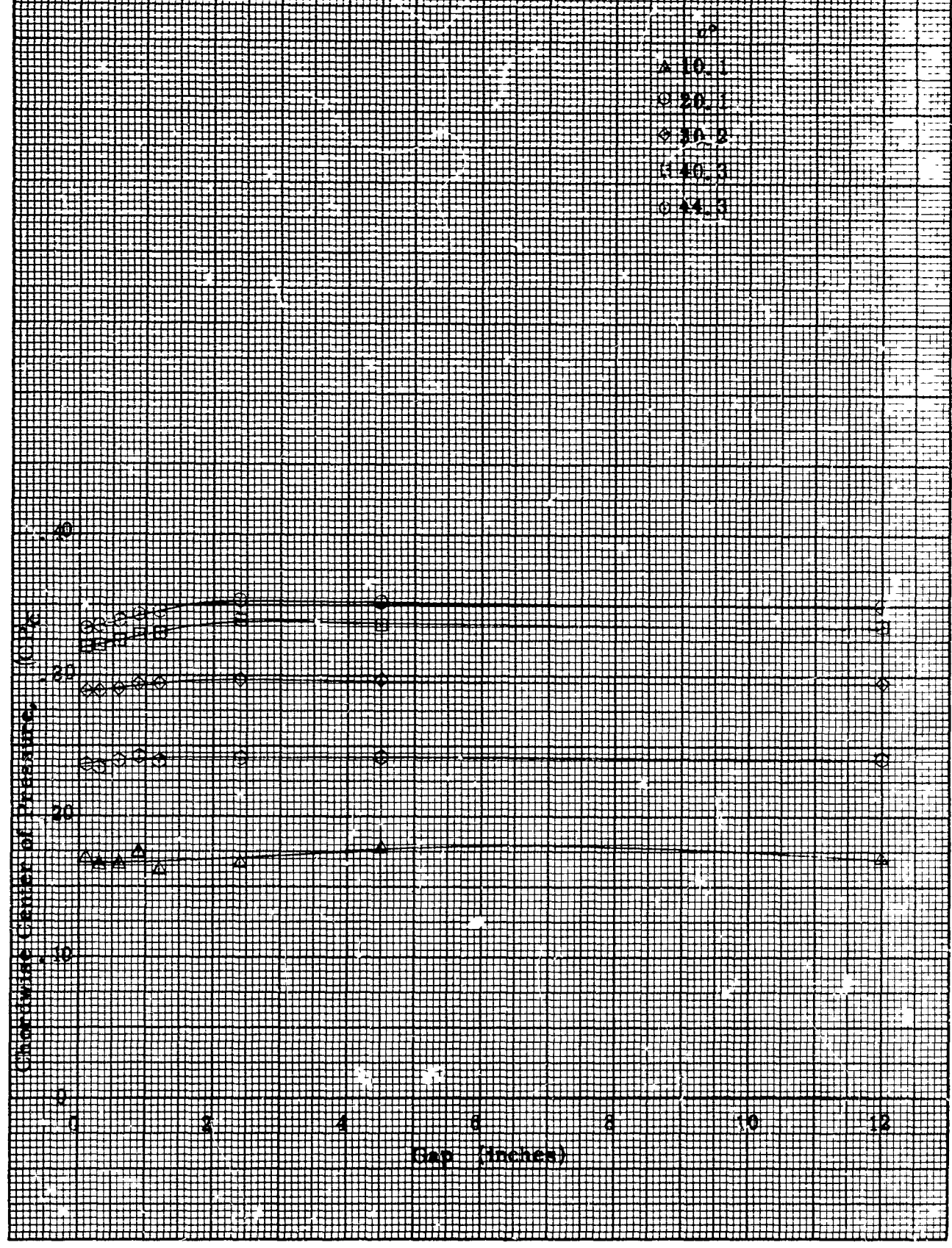
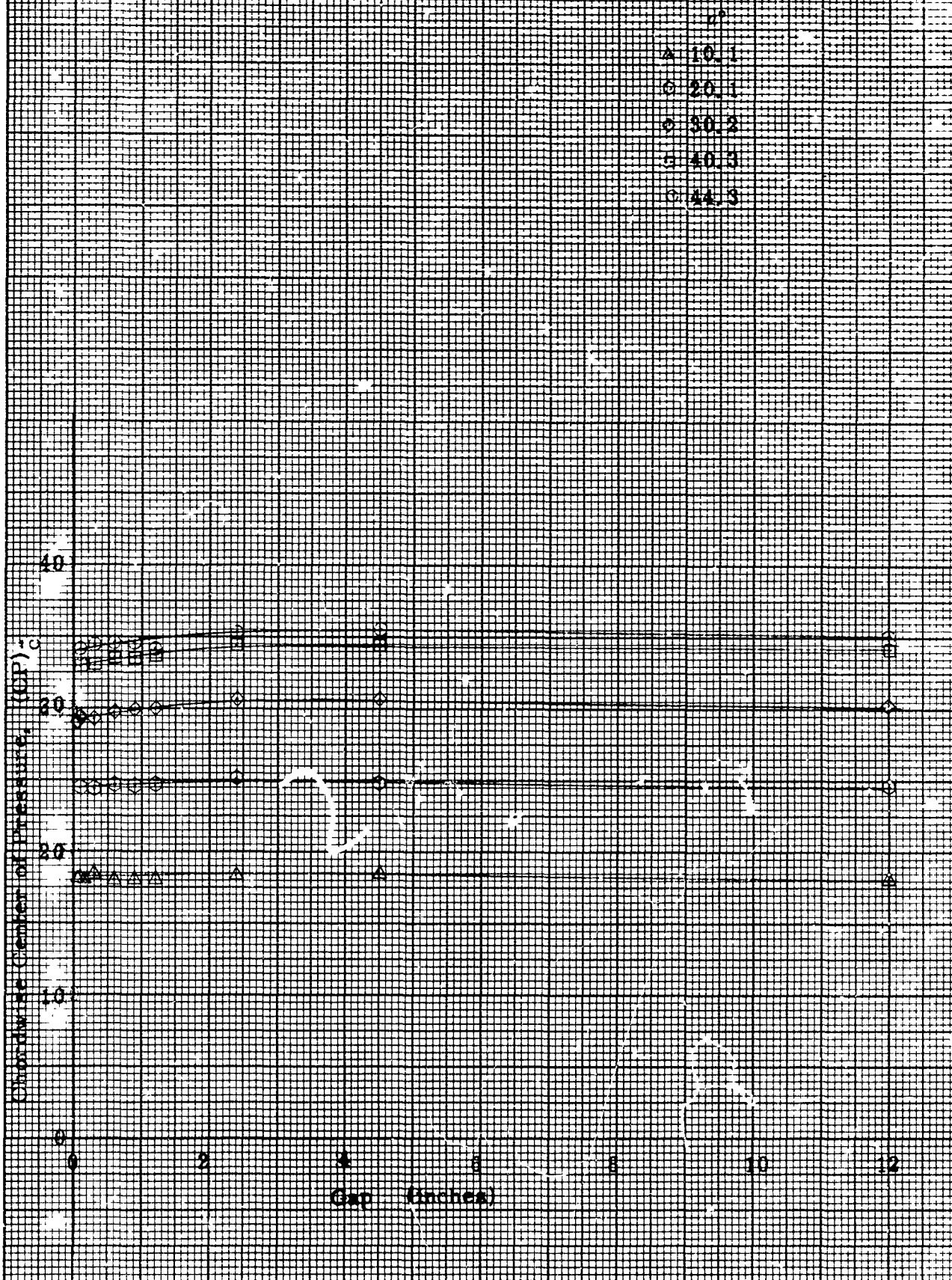
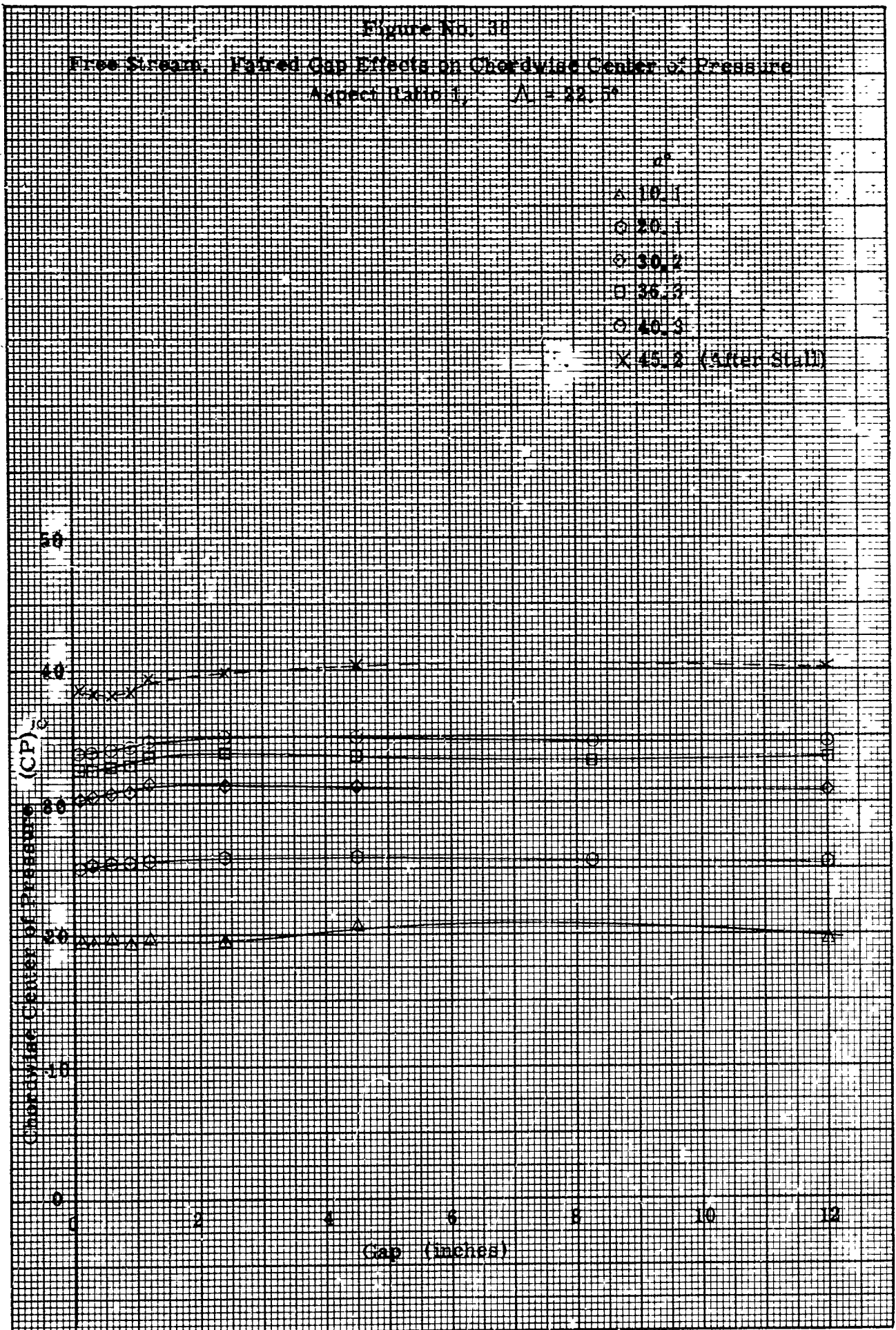
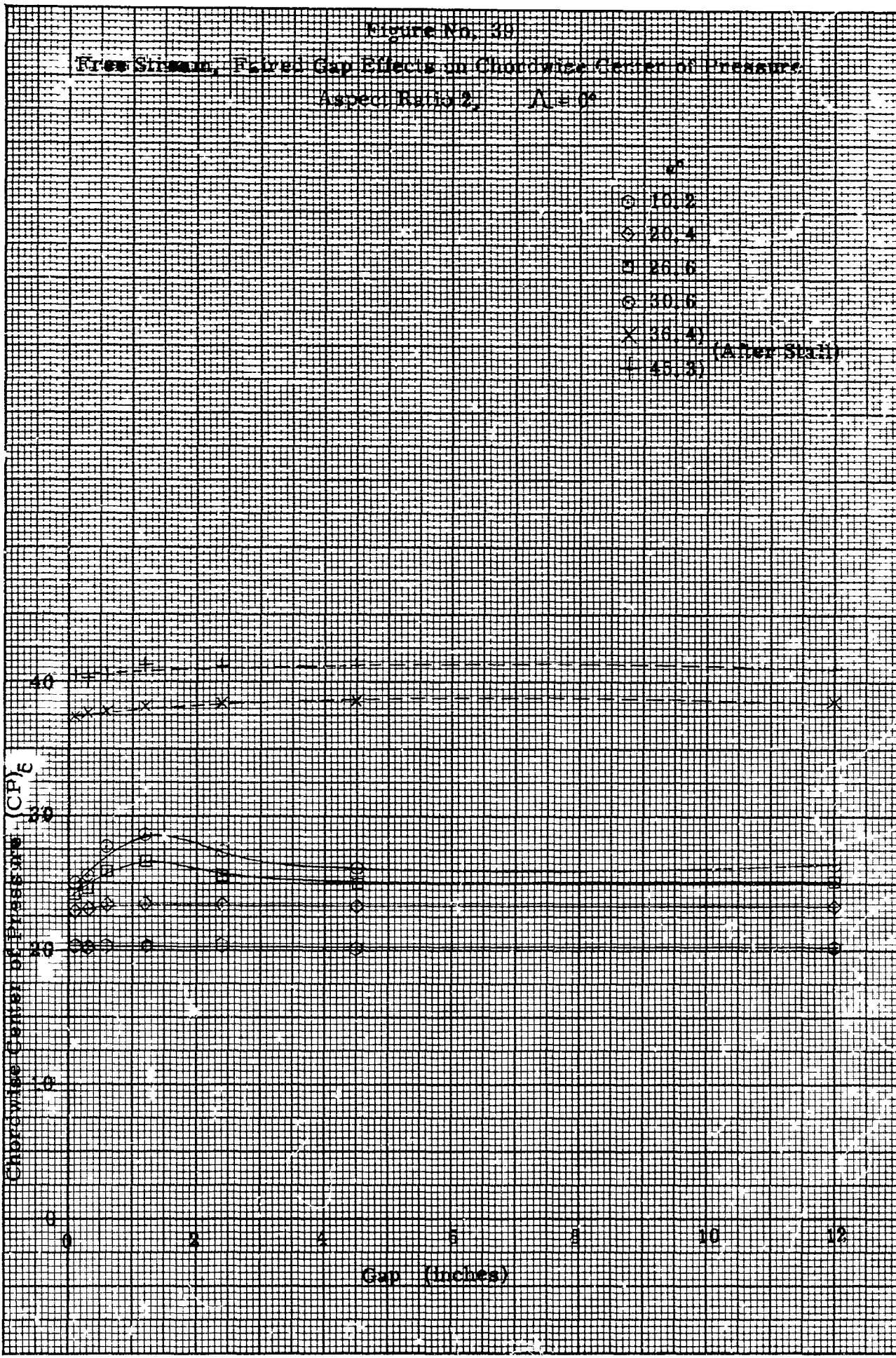


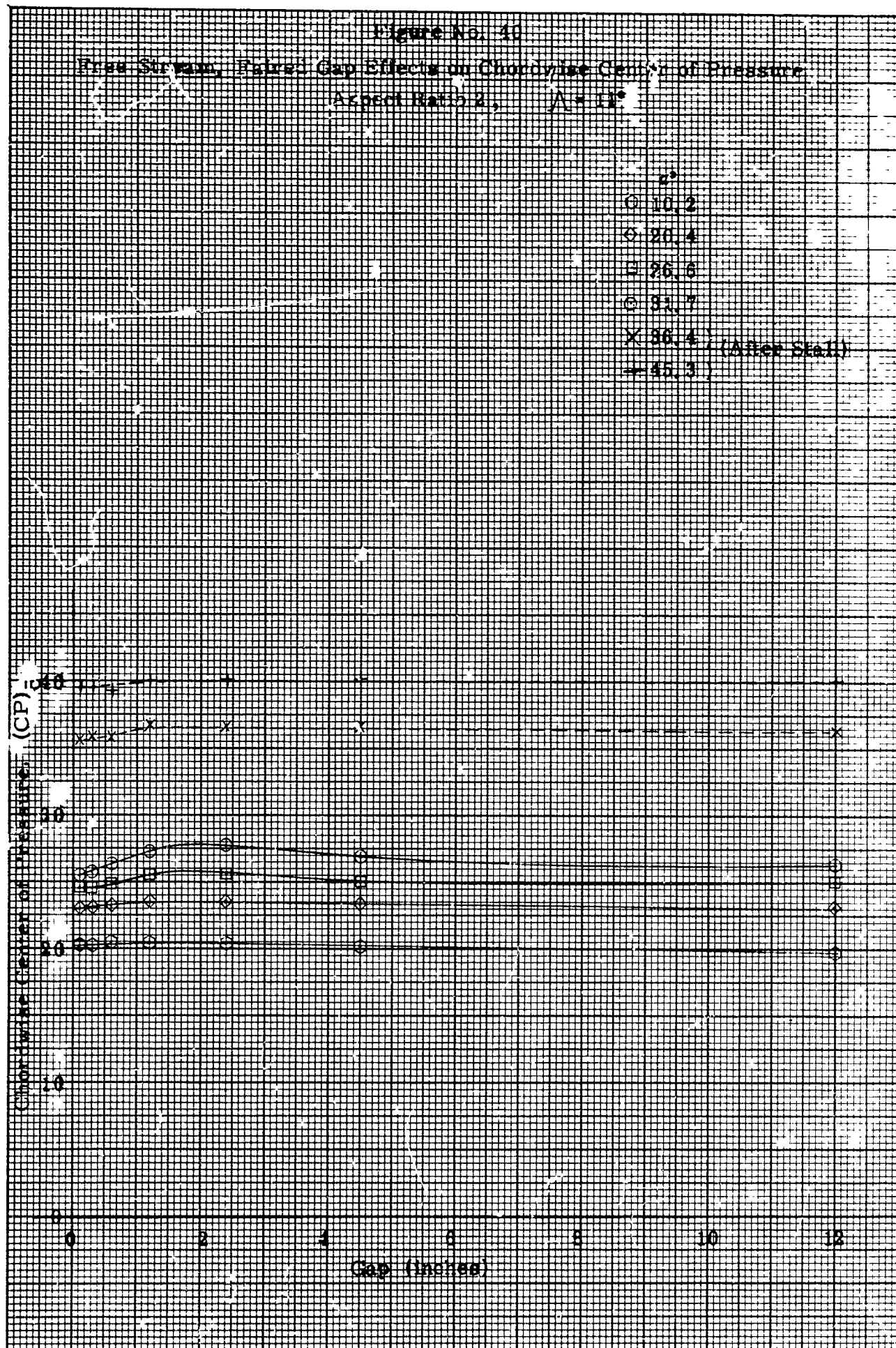
Figure No. 37

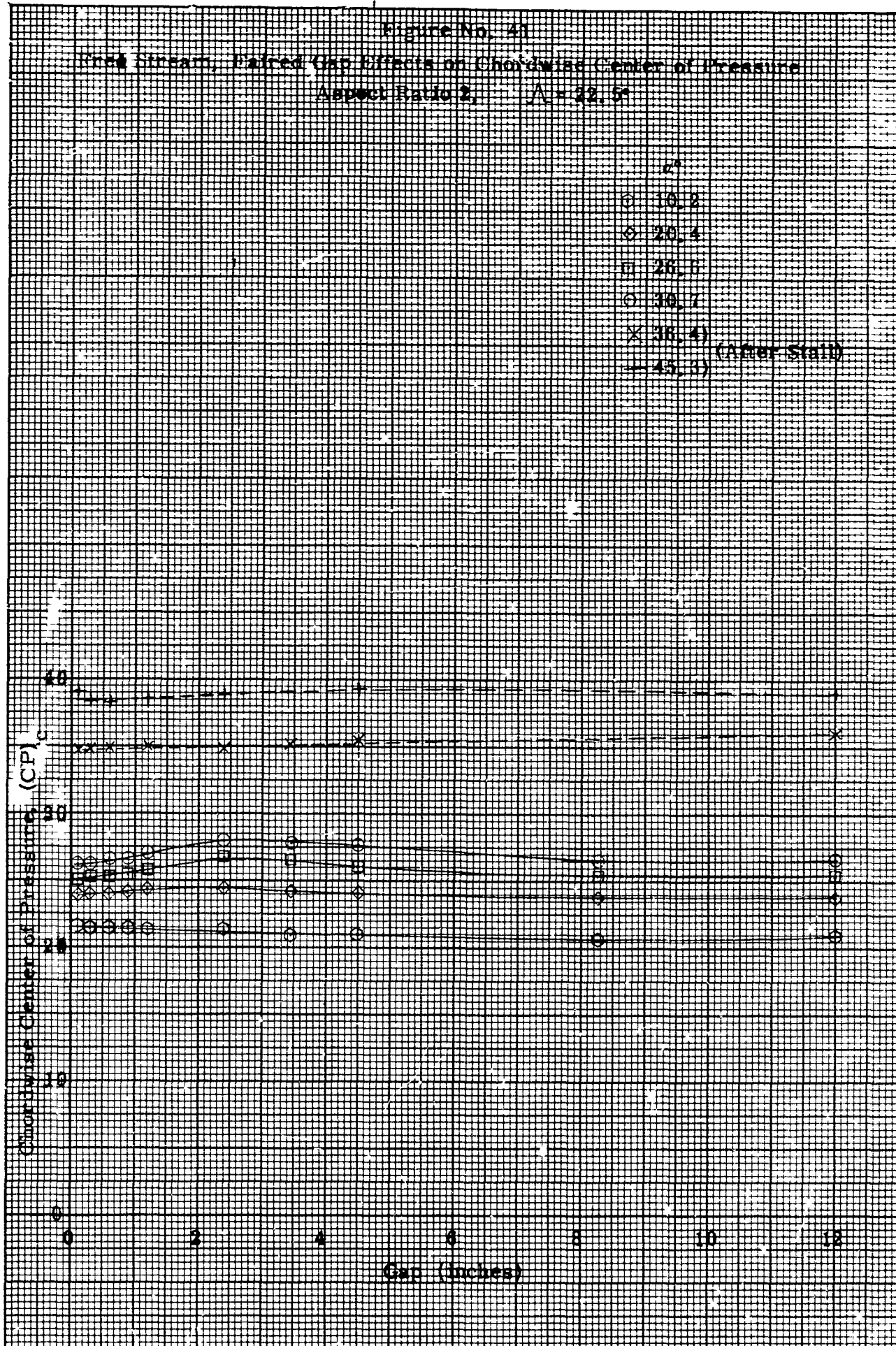
Free Stream, Fairer Gap Effects on Chordwise Center of Pressure
Aspect Ratio 1, $\Lambda = 10^\circ$

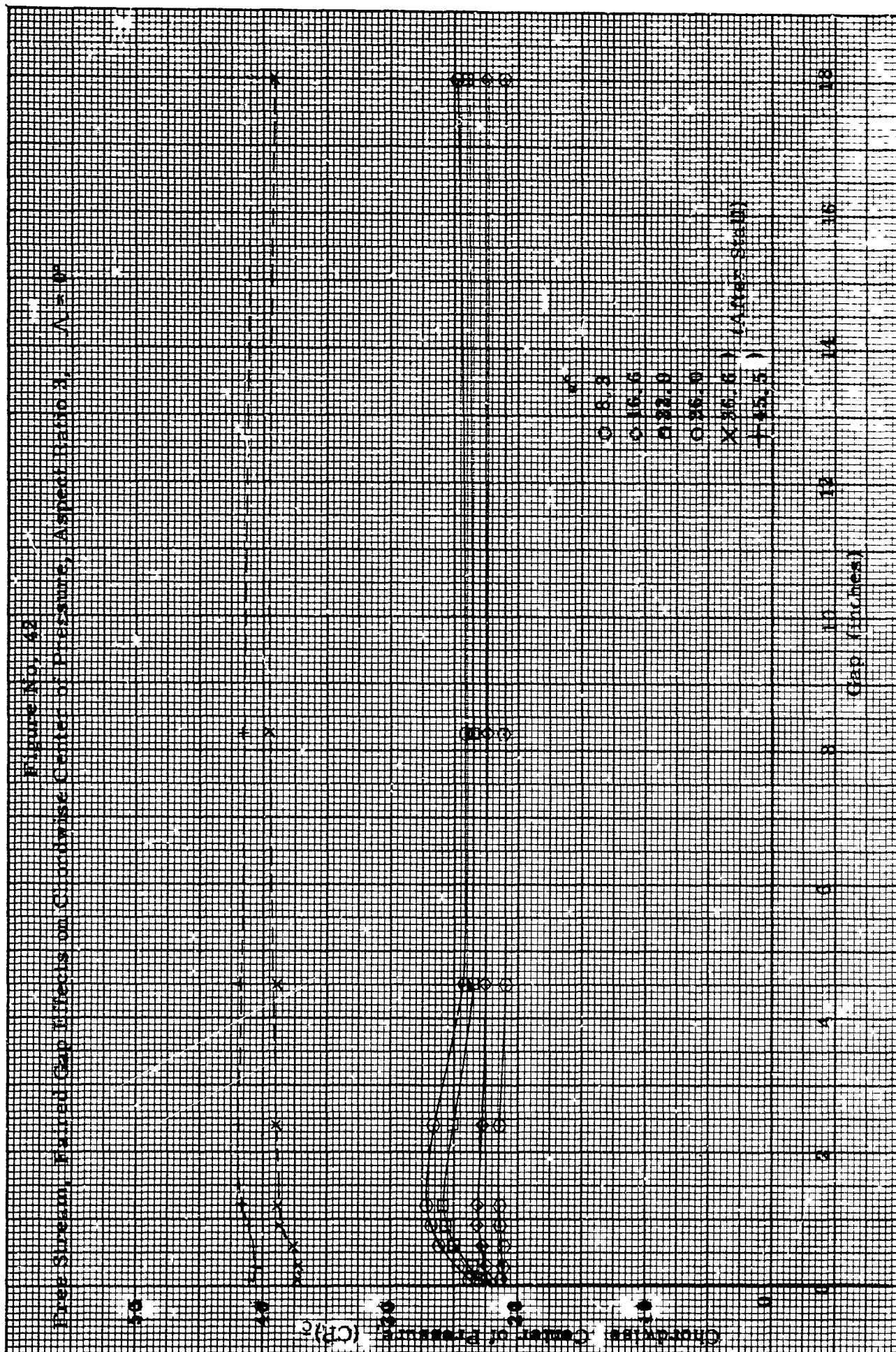


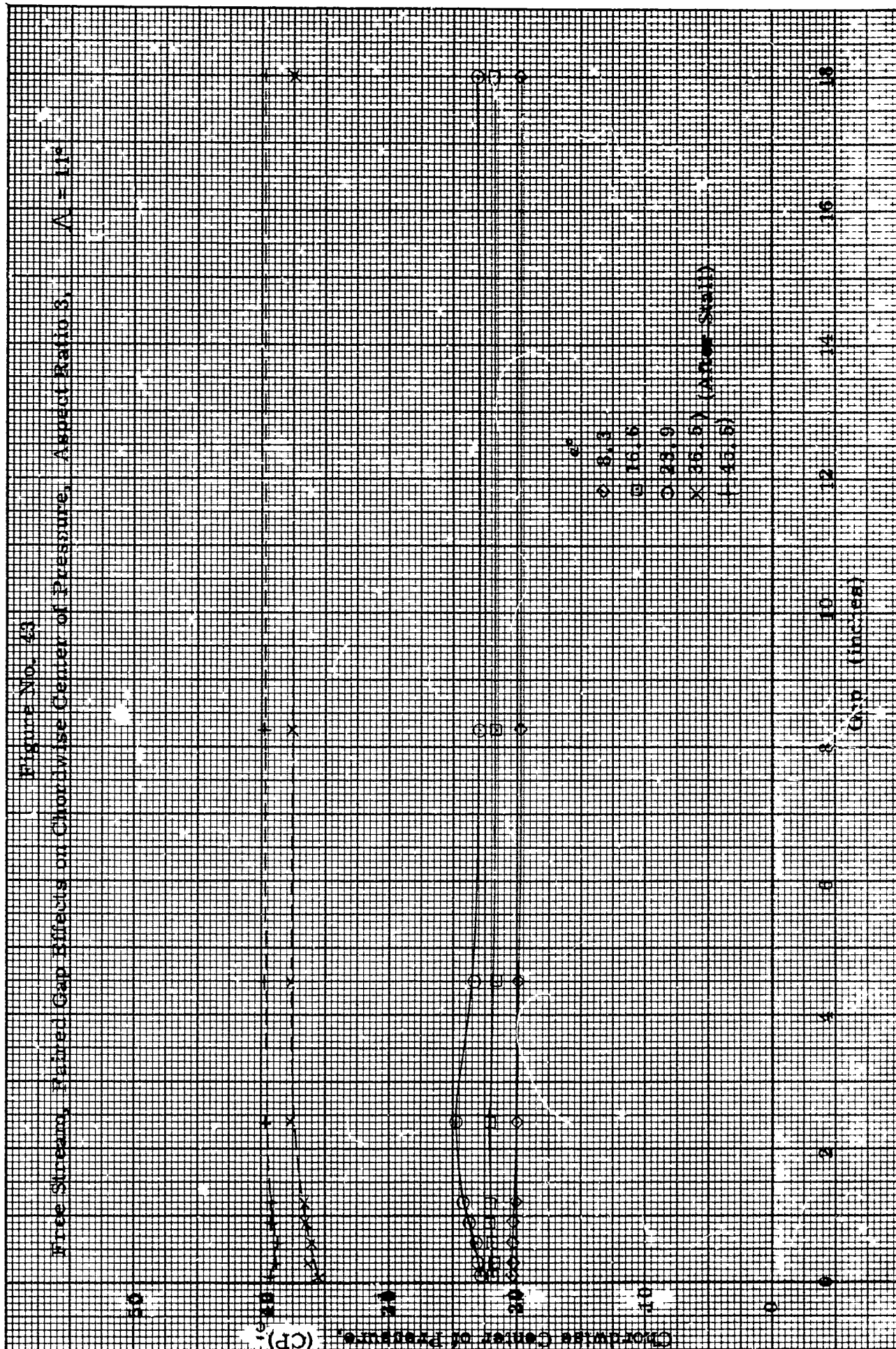


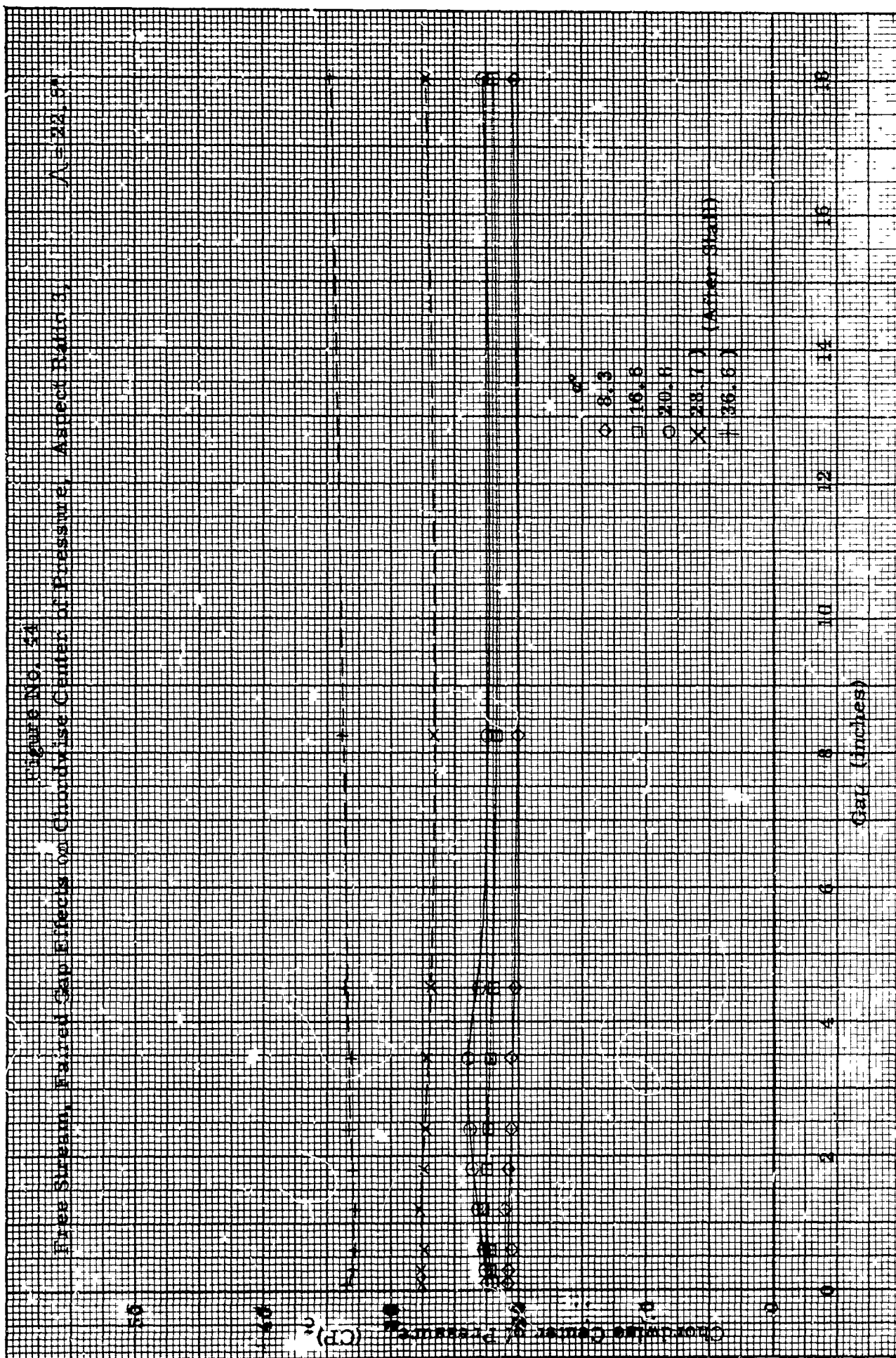


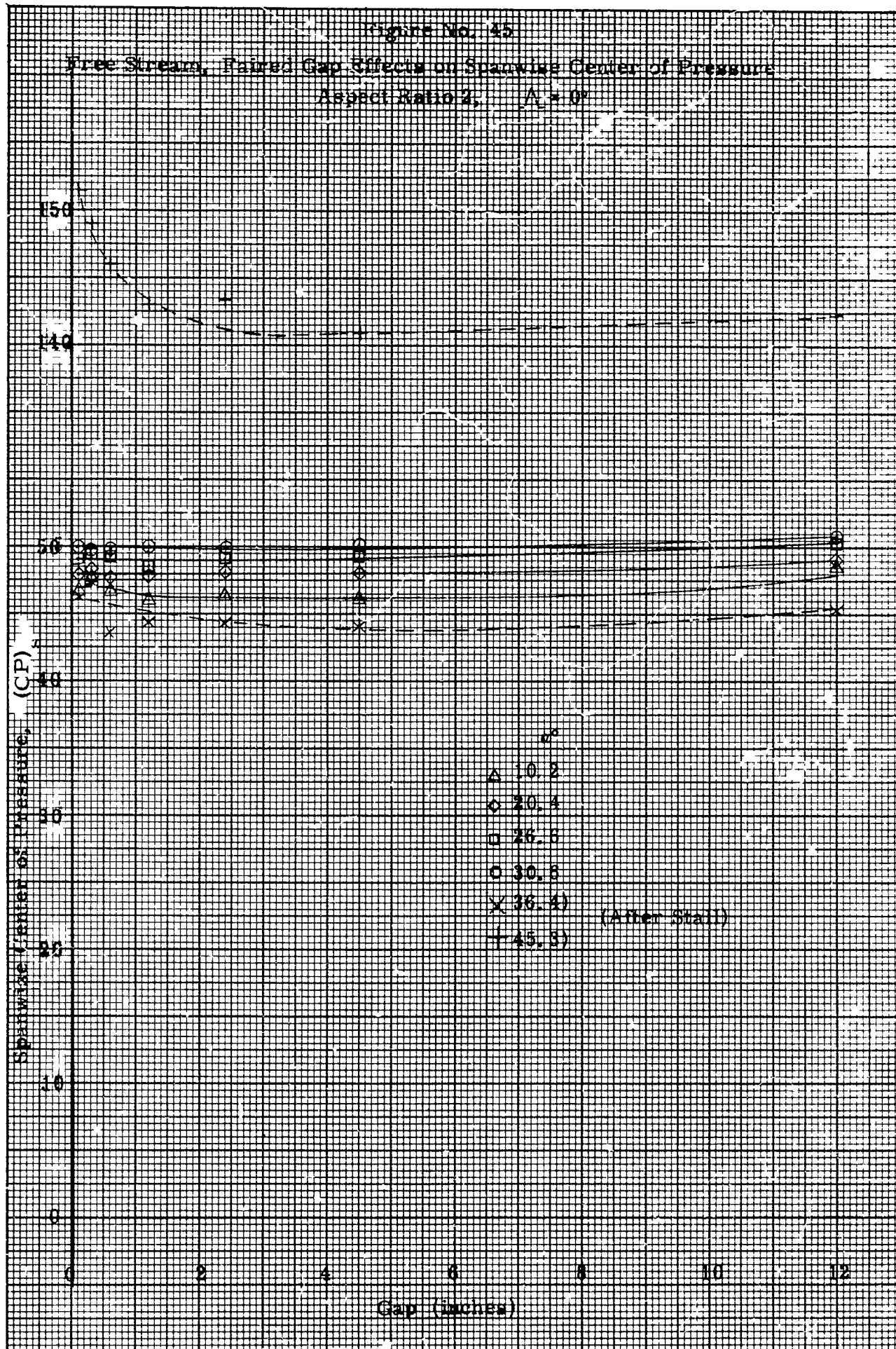












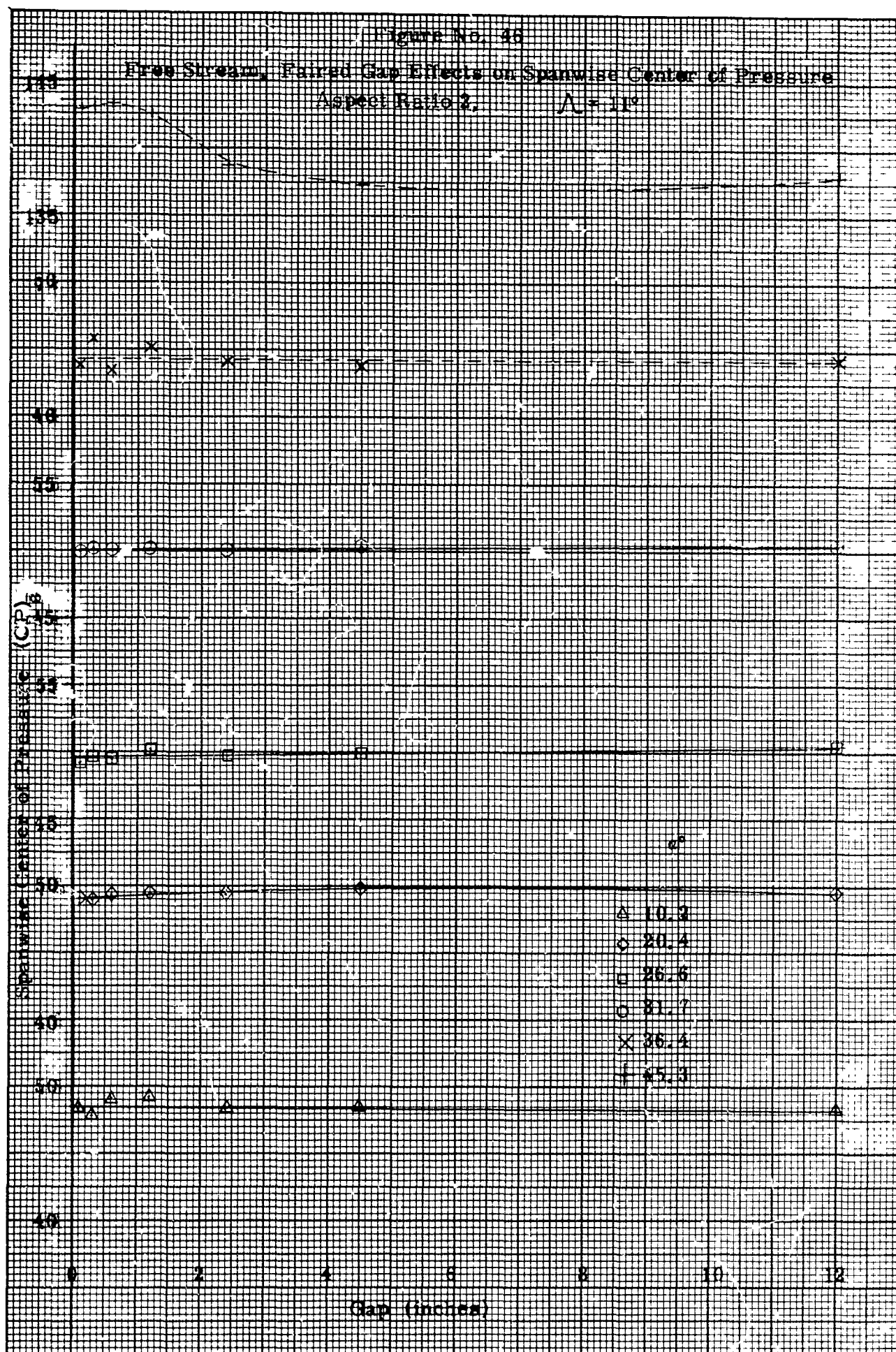
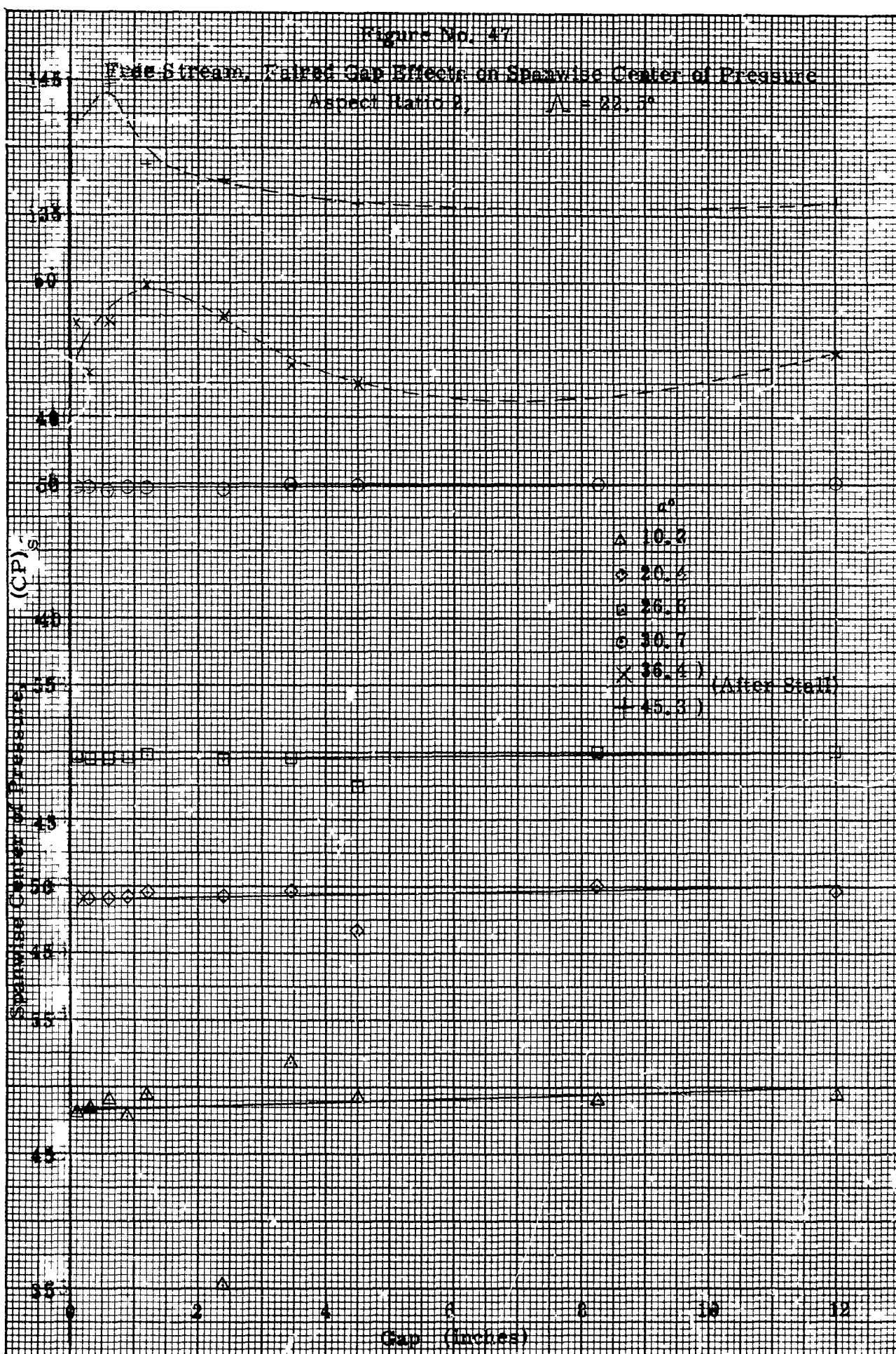


Figure No. 47

Free-Stream, Filled Gap Effects on Spanwise Center of Pressure
Aspect Ratio 2, $\Lambda = 20.5^\circ$



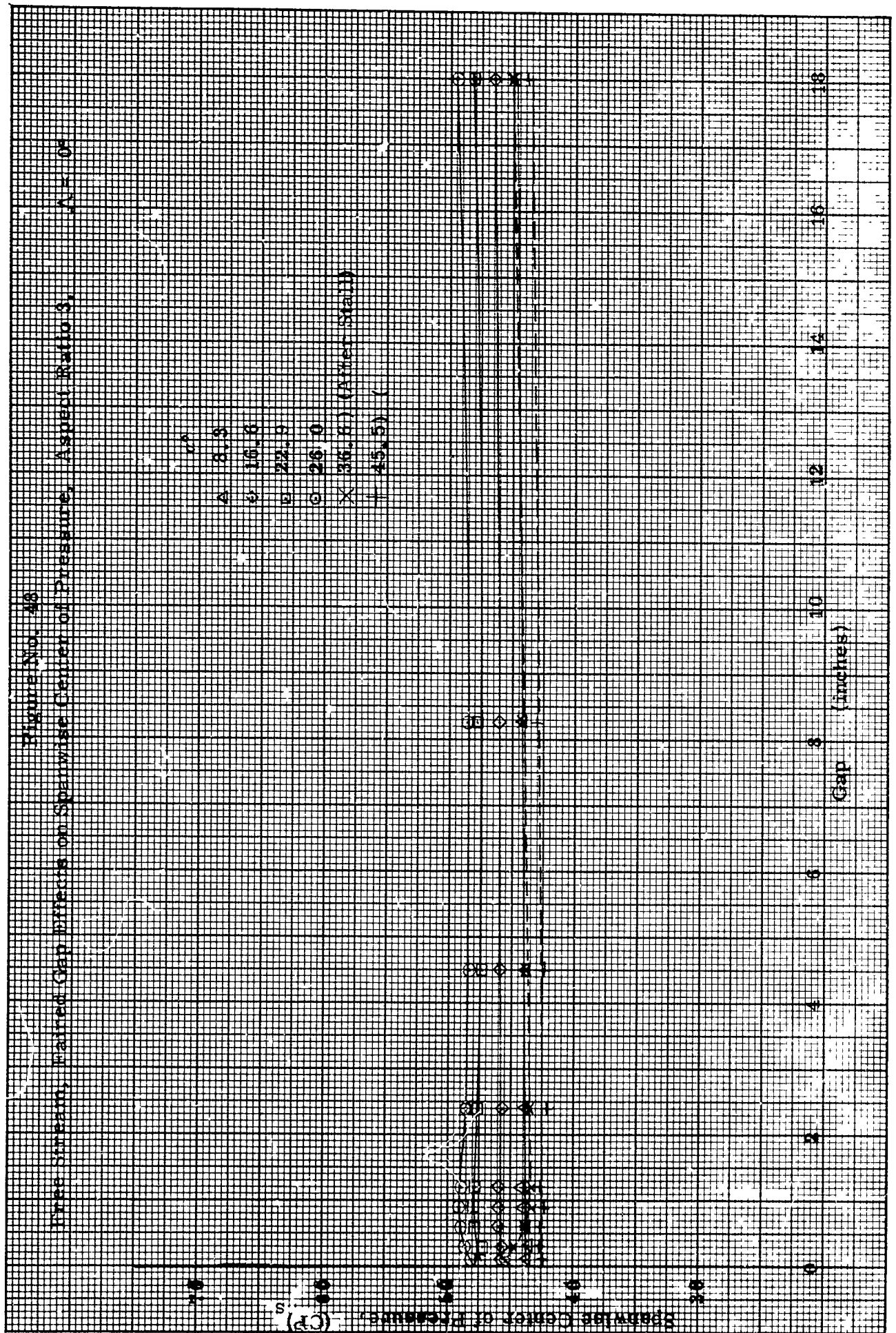
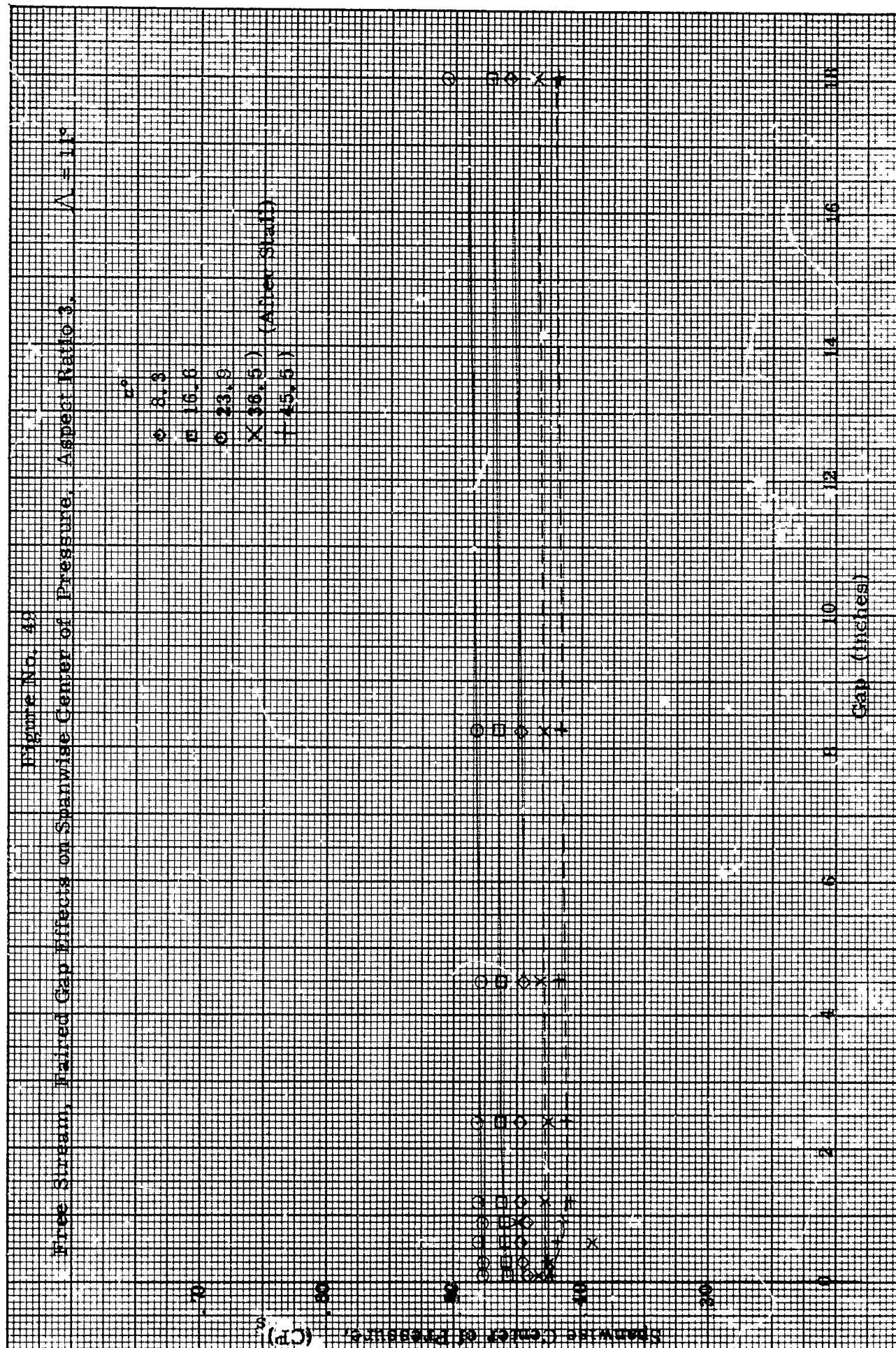
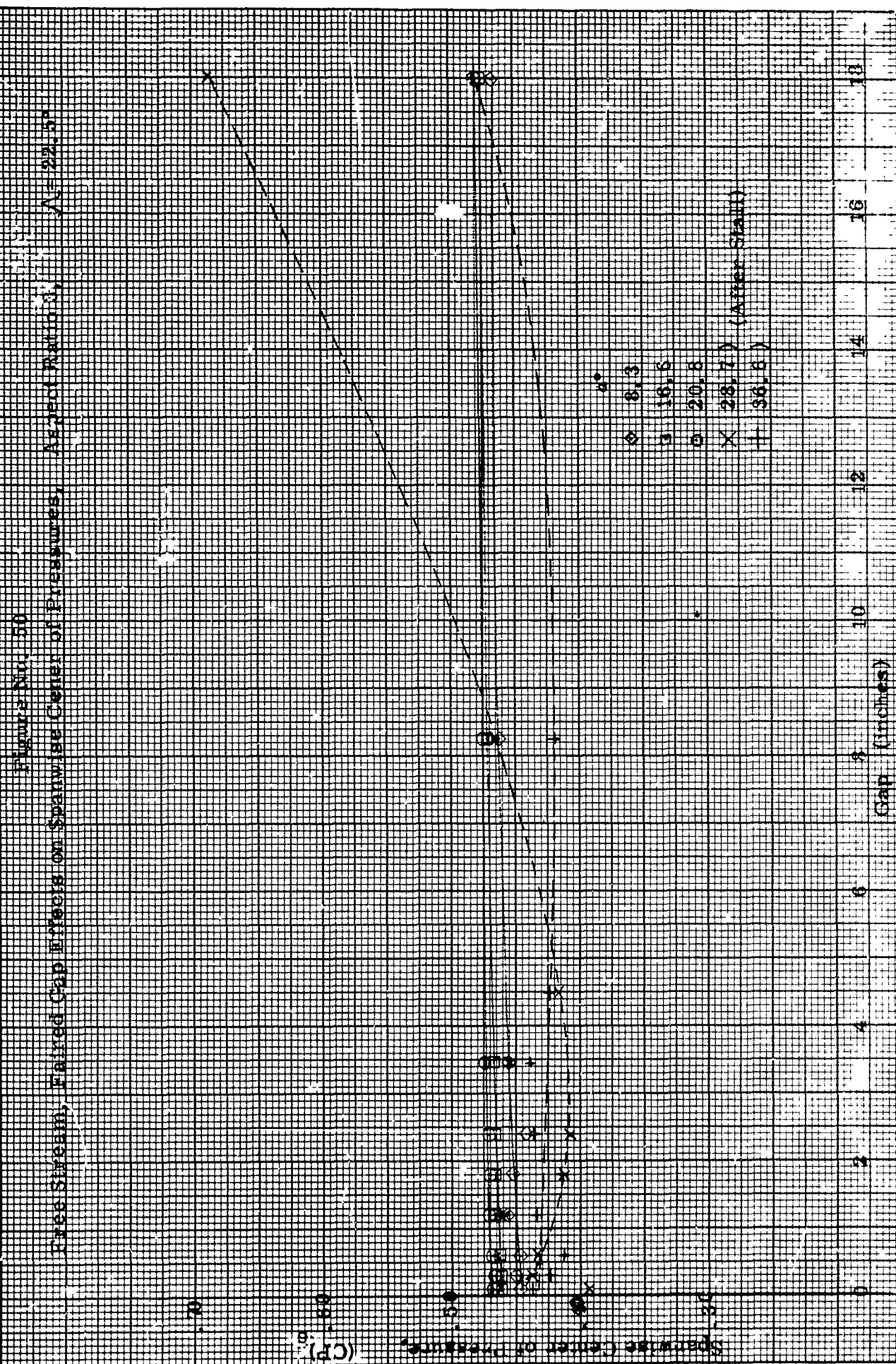


Figure No. 49

Free Stream, Paired Gap Effects on Spanwise Center of Pressure, Aspect Ratio 3, $\Lambda = 11^\circ$

ρ^*
 ϕ 8.3
 \square 16.8
 \circ 23.9
 \times 36.5 (After Stall)
 $+$ 45.5





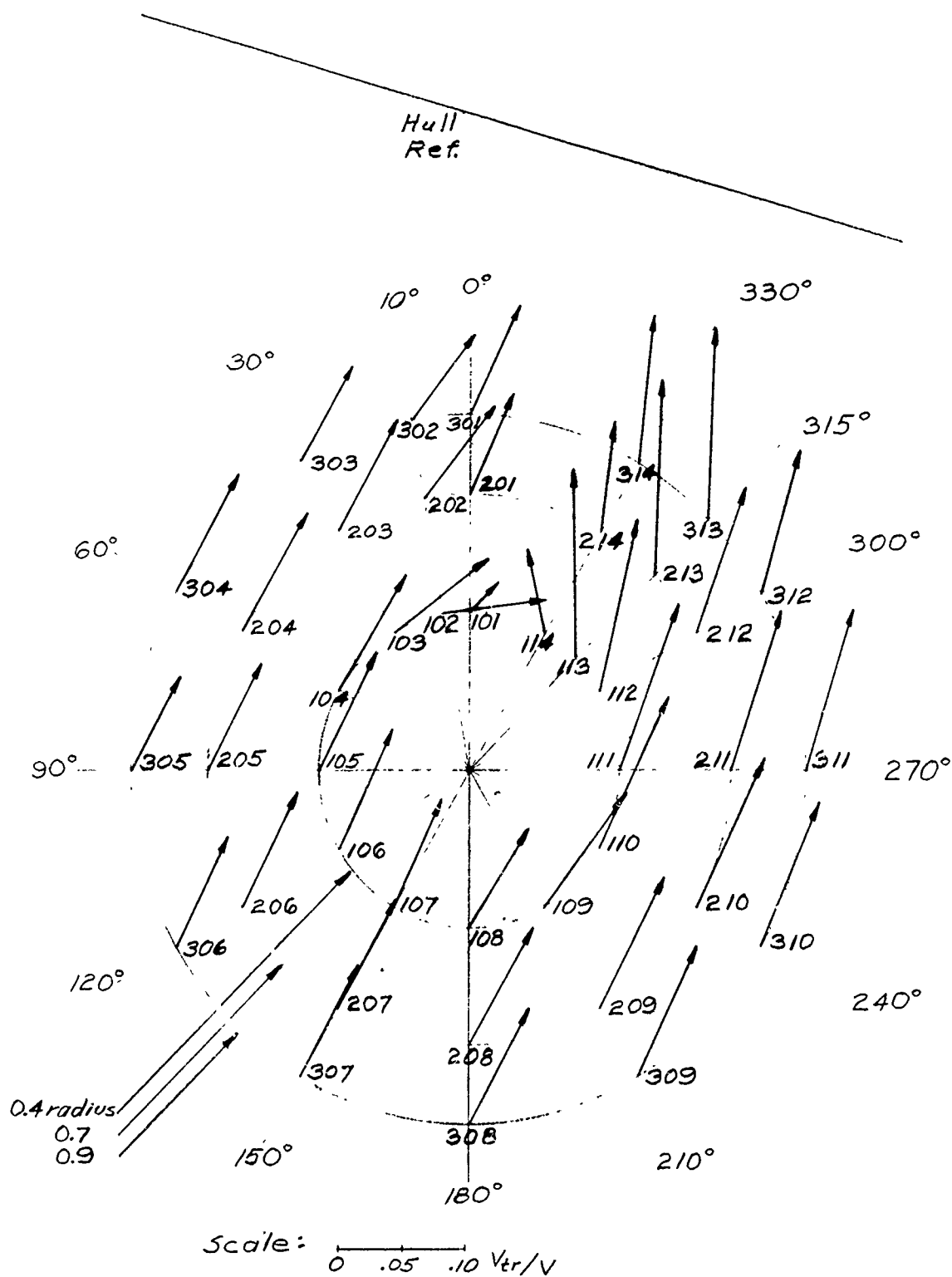


Figure No. 51. Wake Velocity Diagram
(From Figure 11 of Reference 6)

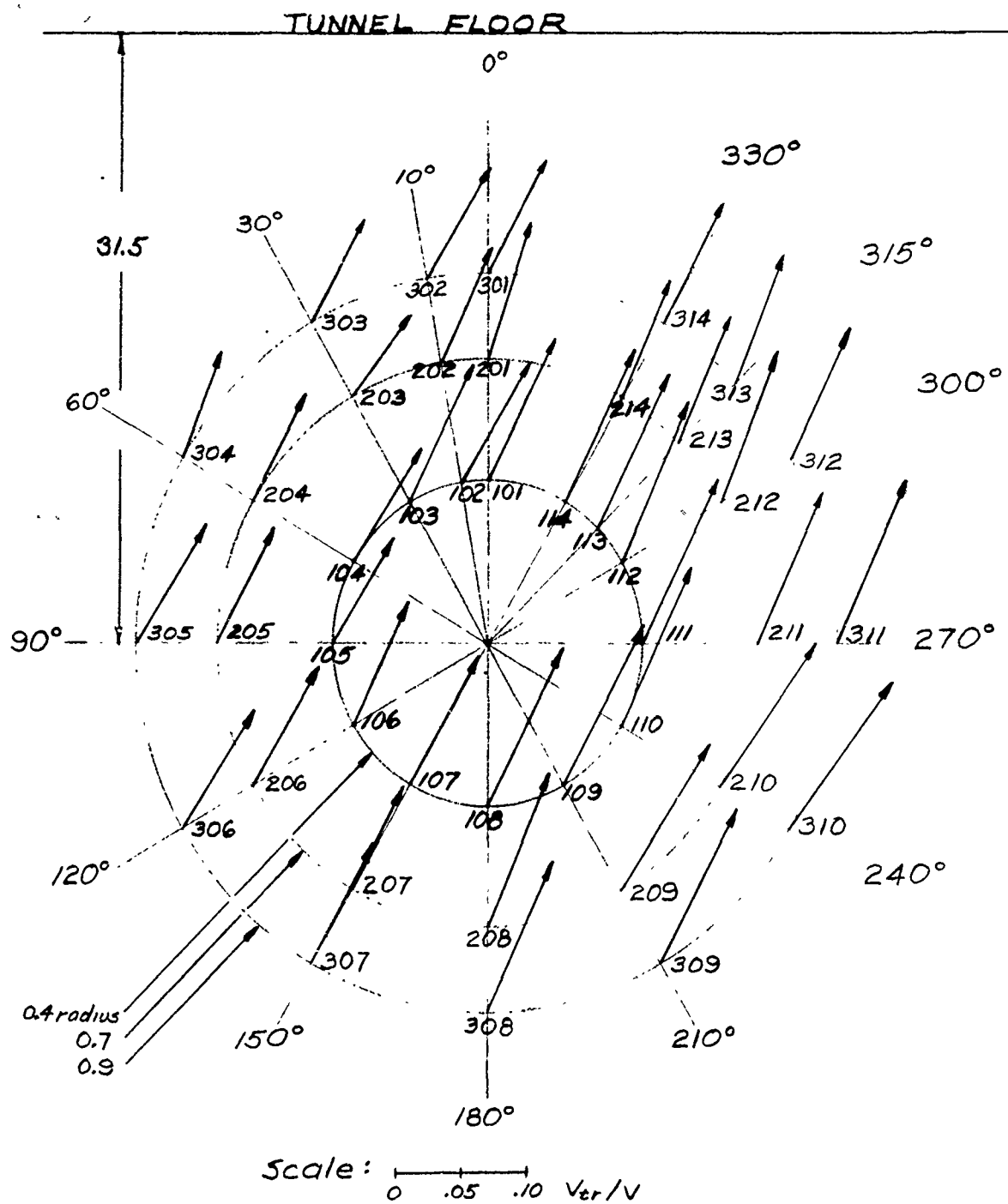


Figure No. 52. Wake Velocity Diagram For Simulated Hull Flow.

Figure No. 53

Paired Gap Effects on Lift Coefficient for Simulated Full Flow,
Aspect Ratio 2, $\Lambda = 0^\circ$

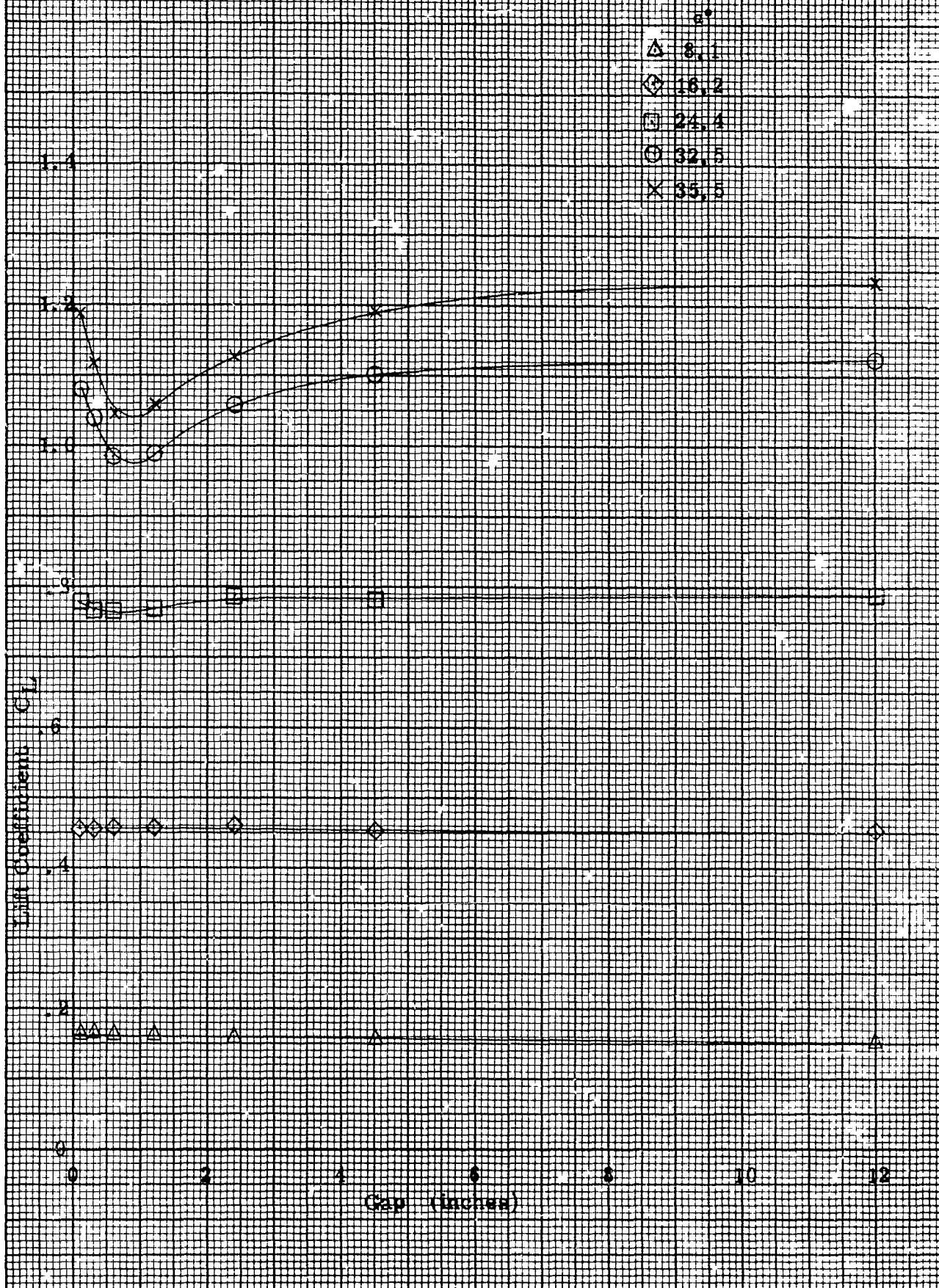
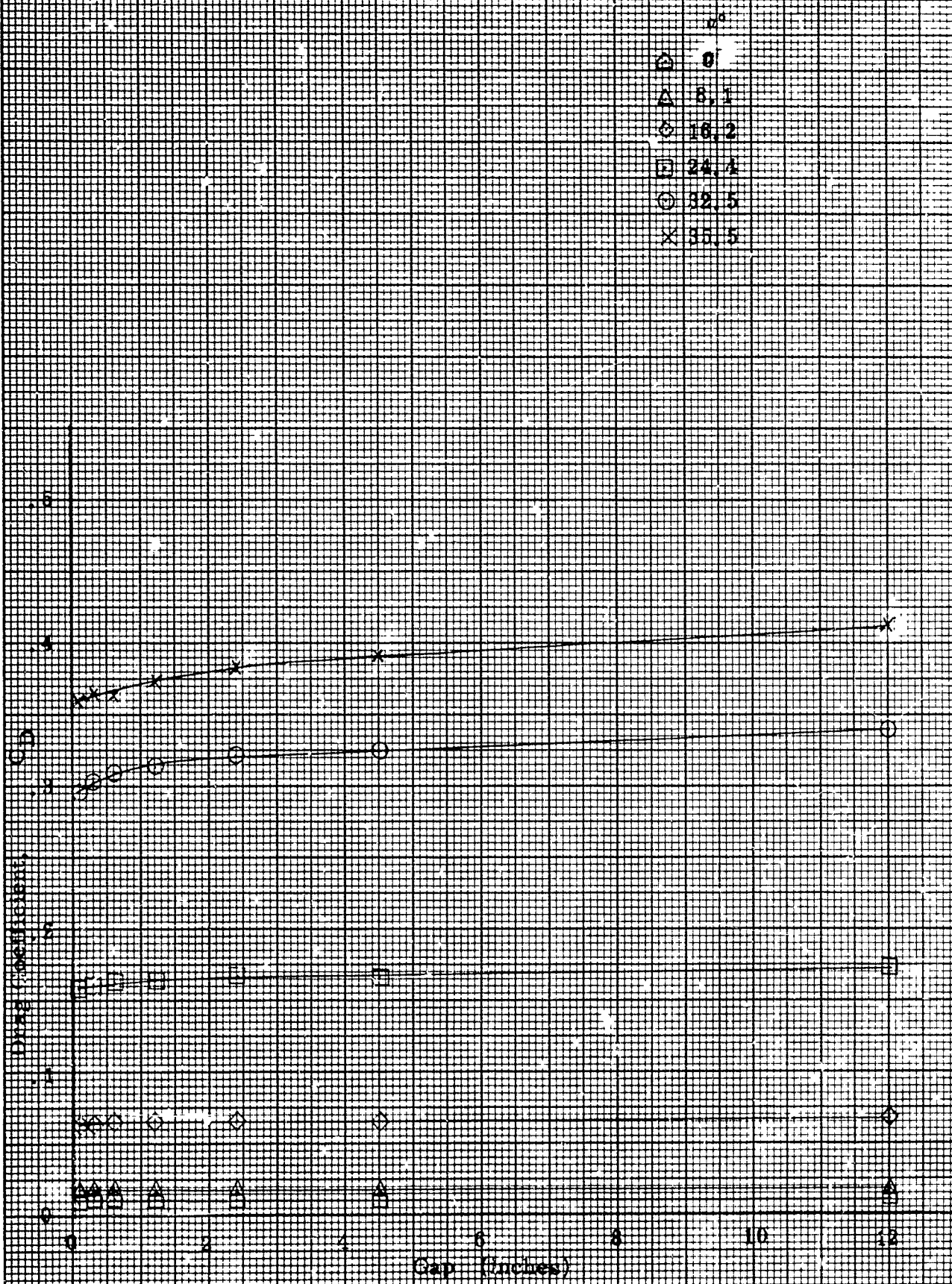
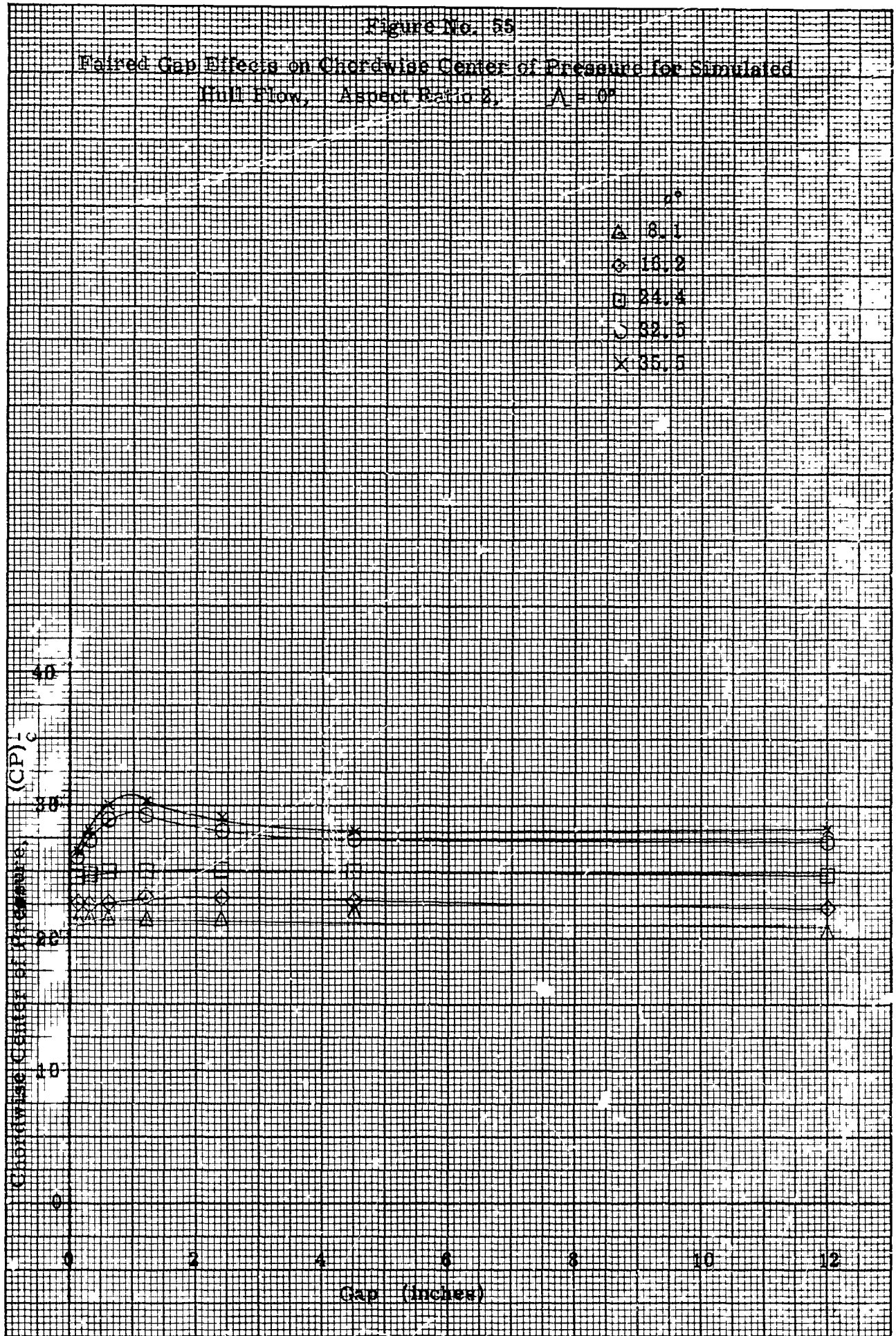


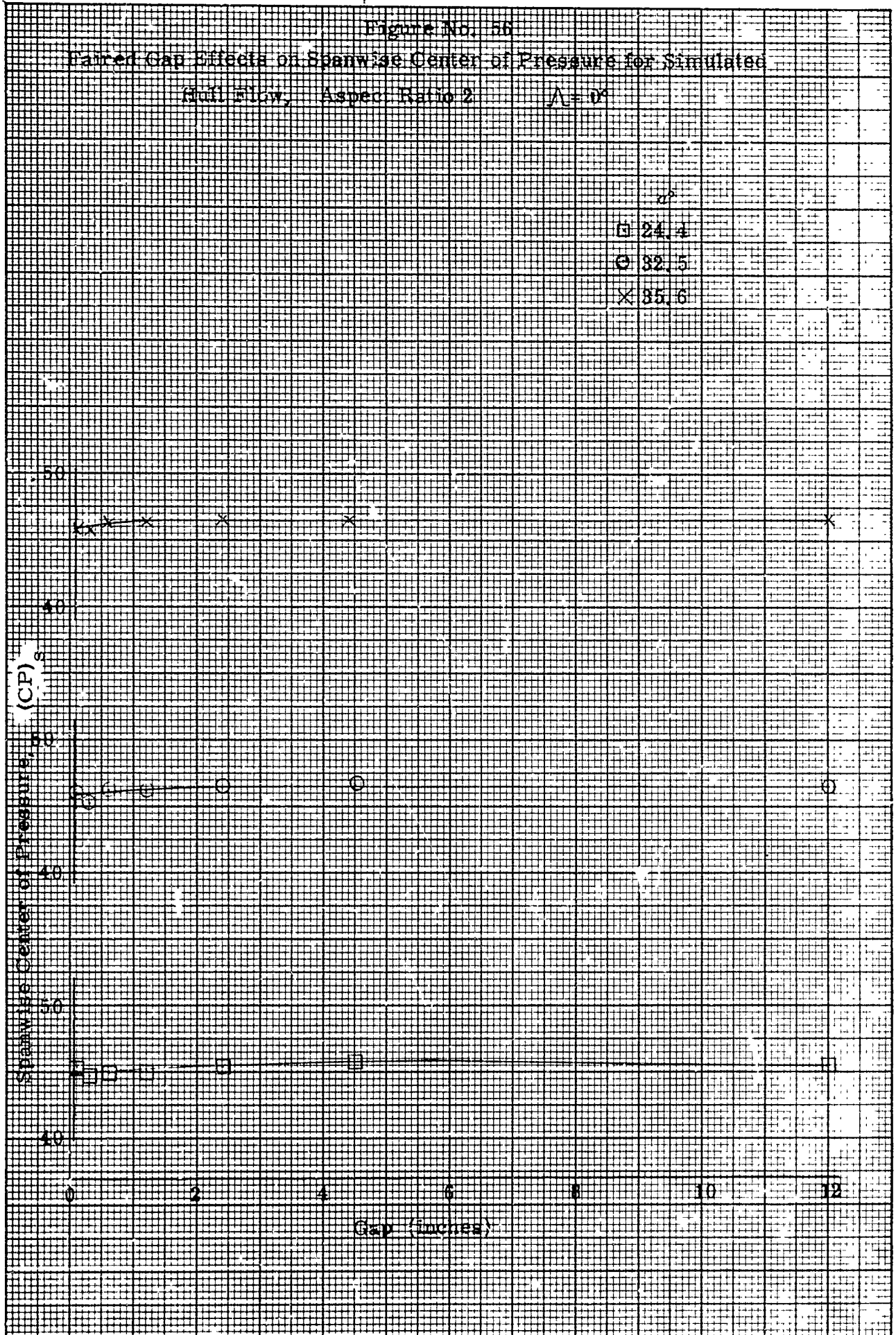
Figure No. 54

Faired Gap Effects on Drag Coefficient for Simulated Hull Flow
Aspect Ratio 2, $\Delta = 0^\circ$



K-E 10 X 10 TO 1/2 INCH 46 1323
7 X 10 INCHES
MADE IN U.S.A.
KEUFFEL & ESSER CO.





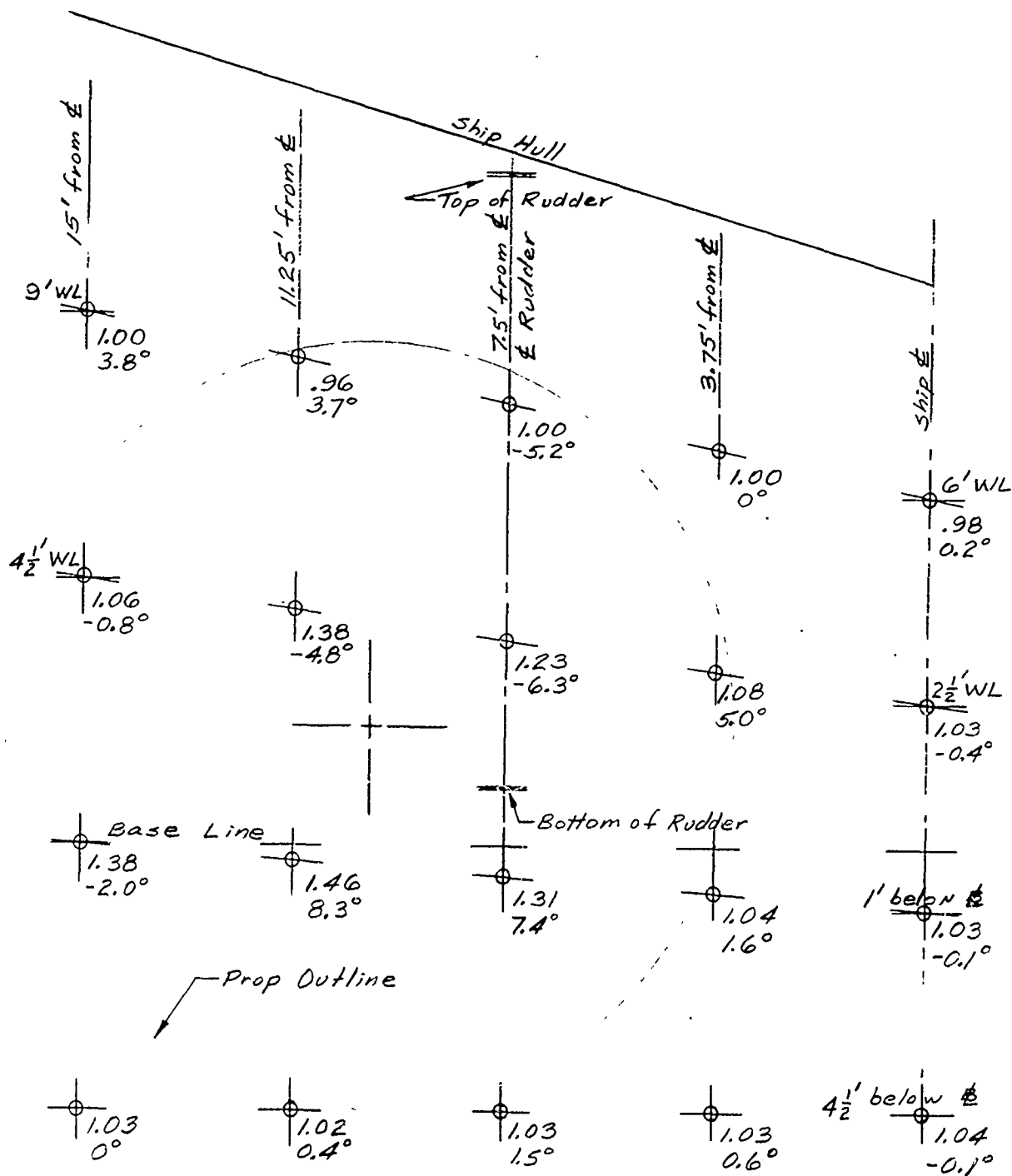


Figure No. 57. Velocity Field at Rudder Leading Edge,
(From Figure 5 of Reference 7)

Note: At each location, the upper figure is the value of V_x/V , and the lower figure is the flow angle. (Positive in the direction of the ship CL)

Variable	Unit	Mean	Standard deviation	Minimum	Maximum
Age	Years	35.2	12.5	18	65
Gender	Male/Female	50.0/50.0	-	-	-
Education	Years	12.8	2.1	8	16
Income	\$/month	1500	500	500	3000
Marital status	Married/Single	60.0/40.0	-	-	-
Occupation	Various	-	-	-	-
Health status	Good/Poor	70.0/30.0	-	-	-
Smoking status	Smoker/Non-smoker	30.0/70.0	-	-	-
Alcohol consumption	Yes/No	20.0/80.0	-	-	-
Exercise frequency	Times/week	2.5	1.5	0	5
Dietary habits	Healthy/Unhealthy	40.0/60.0	-	-	-
Stress level	Low/High	55.0/45.0	-	-	-
Sleep quality	Good/Poor	65.0/35.0	-	-	-
Family size	Number of children	1.5	1.0	0	3
Home ownership	Owner/Renter	75.0/25.0	-	-	-
Commute time	Minutes	25	15	10	45
Neighborhood safety	High/Low	60.0/40.0	-	-	-
Access to healthcare	Yes/No	90.0/10.0	-	-	-
Health insurance	Yes/No	85.0/15.0	-	-	-
Chronic conditions	Number of conditions	0.8	1.2	0	3
Medication use	Yes/No	35.0/65.0	-	-	-
Healthcare utilization	Visits/year	2.0	1.5	0	5
Healthcare costs	\$/year	1000	500	0	2000
Healthcare satisfaction	High/Low	50.0/50.0	-	-	-
Healthcare accessibility	Good/Poor	60.0/40.0	-	-	-
Healthcare quality	High/Low	55.0/45.0	-	-	-
Healthcare equity	High/Low	50.0/50.0	-	-	-
Healthcare transparency	High/Low	50.0/50.0	-	-	-
Healthcare accountability	High/Low	50.0/50.0	-	-	-
Healthcare responsiveness	High/Low	50.0/50.0	-	-	-
Healthcare effectiveness	High/Low	50.0/50.0	-	-	-
Healthcare efficiency	High/Low	50.0/50.0	-	-	-
Healthcare safety	High/Low	50.0/50.0	-	-	-
Healthcare security	High/Low	50.0/50.0	-	-	-
Healthcare privacy	High/Low	50.0/50.0	-	-	-
Healthcare integrity	High/Low	50.0/50.0	-	-	-
Healthcare honesty	High/Low	50.0/50.0	-	-	-
Healthcare trustworthiness	High/Low	50.0/50.0	-	-	-
Healthcare reliability	High/Low	50.0/50.0	-	-	-
Healthcare dependability	High/Low	50.0/50.0	-	-	-
Healthcare predictability	High/Low	50.0/50.0	-	-	-
Healthcare consistency	High/Low	50.0/50.0	-	-	-
Healthcare uniformity	High/Low	50.0/50.0	-	-	-
Healthcare standardization	High/Low	50.0/50.0	-	-	-
Healthcare harmonization	High/Low	50.0/50.0	-	-	-
Healthcare synchronization	High/Low	50.0/50.0	-	-	-
Healthcare coordination	High/Low	50.0/50.0	-	-	-
Healthcare integration	High/Low	50.0/50.0	-	-	-
Healthcare collaboration	High/Low	50.0/50.0	-	-	-
Healthcare partnership	High/Low	50.0/50.0	-	-	-
Healthcare alliance	High/Low	50.0/50.0	-	-	-
Healthcare coalition	High/Low	50.0/50.0	-	-	-
Healthcare confederation	High/Low	50.0/50.0	-	-	-
Healthcare federation	High/Low	50.0/50.0	-	-	-
Healthcare union	High/Low	50.0/50.0	-	-	-
Healthcare association	High/Low	50.0/50.0	-	-	-
Healthcare organization	High/Low	50.0/50.0	-	-	-
Healthcare institution	High/Low	50.0/50.0	-	-	-
Healthcare establishment	High/Low	50.0/50.0	-	-	-
Healthcare organization	High/Low	50.0/50.0	-	-	-
Healthcare institution	High/Low	50.0/50.0	-	-	-
Healthcare establishment	High/Low	50.0/50.0	-	-	-
Healthcare organization	High/Low	50.0/50.0	-	-	-
Healthcare institution	High/Low	50.0/50.0	-	-	-
Healthcare establishment	High/Low	50.0/50.0	-	-	-
Healthcare organization	High/Low	50.0/50.0	-	-	-
Healthcare institution	High/Low	50.0/50.0	-	-	-
Healthcare establishment	High/Low	50.0/50.0	-	-	-
Healthcare organization	High/Low	50.0/50.0	-	-	-
Healthcare institution	High/Low	50.0/50.0	-		



Variable	Unit	Mean	Standard deviation	Minimum	Maximum
Age	Years	35.2	12.5	18	65
Gender	Male/Female	50/50	0	0	100
Education	Years	12.8	2.1	8	16
Income	Dollars	45,000	15,000	20,000	80,000
Health	Good/Bad	60/40	0	0	100
Marital status	Married/Single	70/30	0	0	100
Occupation	Professional/Service	55/45	0	0	100
Religion	Christian/Jewish/Muslim	65/15/20	0	0	100
Political affiliation	Democrat/Republican	55/45	0	0	100
Home ownership	Own/Rent	75/25	0	0	100
Auto ownership	Own/Don't own	90/10	0	0	100
Travel frequency	Times per year	12	8	0	40
Travel mode	Car/Plane/Train	60/30/10	0	0	100
Travel purpose	Business/Leisure	40/60	0	0	100
Travel satisfaction	1-5	3.2	1.1	1	5

Note: At each location, the upper figure is the value of V_x/V , and the lower figure is the flow angle. (Positive in the direction of the ship ϕ_L)

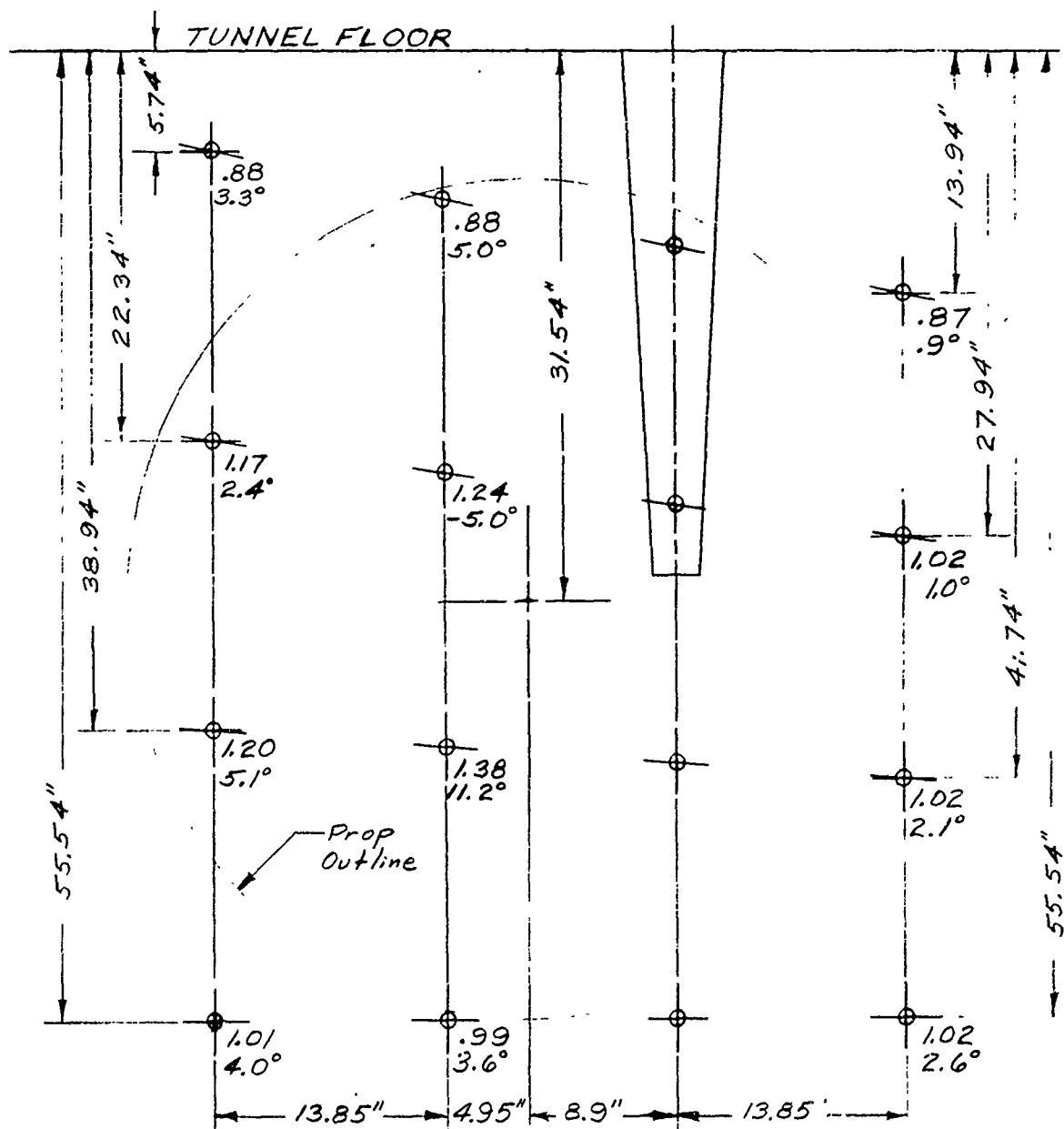
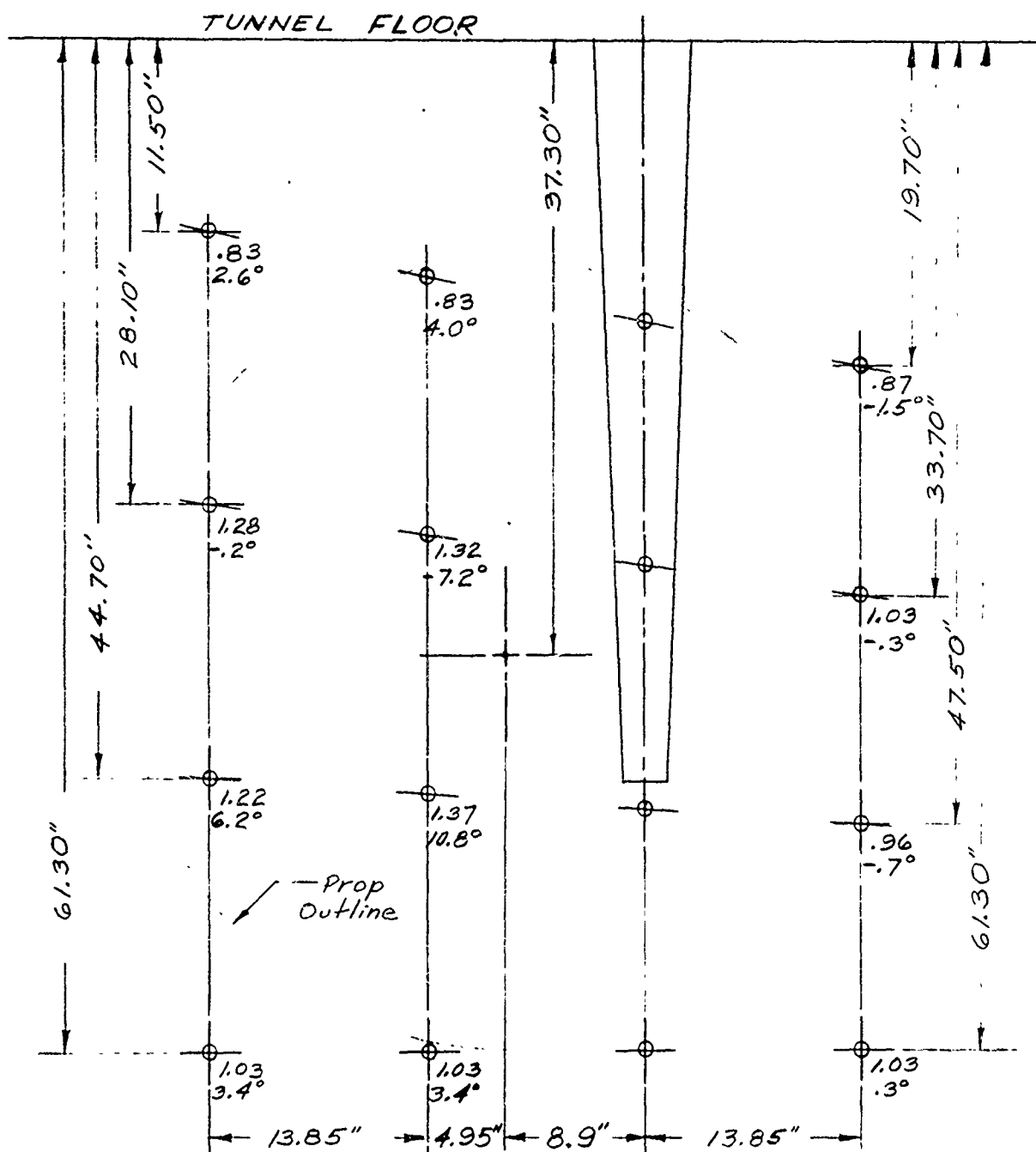
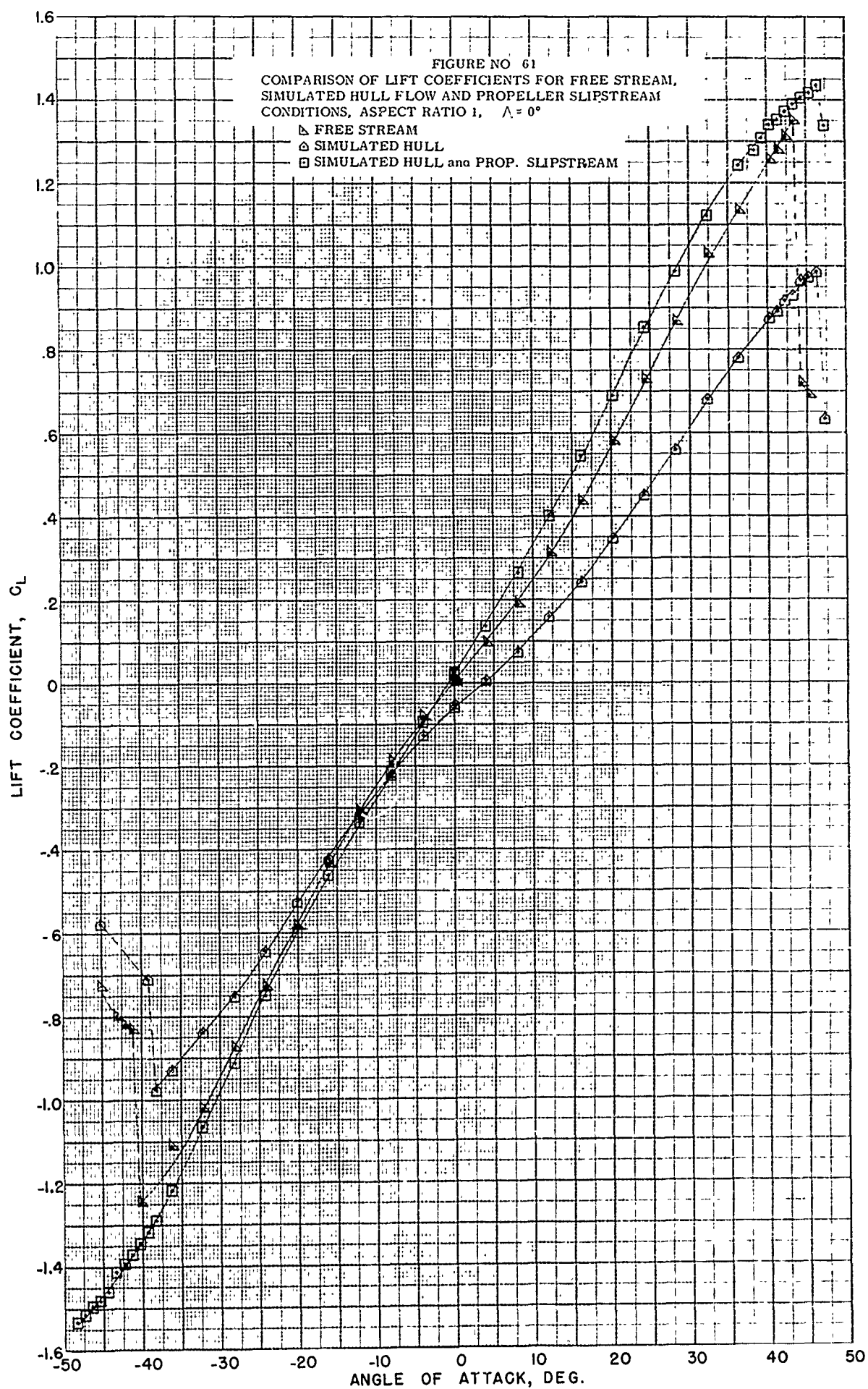


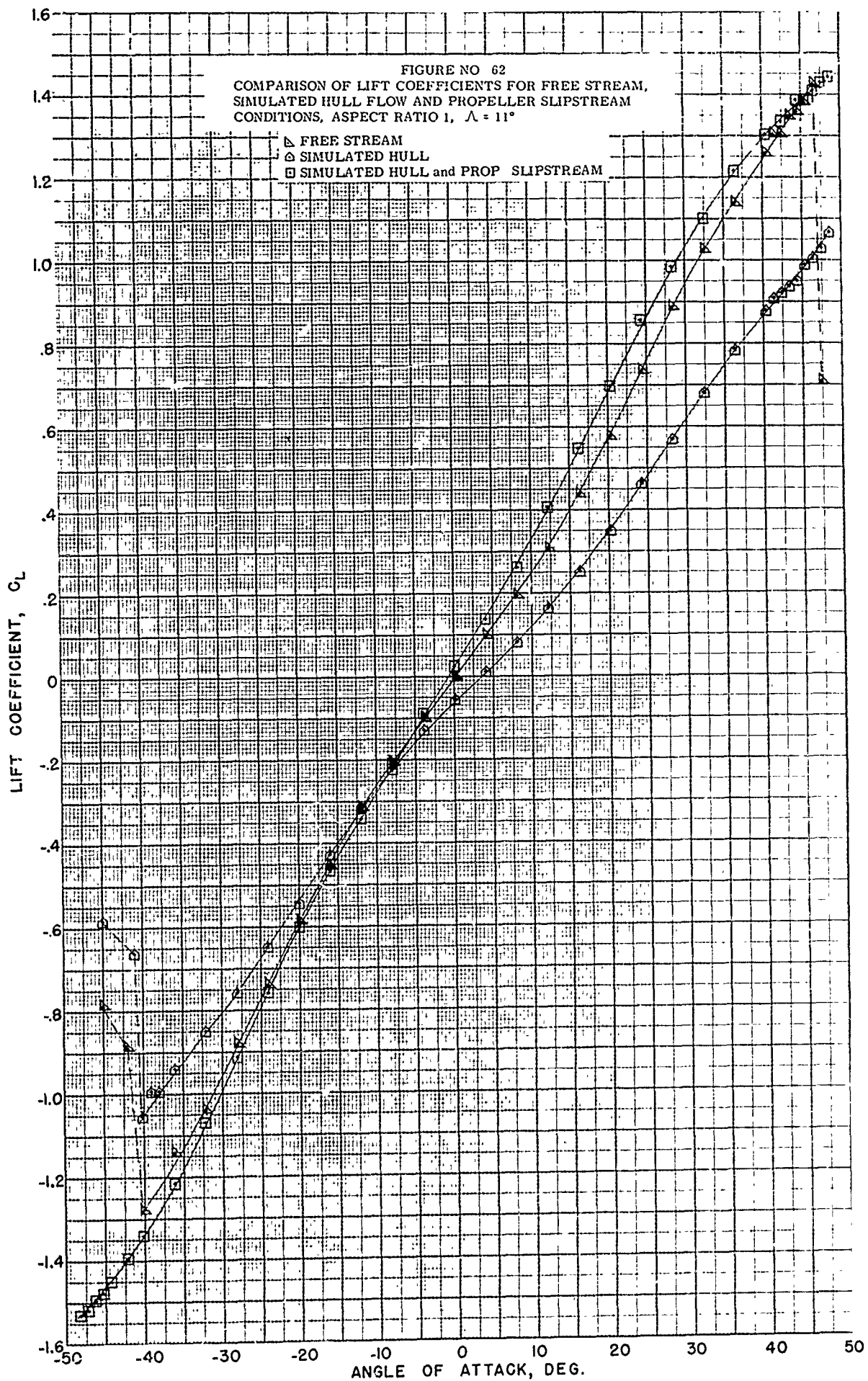
Figure No. 59. Propeller Slipstream Velocity Survey at Rudder Leading Edge, Aspect Ratio 2.

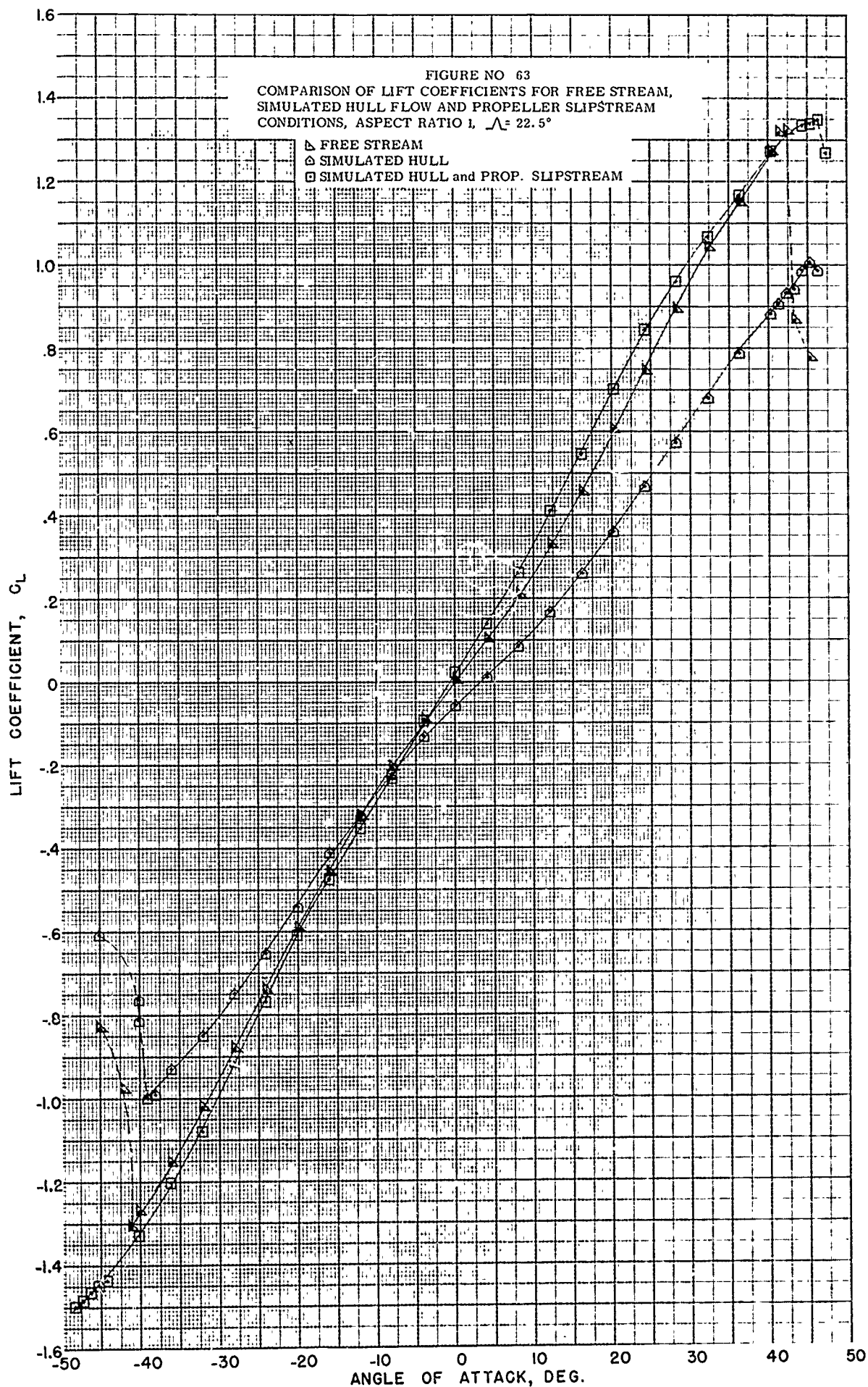
Figure No. 60. Propeller Slipstream Velocity Survey at Rudder Leading Edge, Aspect Ratio 3.

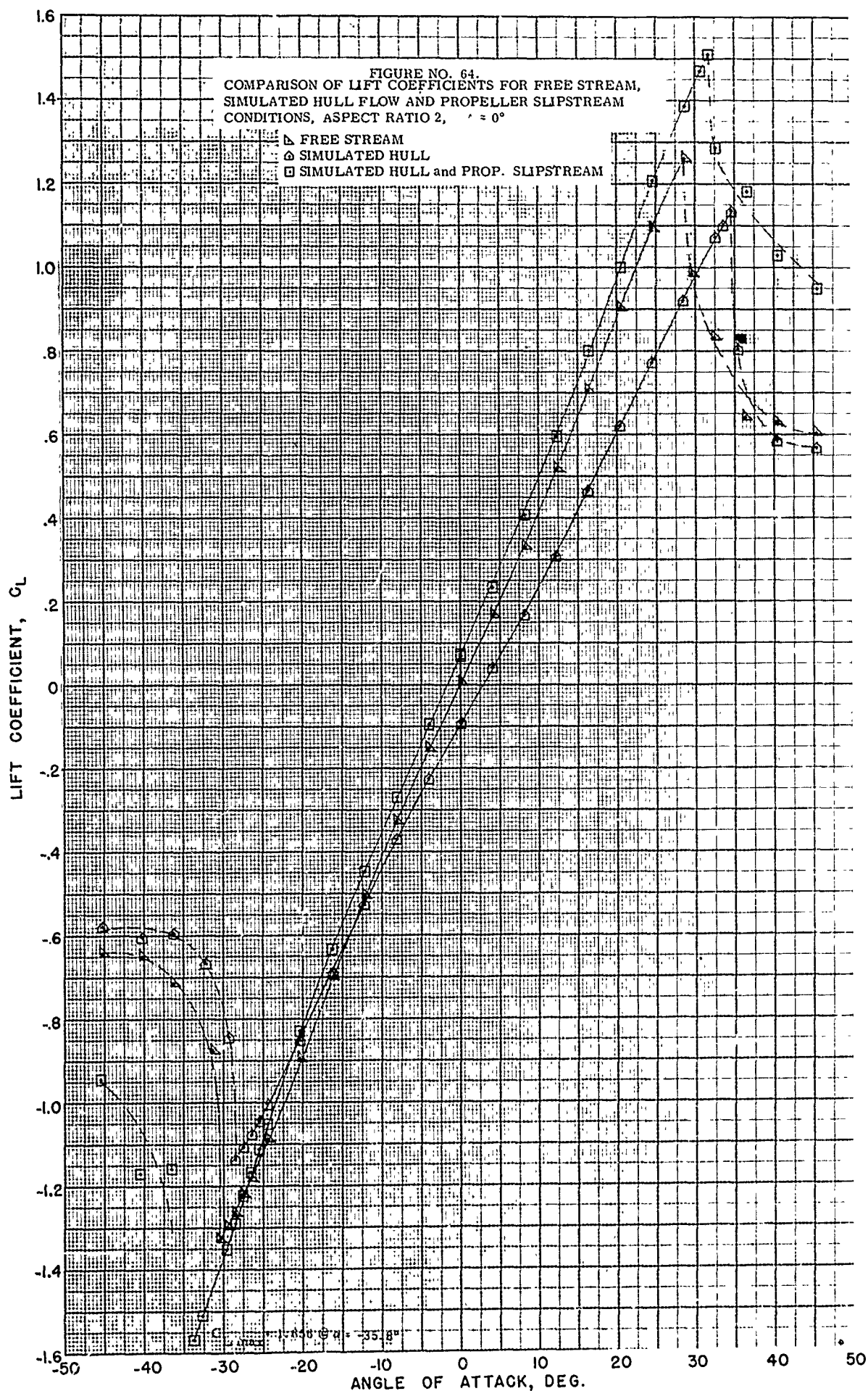
Note: At each location, the upper figure is the value of V_x/V , and the lower figure is the flow angle. (Positive in the direction of the ship C_L)

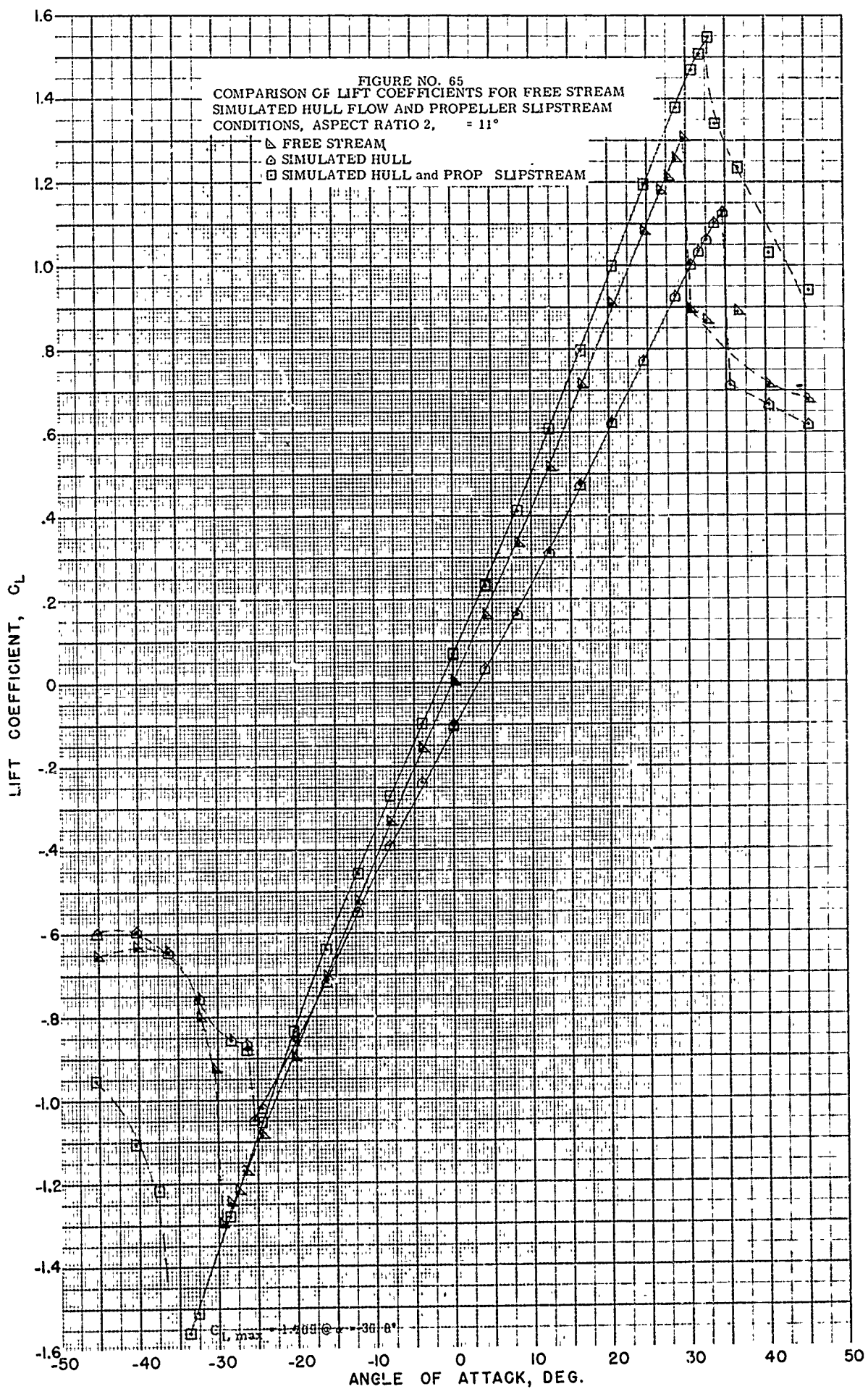


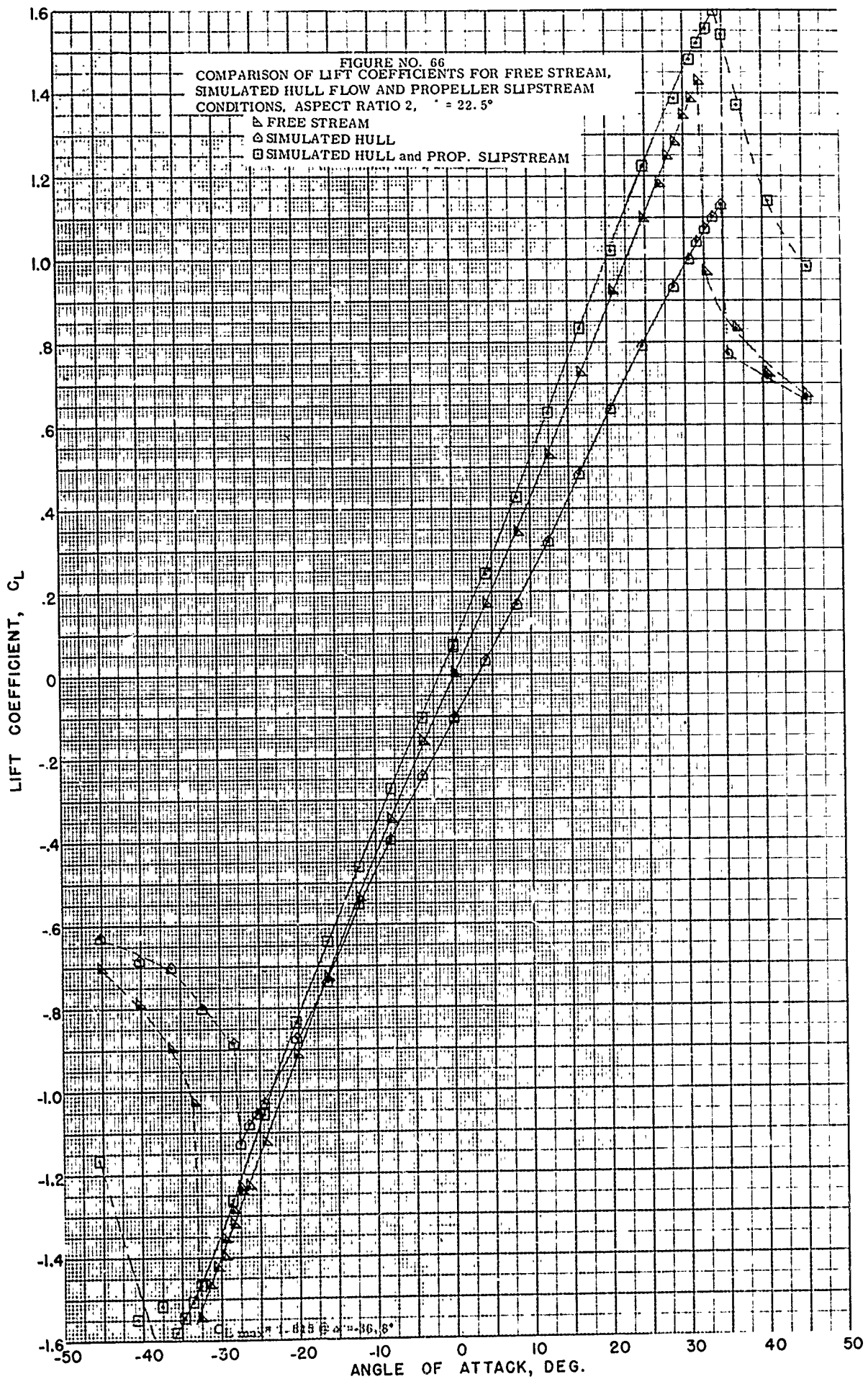


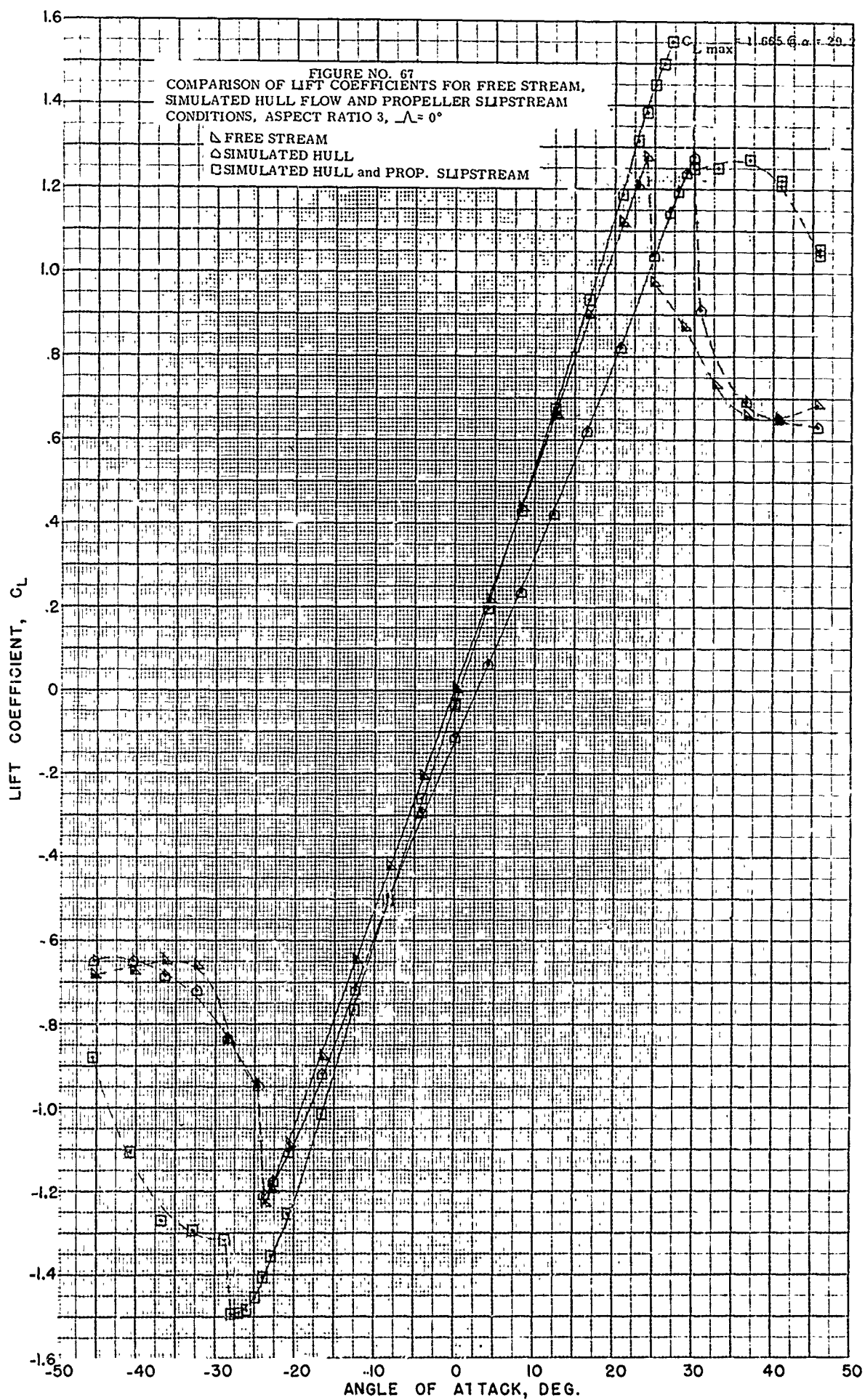


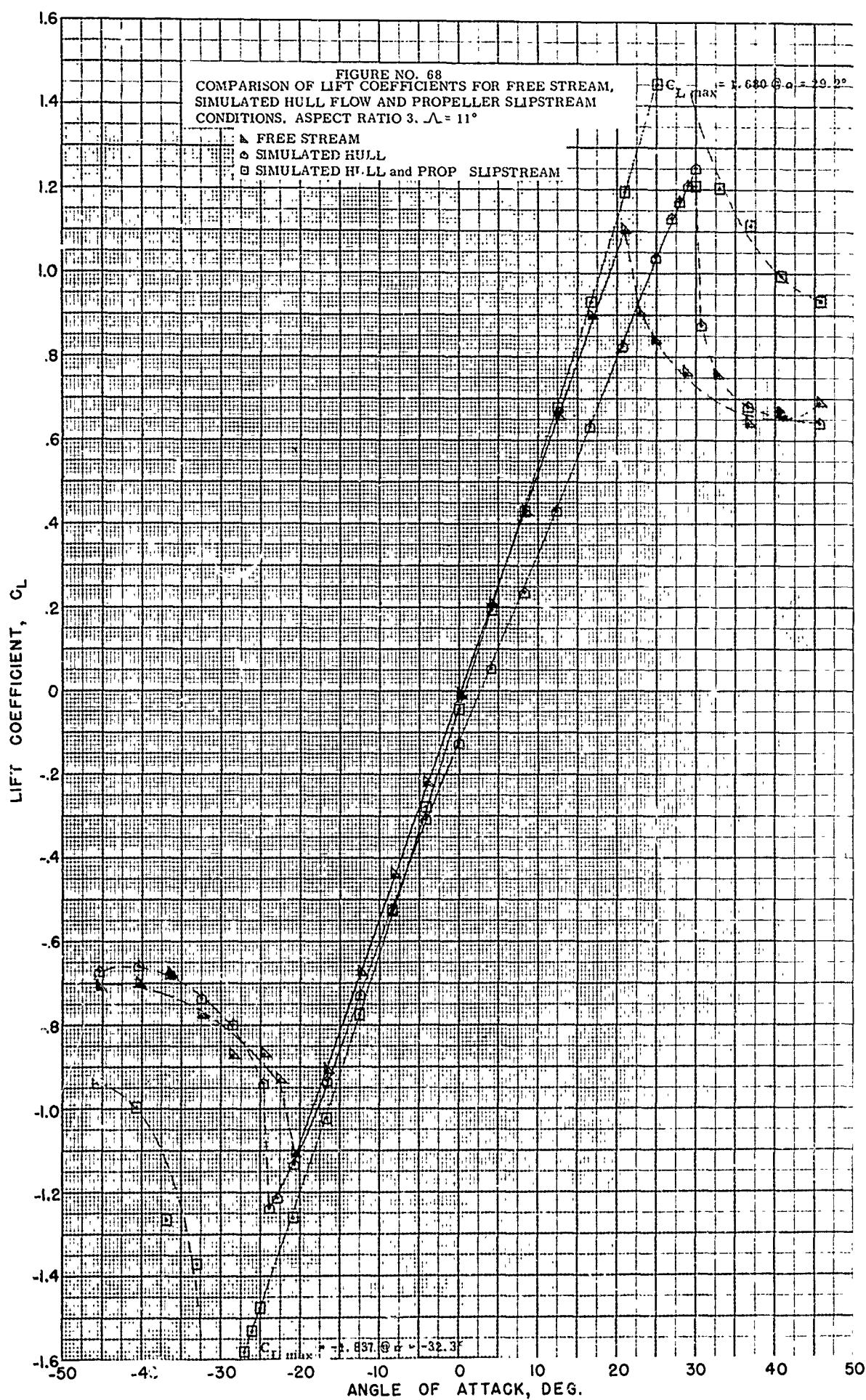


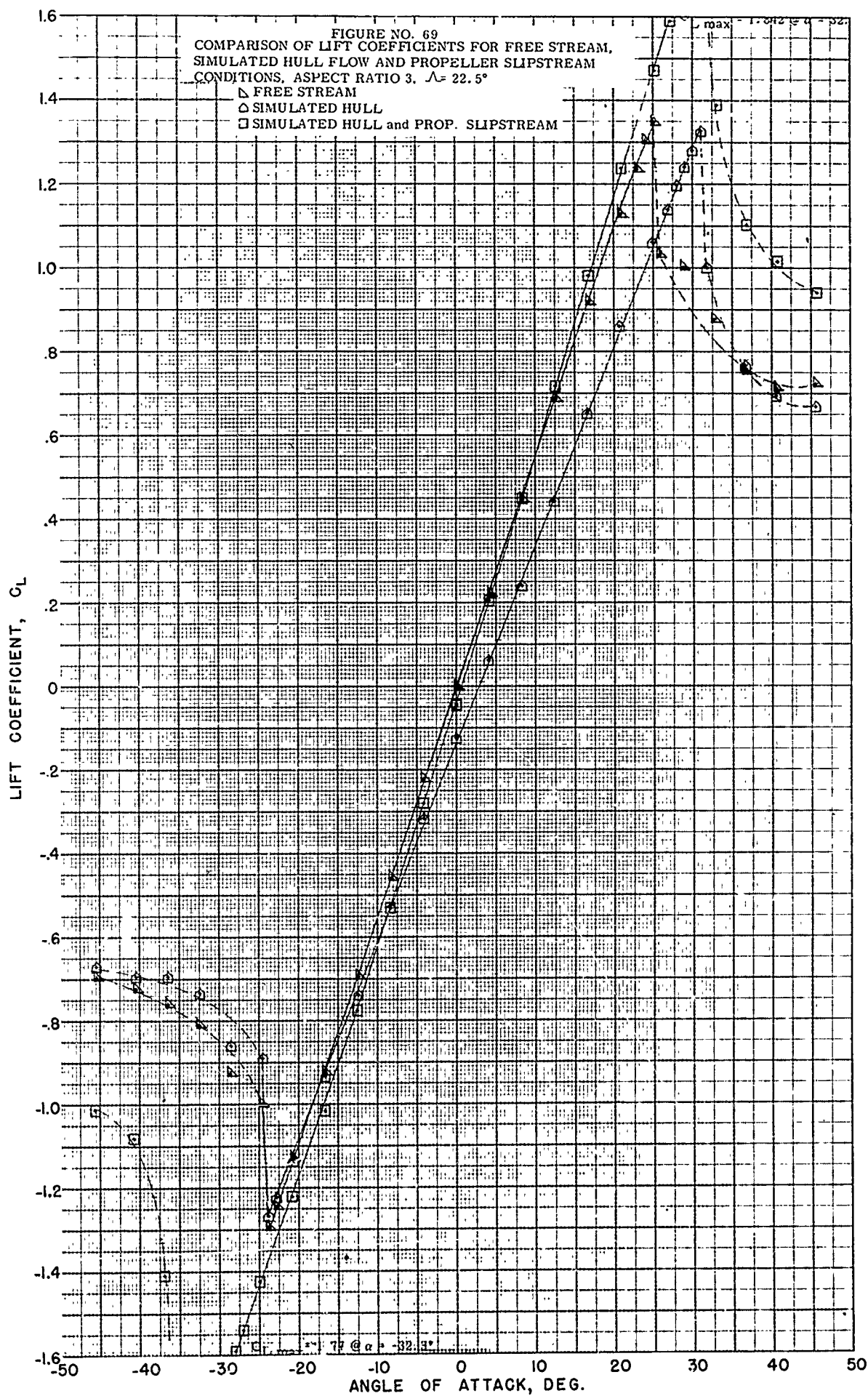


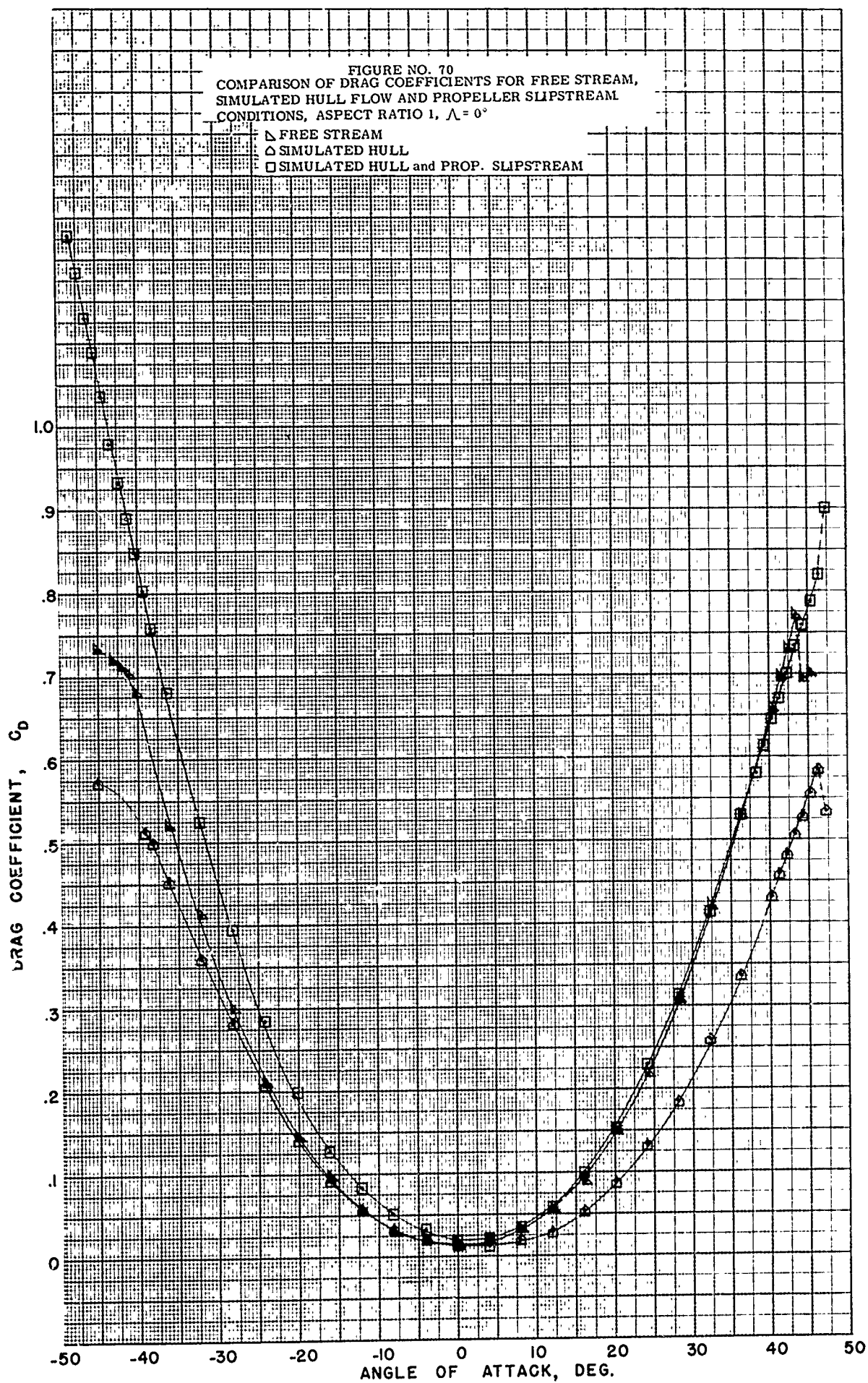


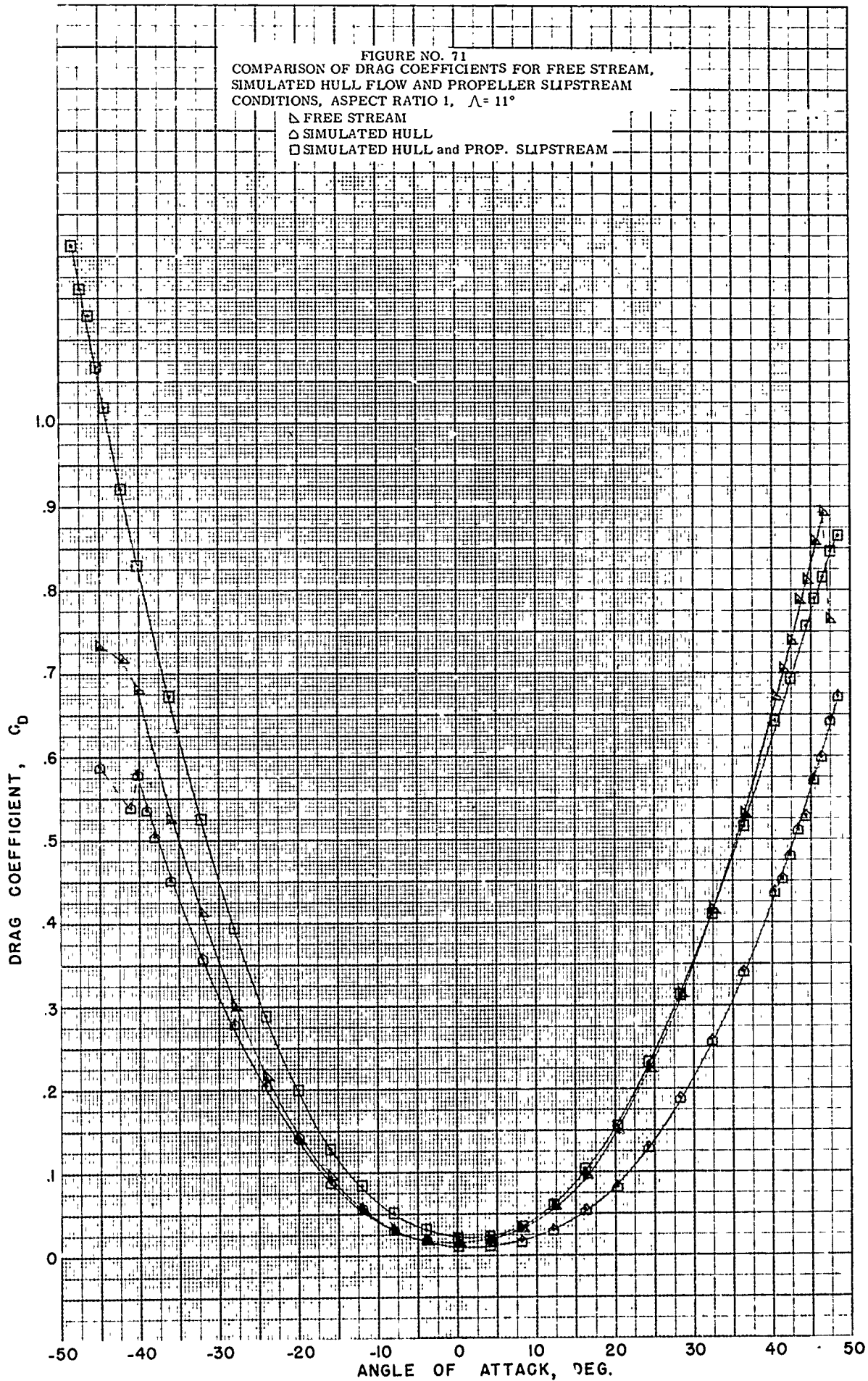












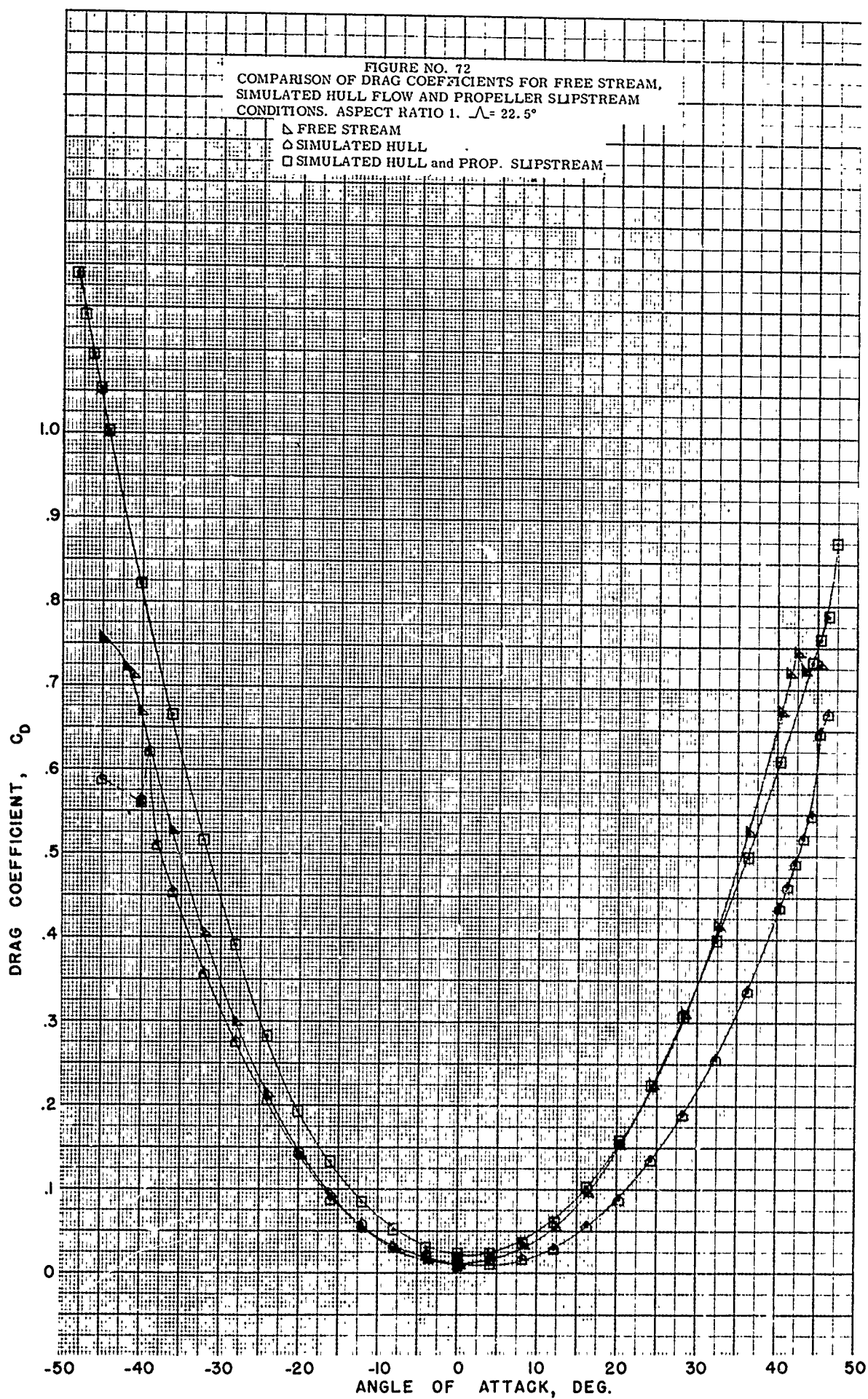


FIGURE NO. 73
COMPARISON OF DRAG COEFFICIENTS FOR FREE STREAM,
SIMULATED HULL FLOW AND PROPELLER SLIPSTREAM
CONDITIONS, ASPECT RATIO 2, $\Lambda = 0^\circ$

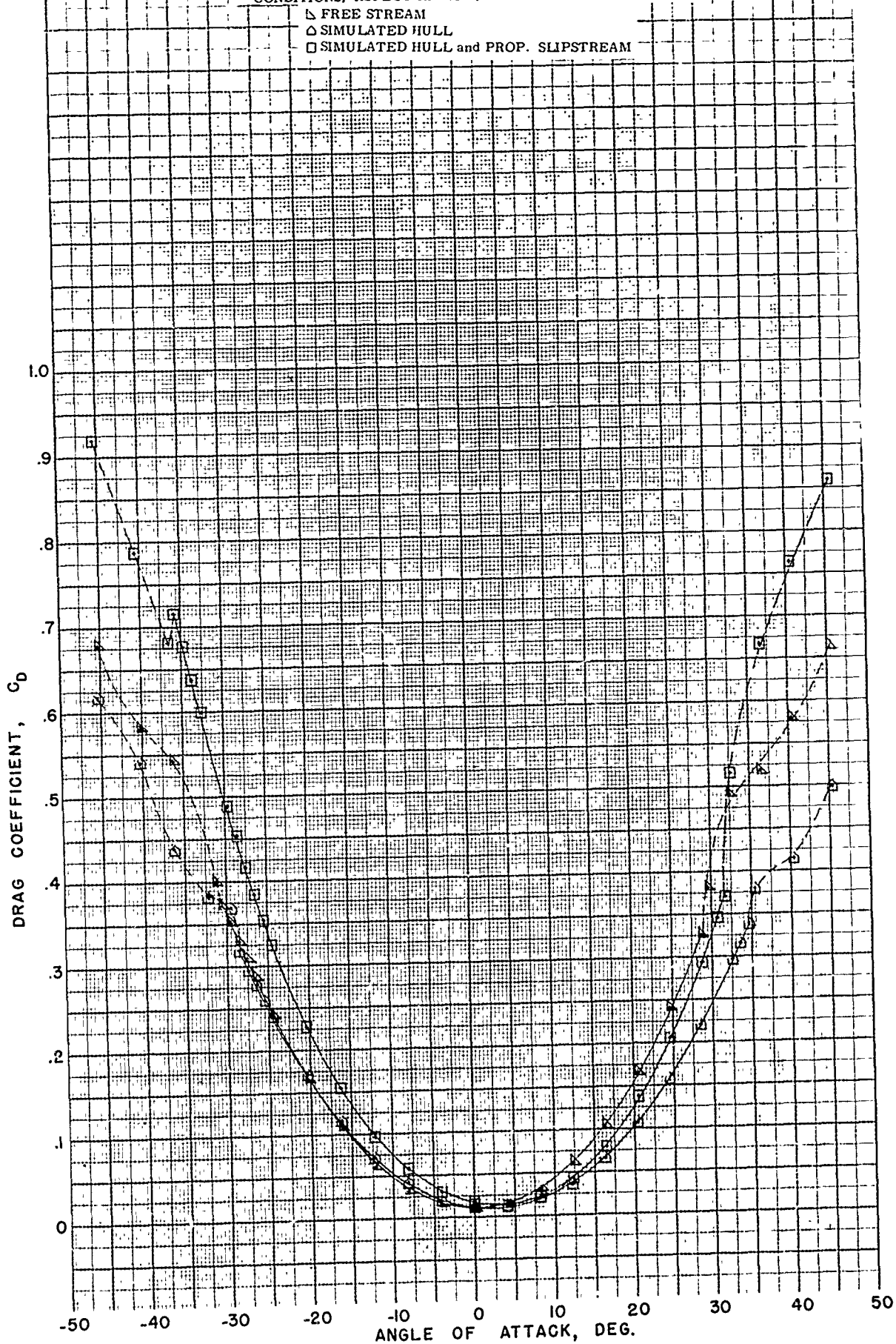
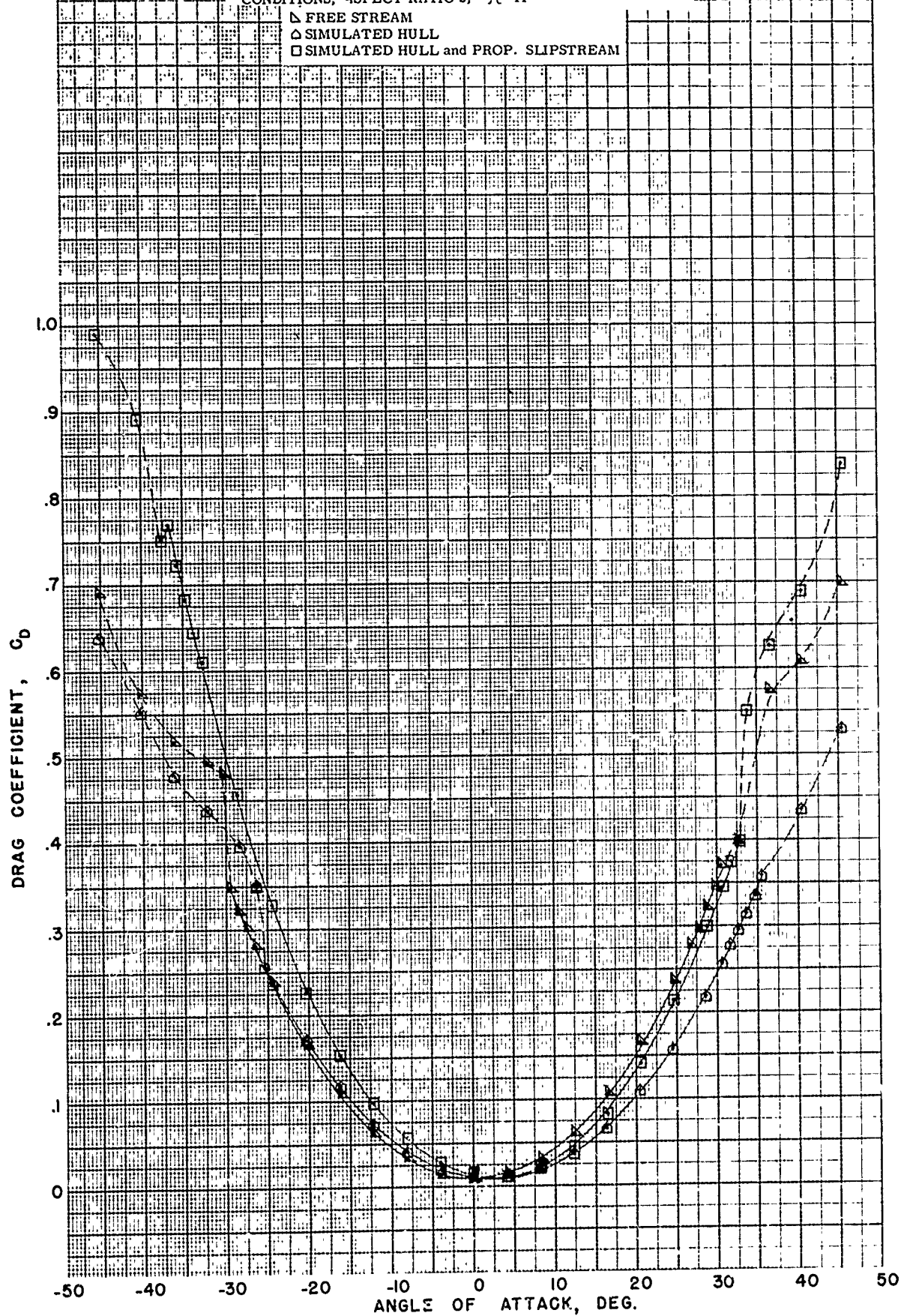
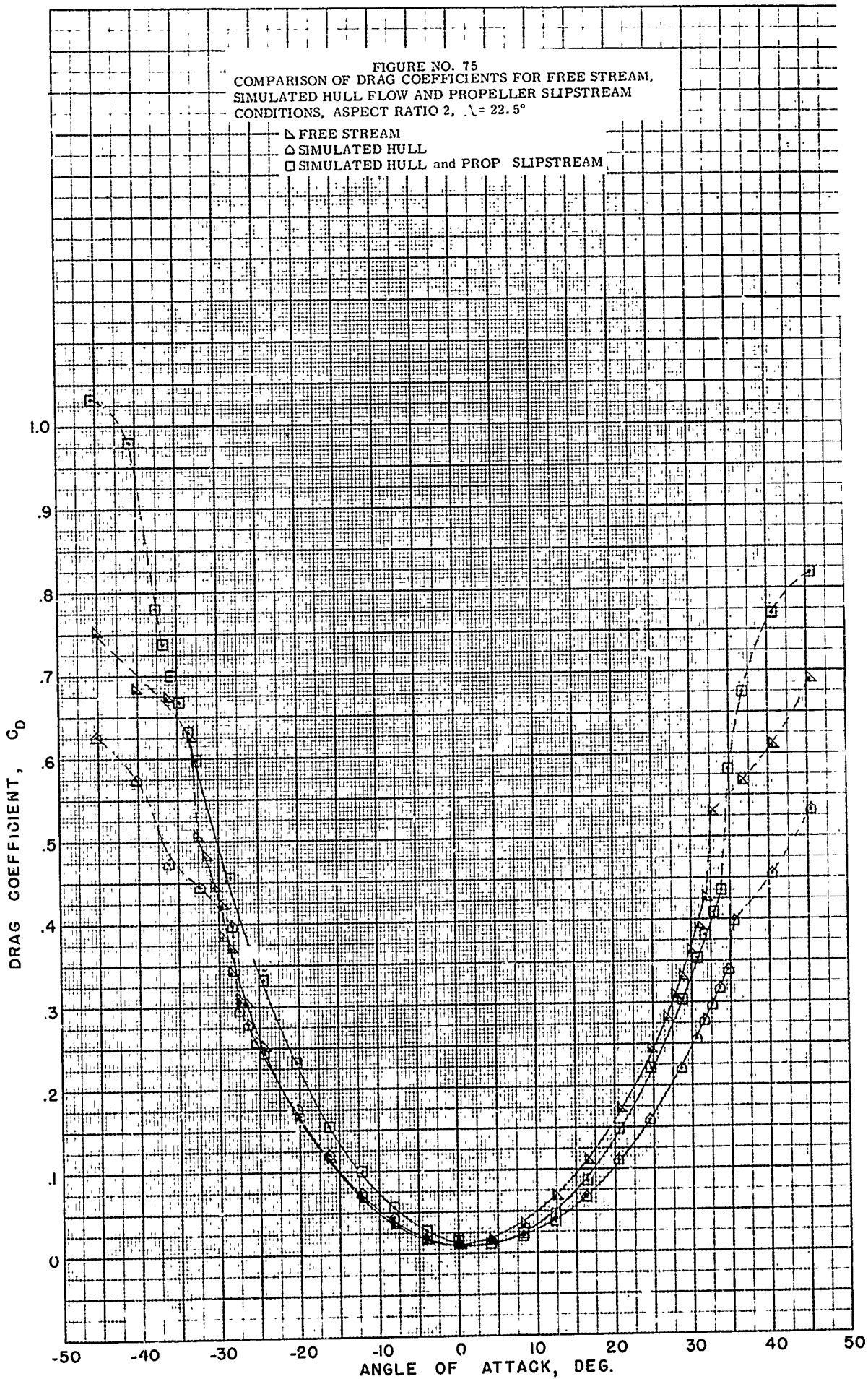


FIGURE NO. 74
COMPARISON OF DRAG COEFFICIENTS FOR FREE STREAM,
SIMULATED HULL FLOW AND PROPELLER SLIPSTREAM
CONDITIONS, ASPECT RATIO 2, $\Lambda = 11^\circ$





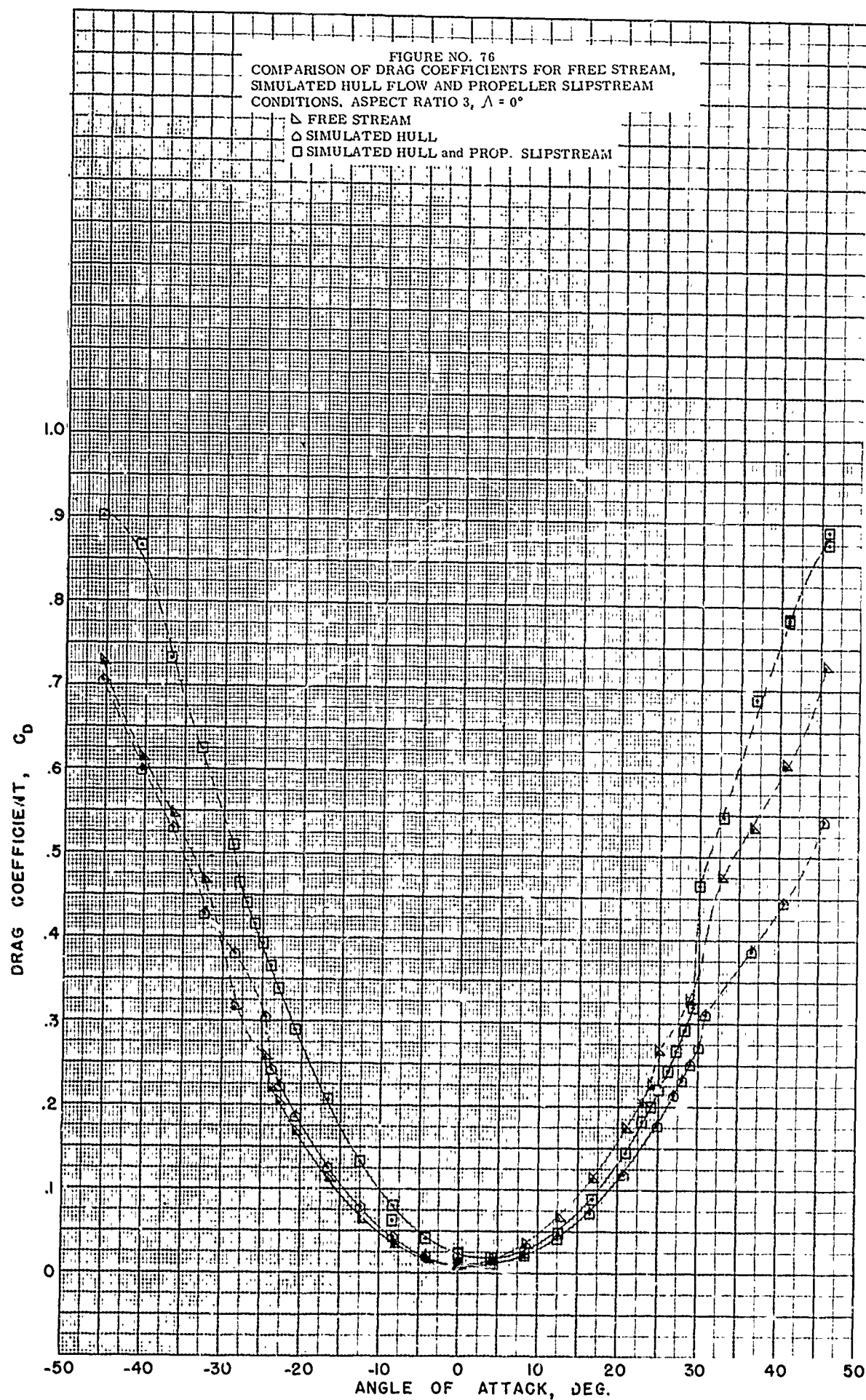


FIGURE NO. 77
COMPARISON OF DRAG COEFFICIENTS FOR FREE STREAM,
SIMULATED HULL FLOW AND PROPELLER SLIPSTREAM
CONDITIONS, ASPECT RATIO 3, $\Lambda = 11^\circ$

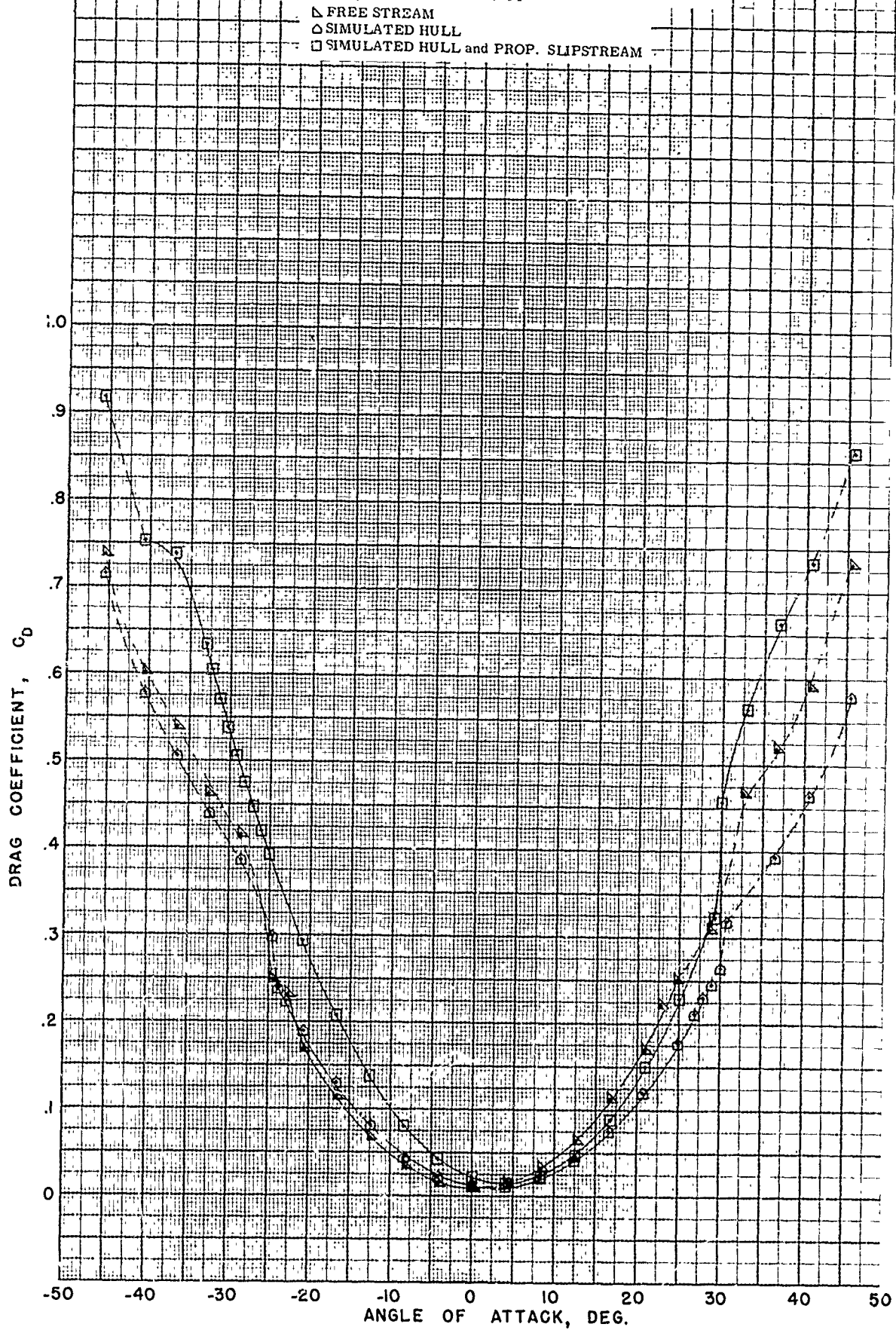
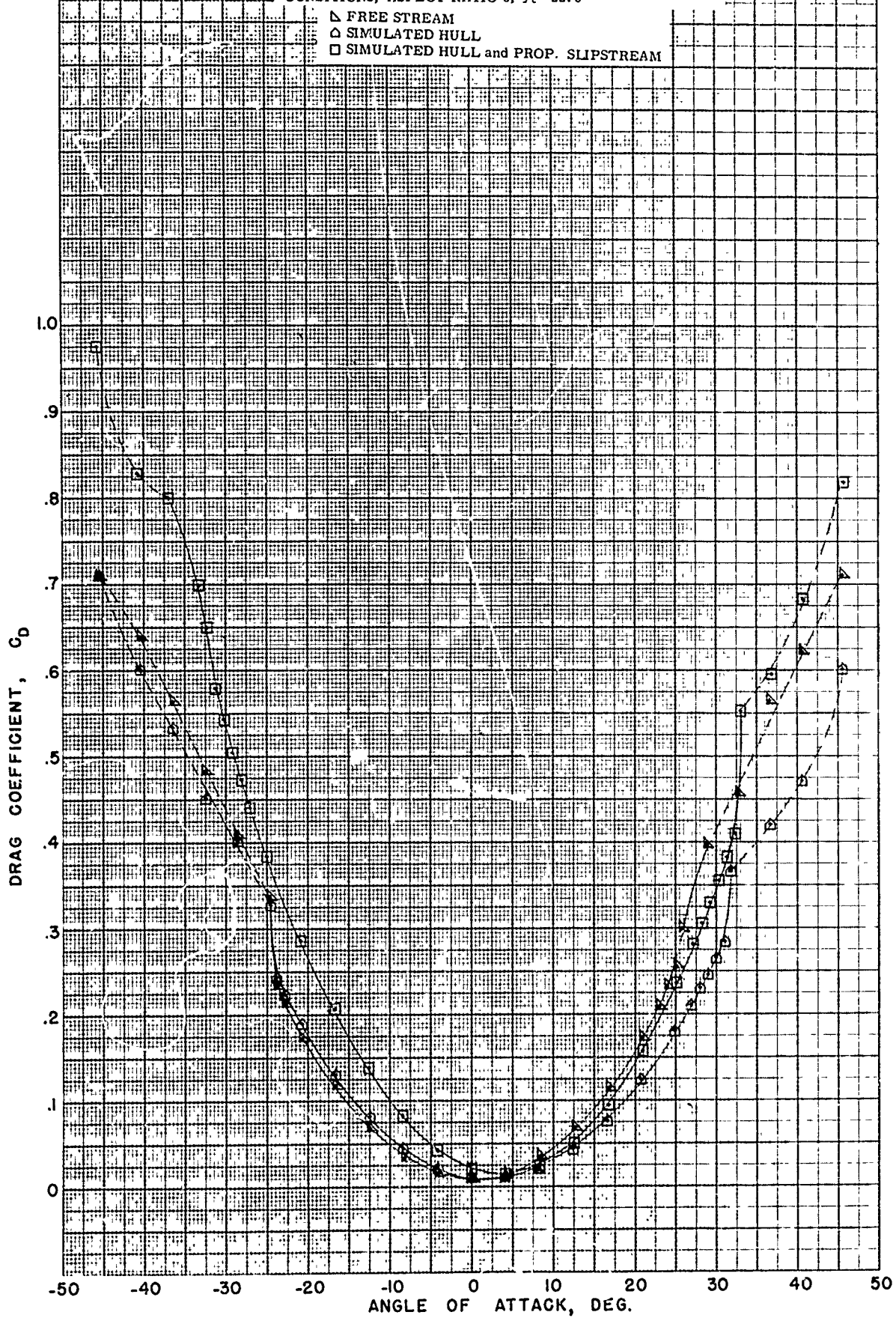
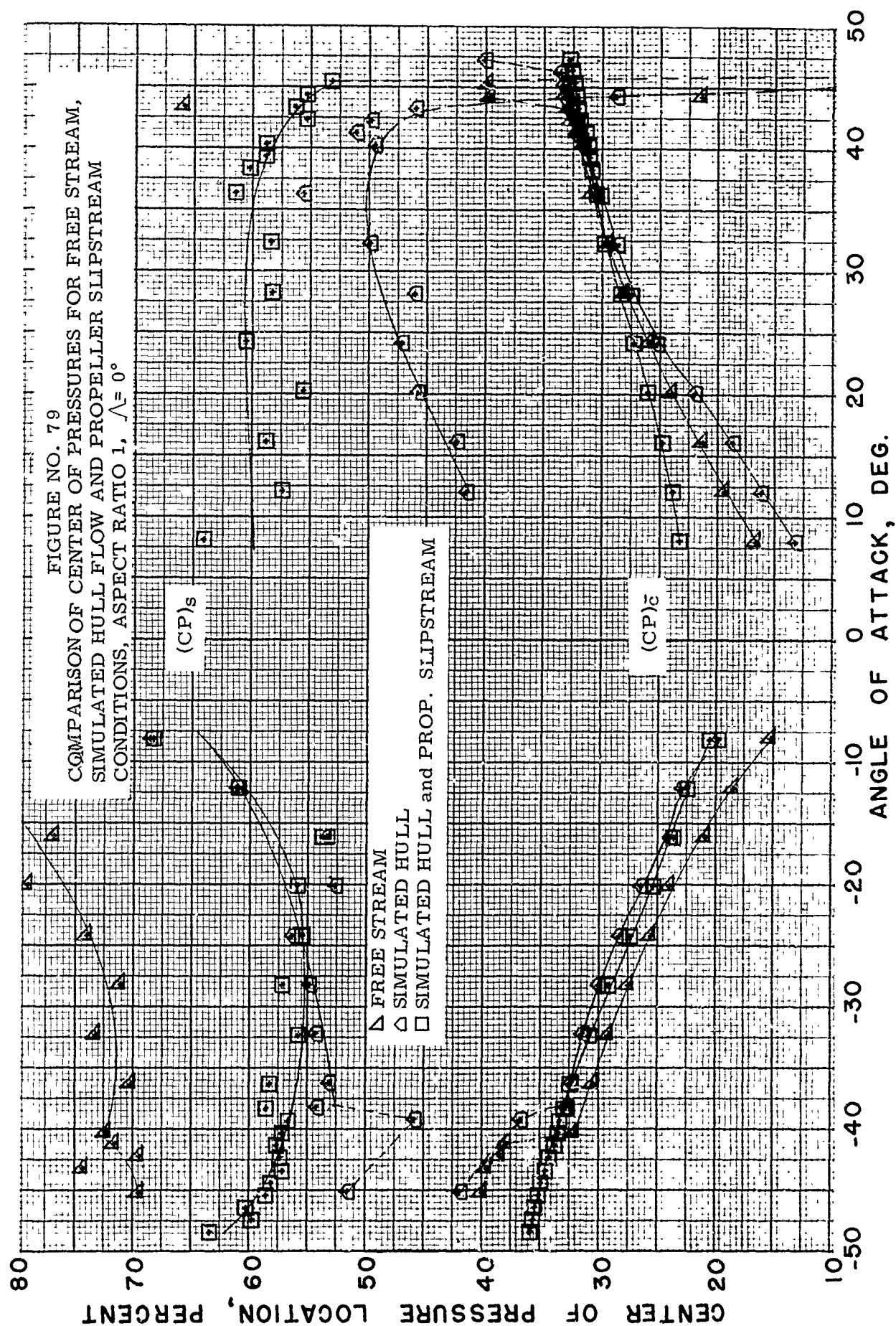
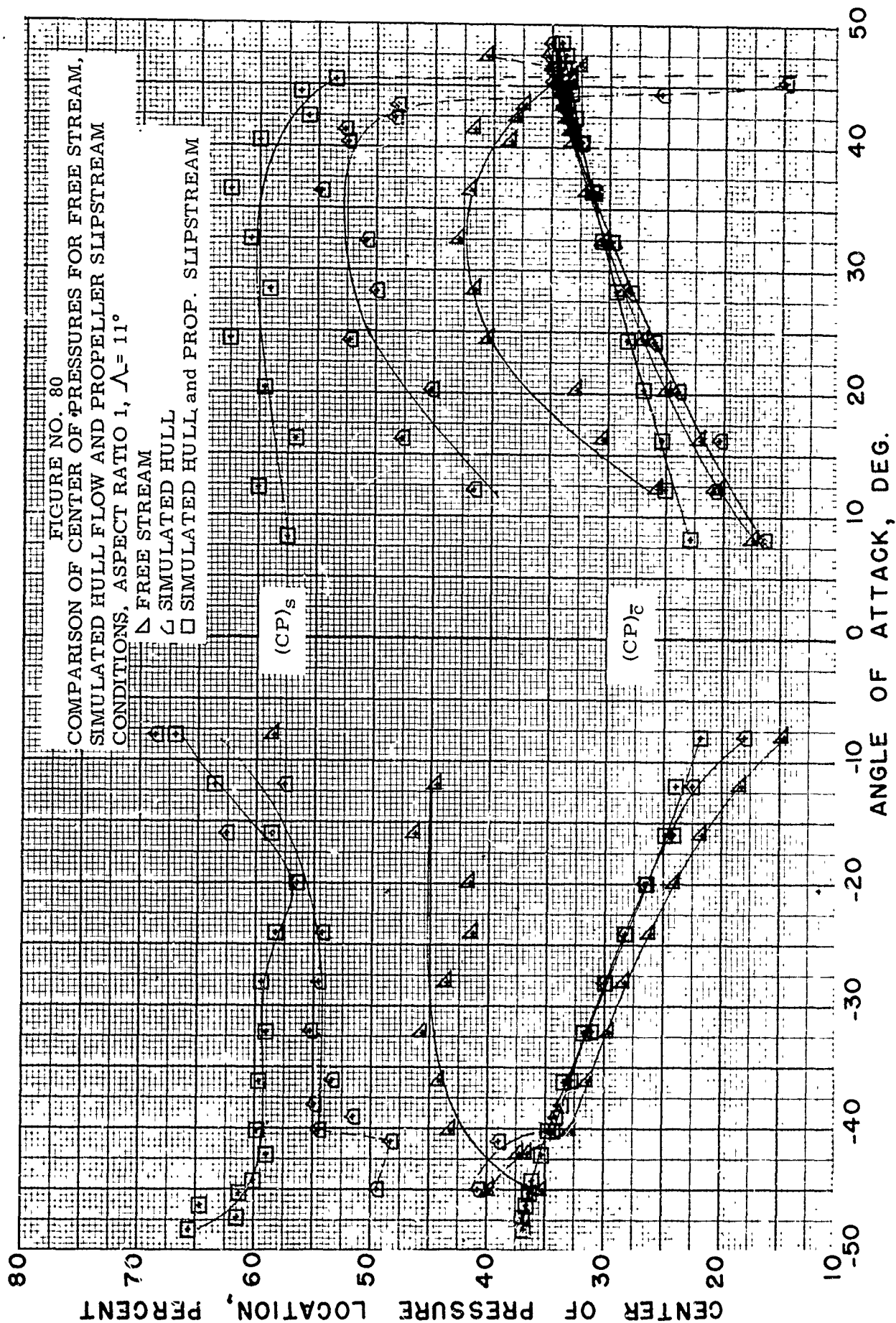
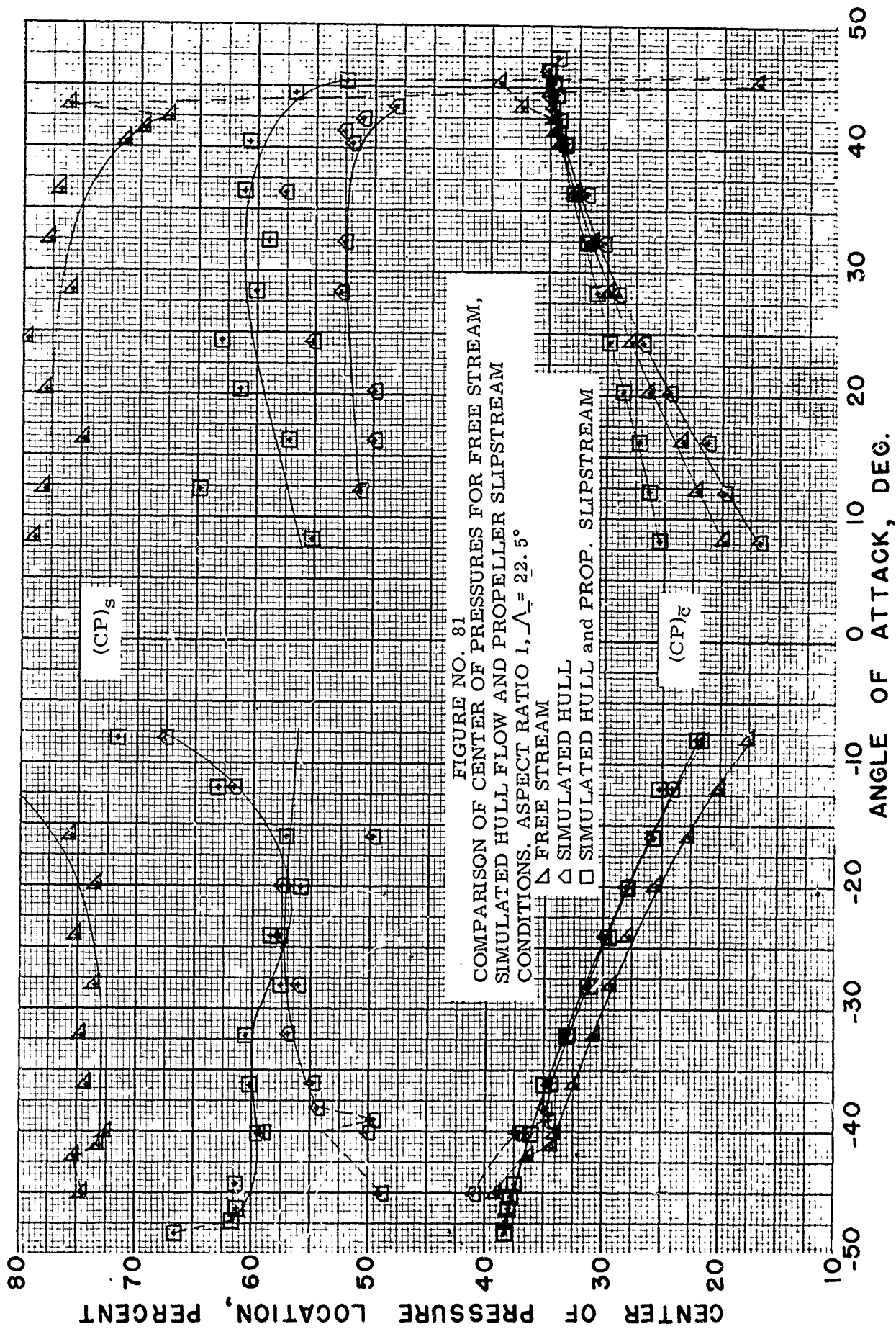


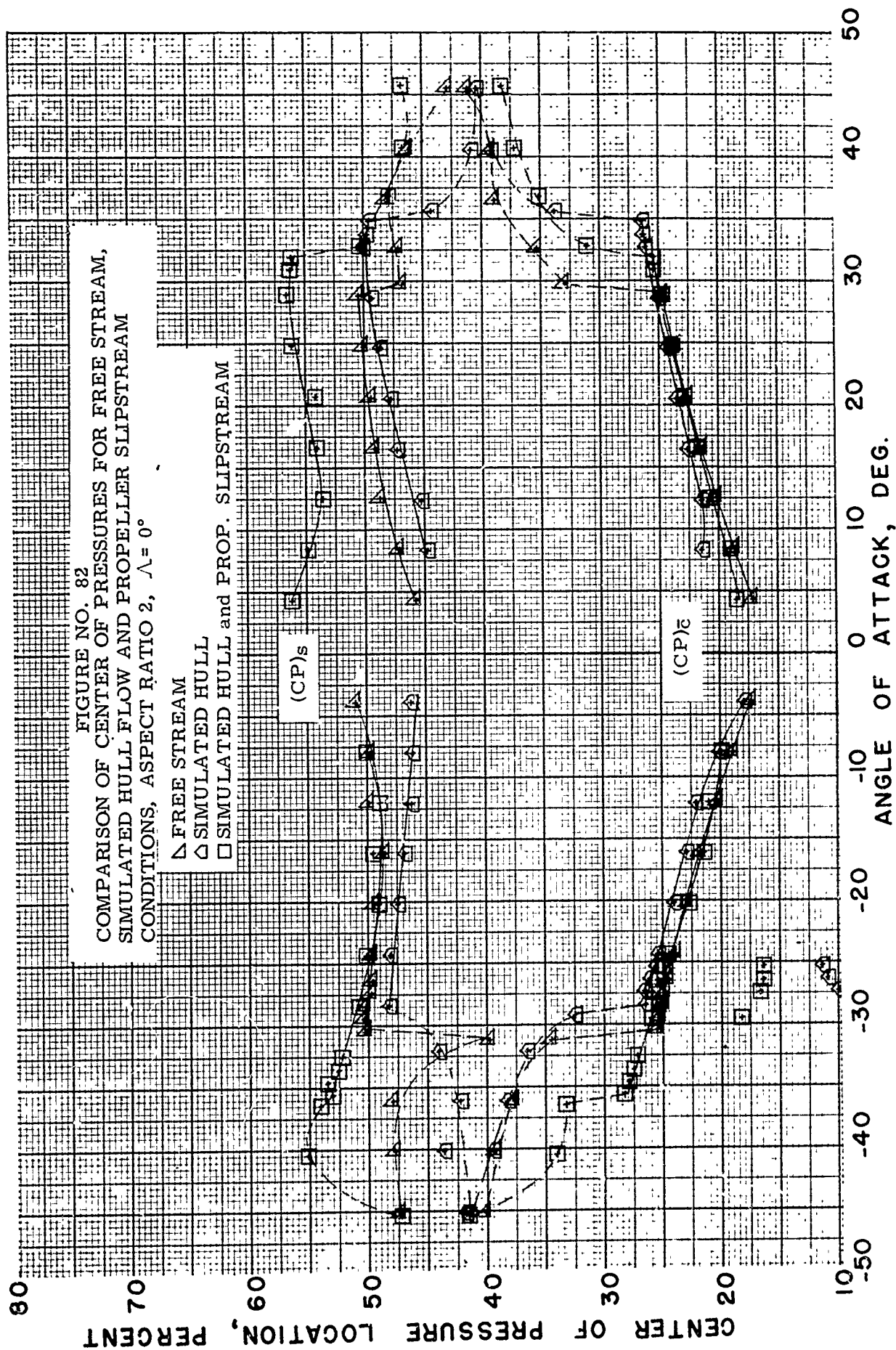
FIGURE NO. 78
COMPARISON OF DRAG COEFFICIENTS FOR FREE STREAM,
SIMULATED HULL FLOW AND PROPELLER SLIPSTREAM
CONDITIONS, ASPECT RATIO 3, $\Lambda = 22.5^\circ$

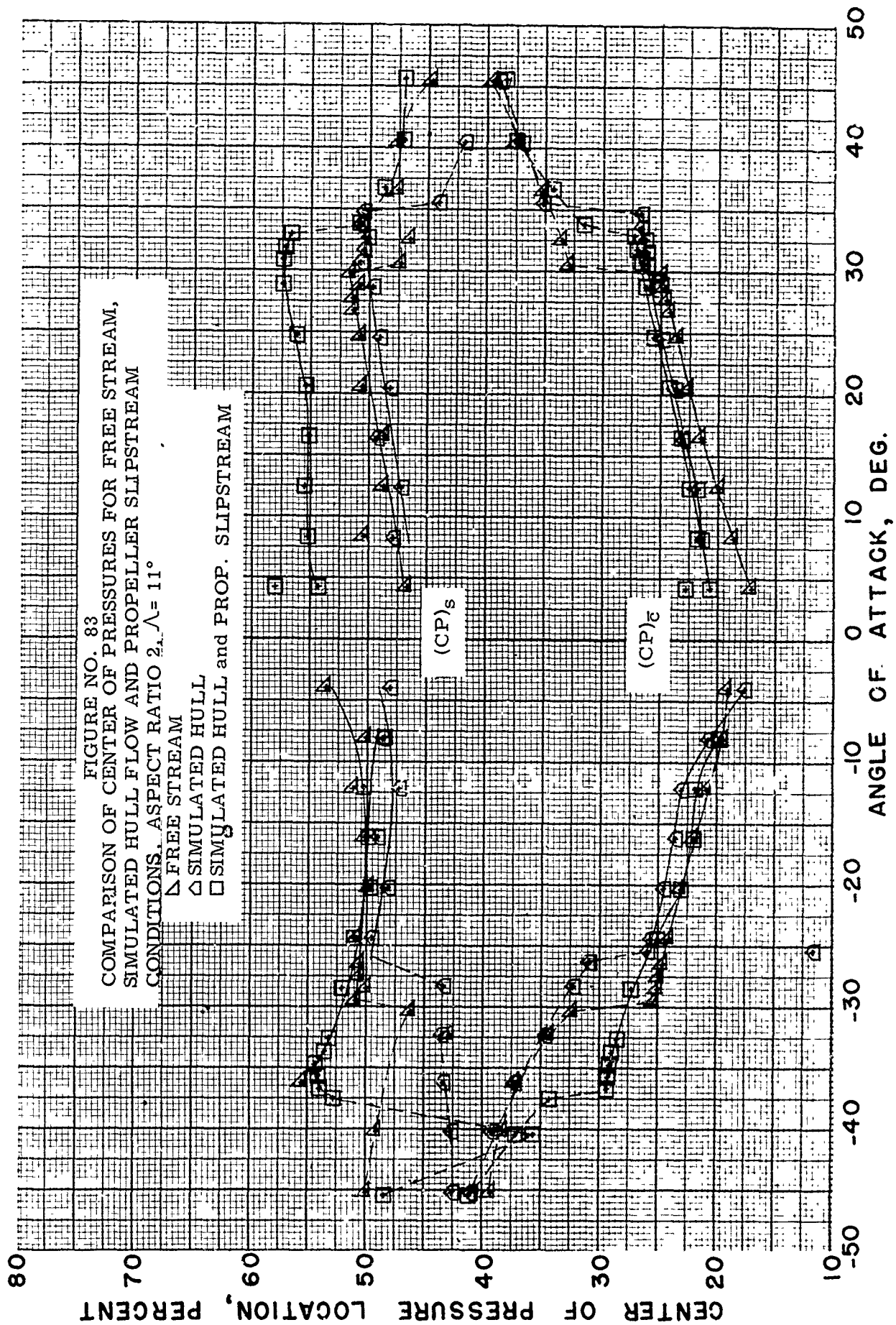


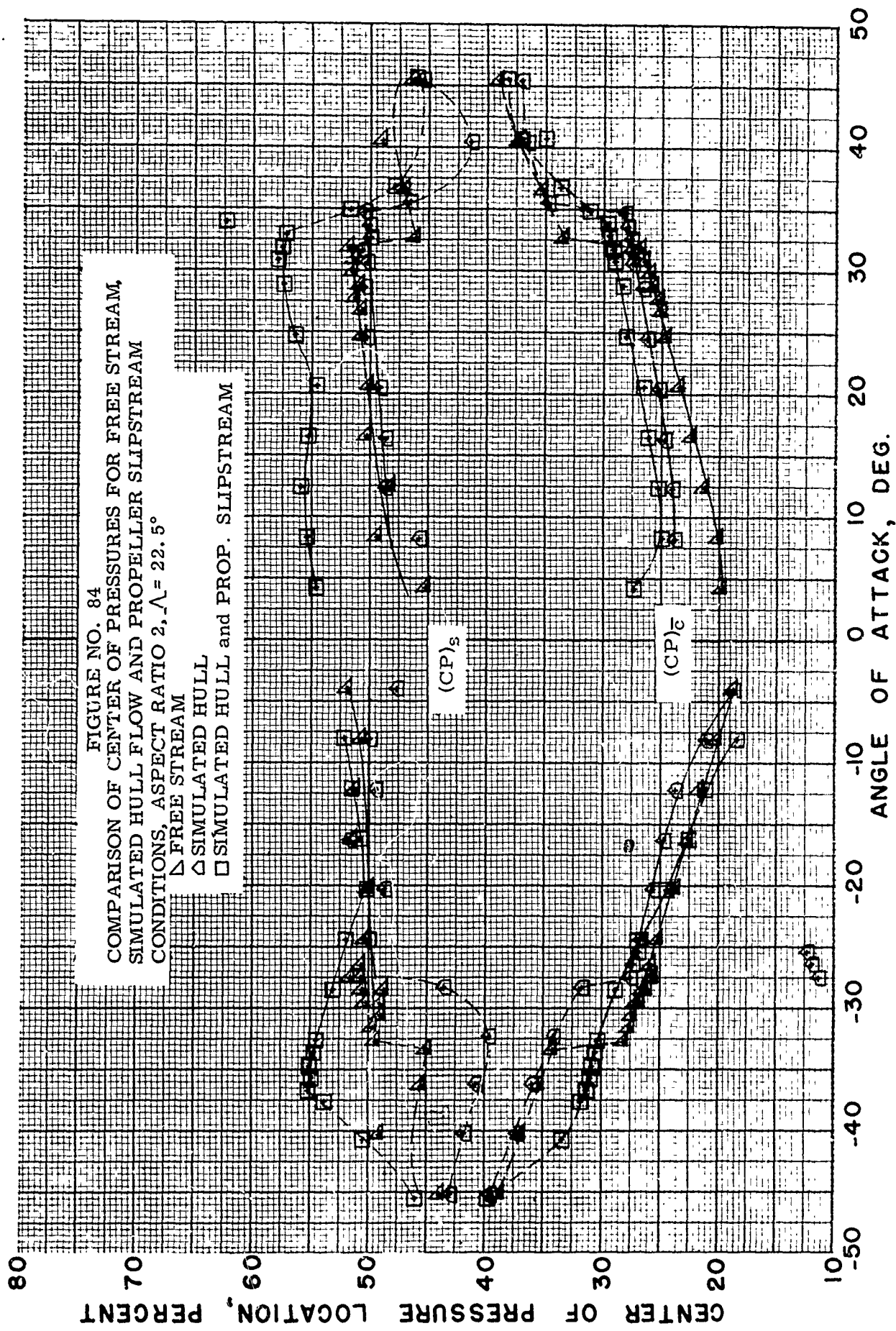


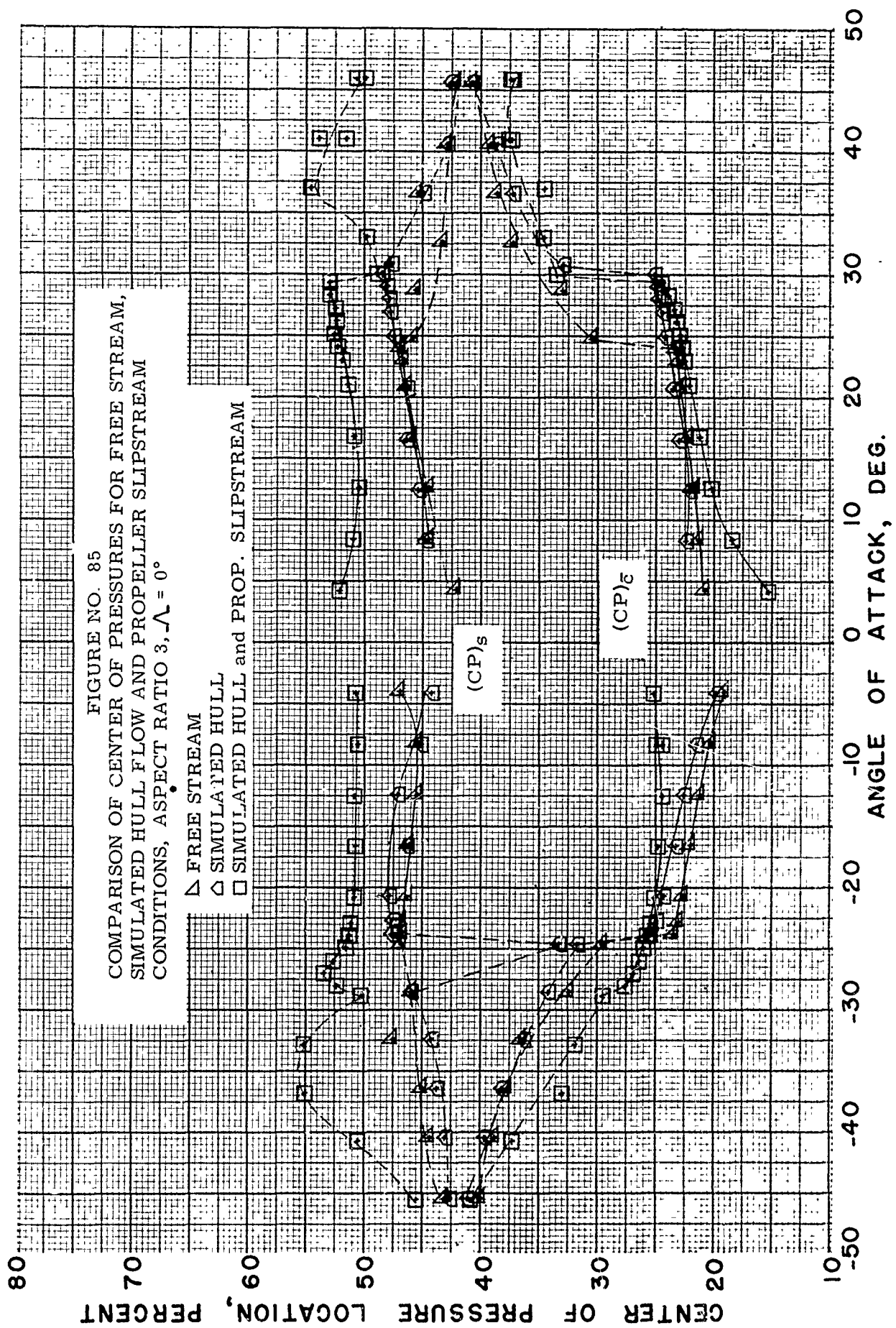


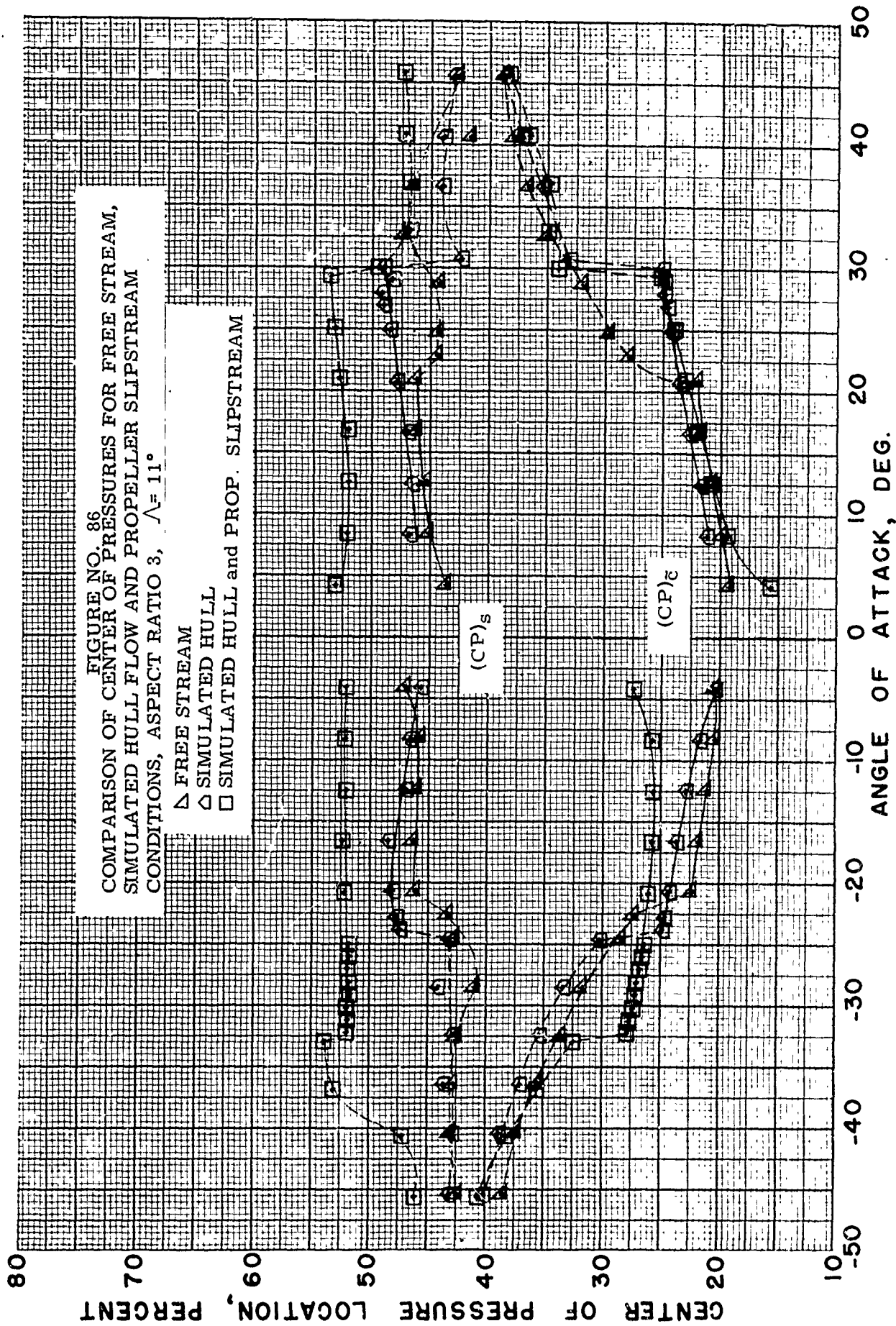


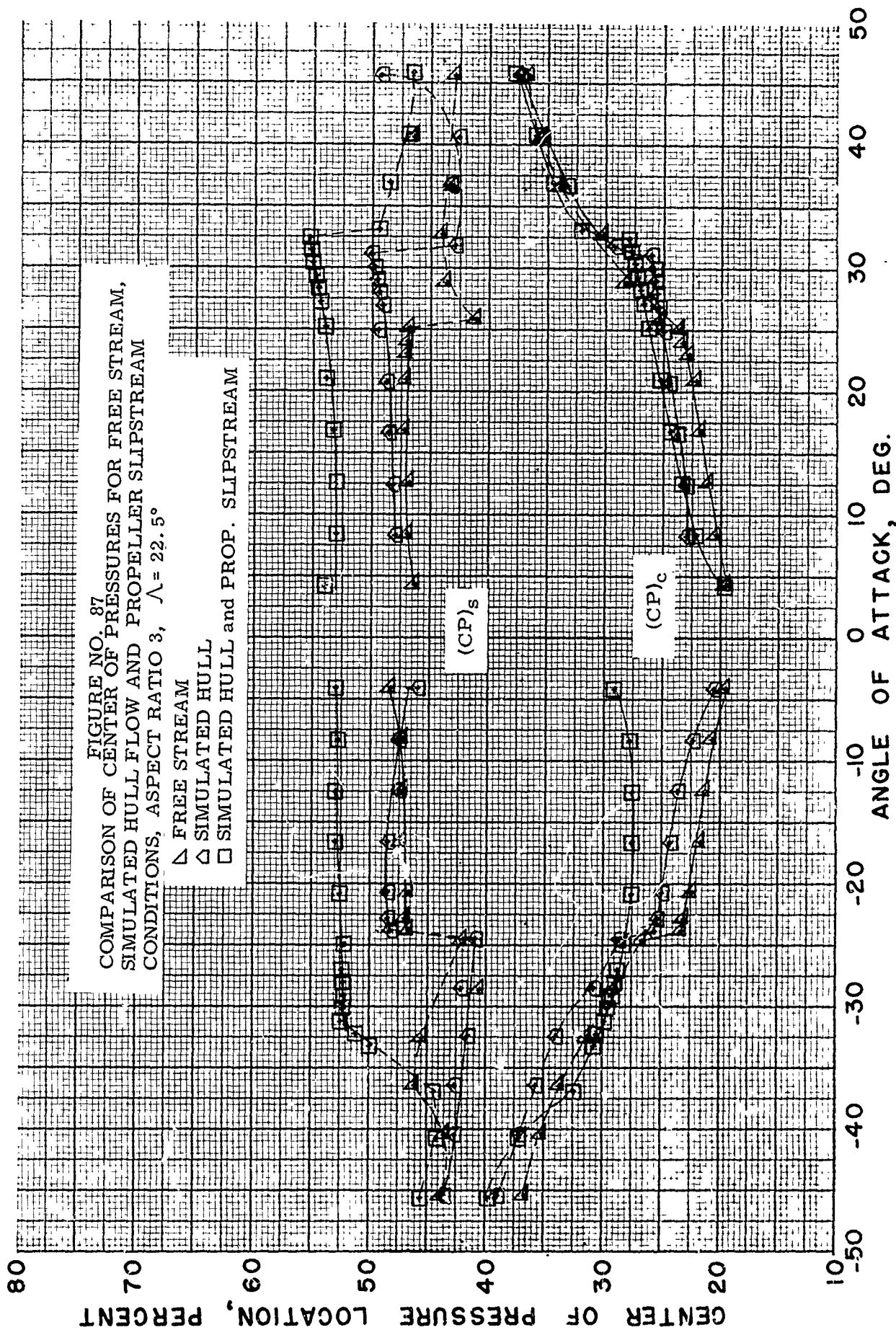






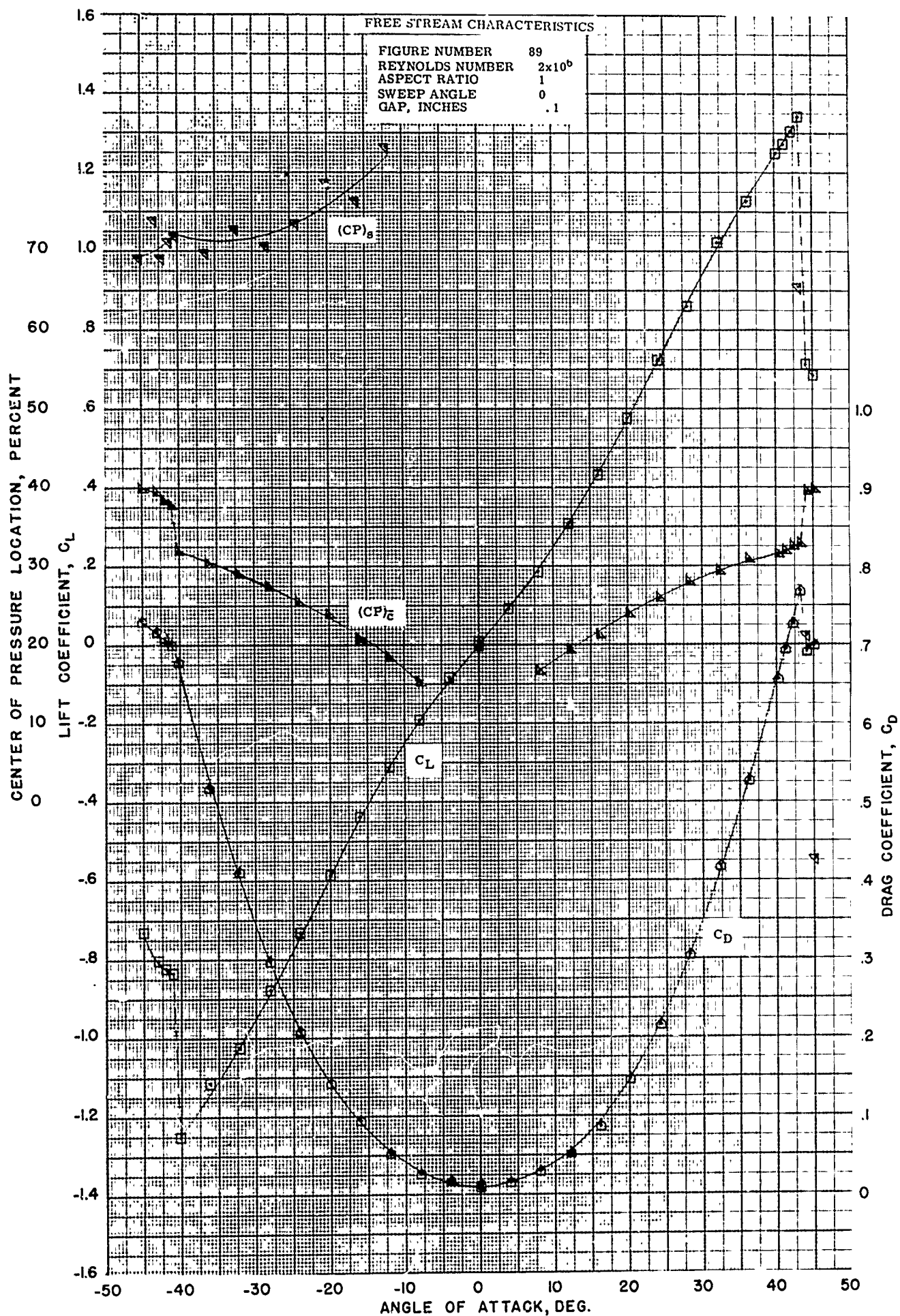


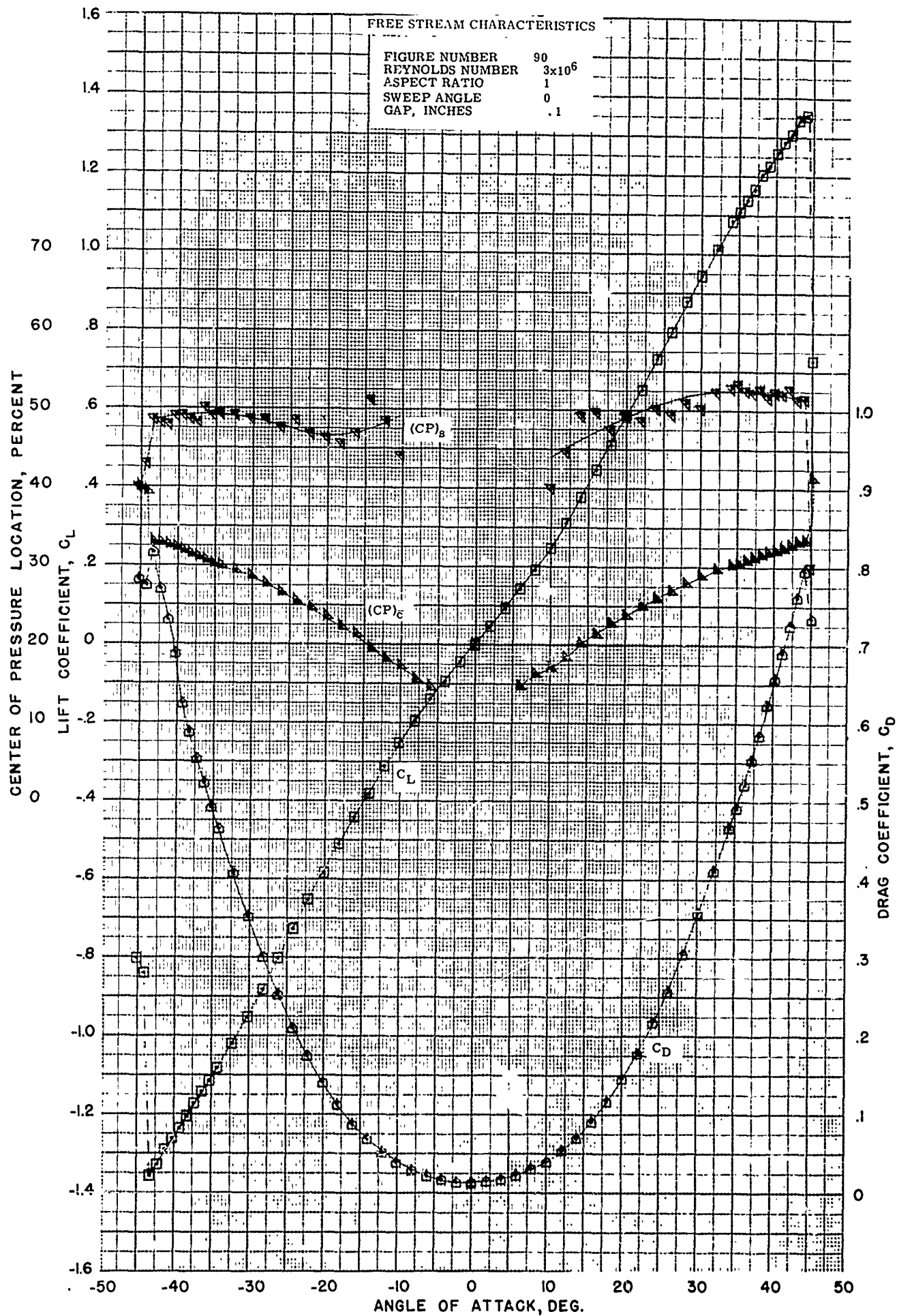


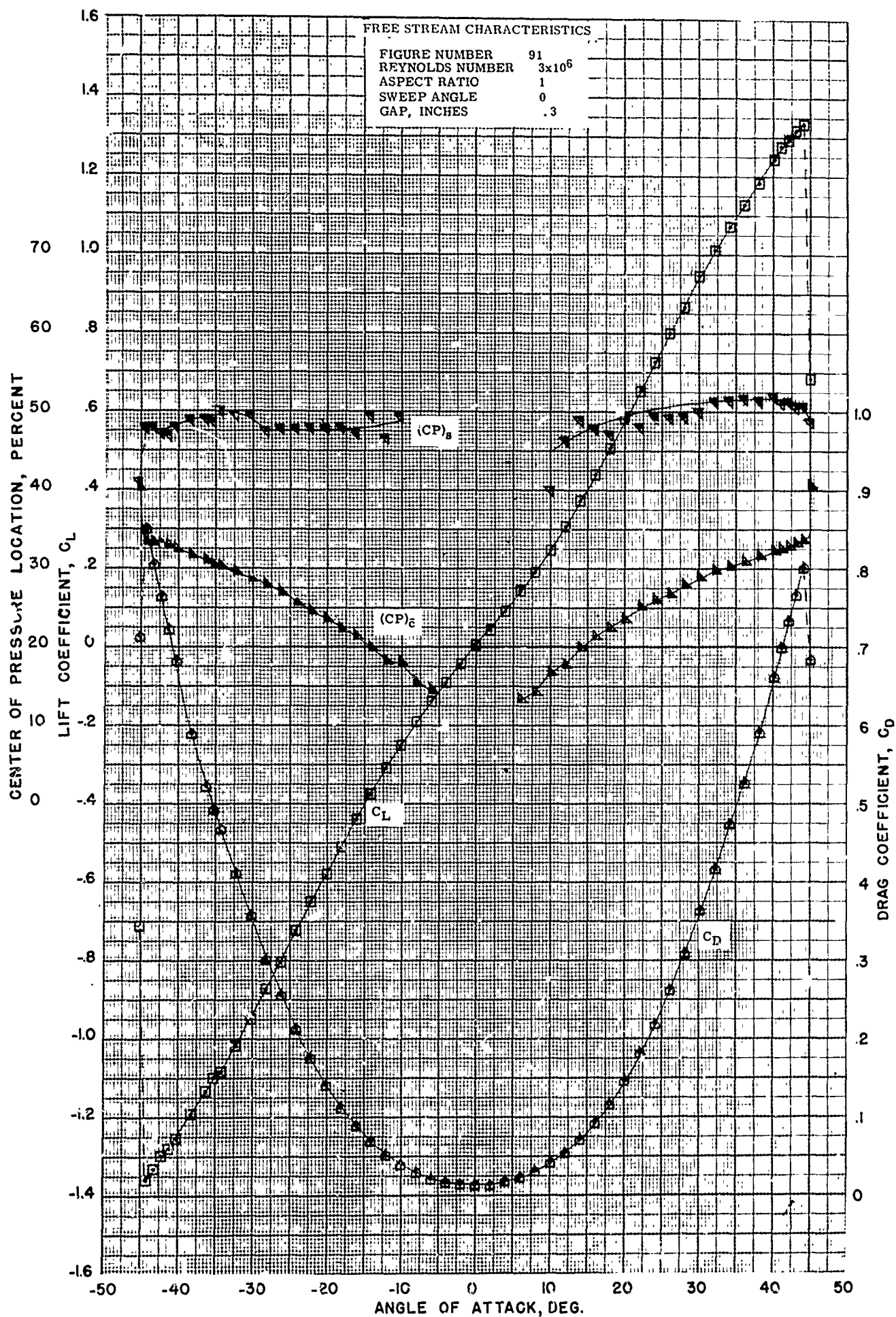


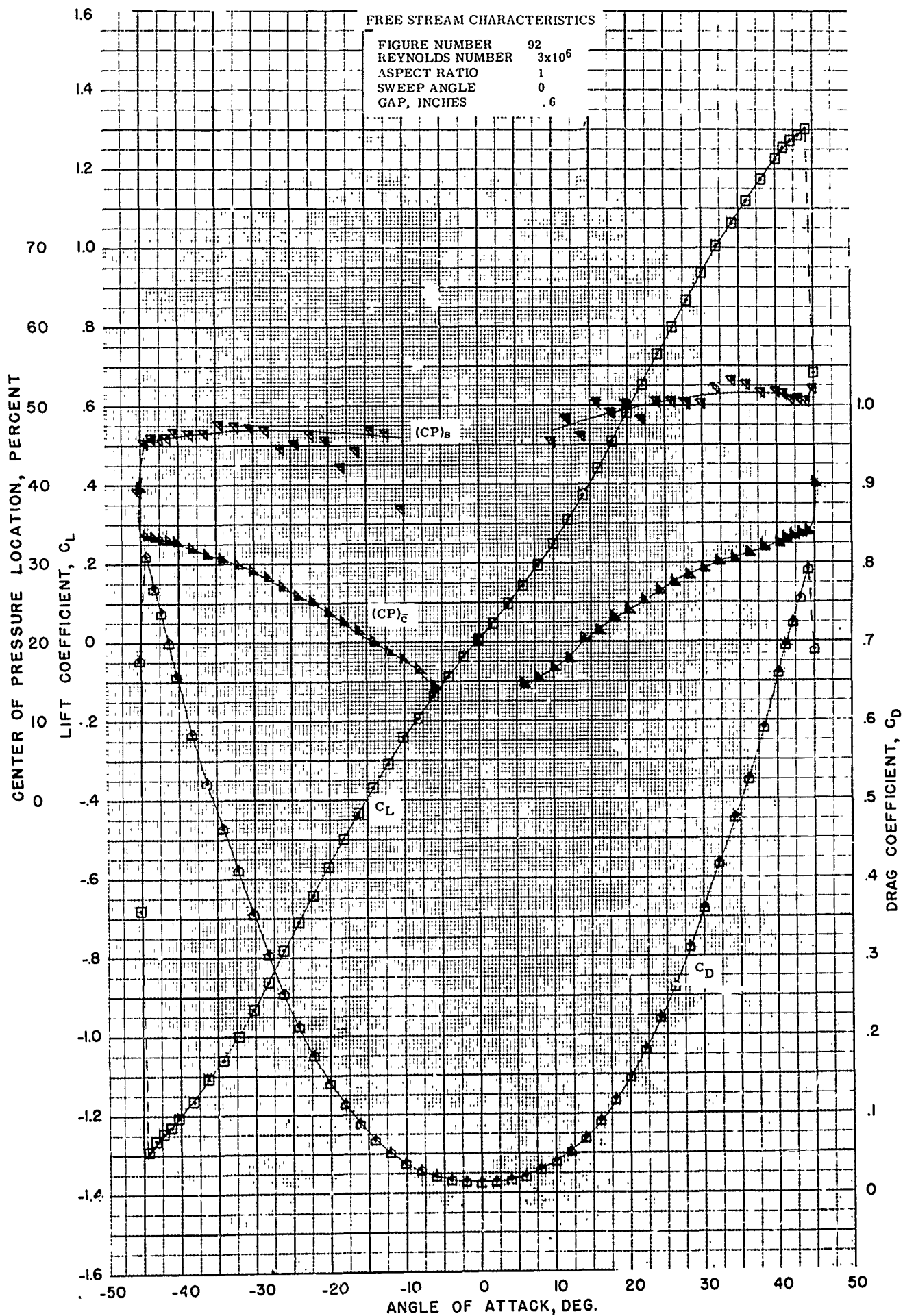
APPENDIX A

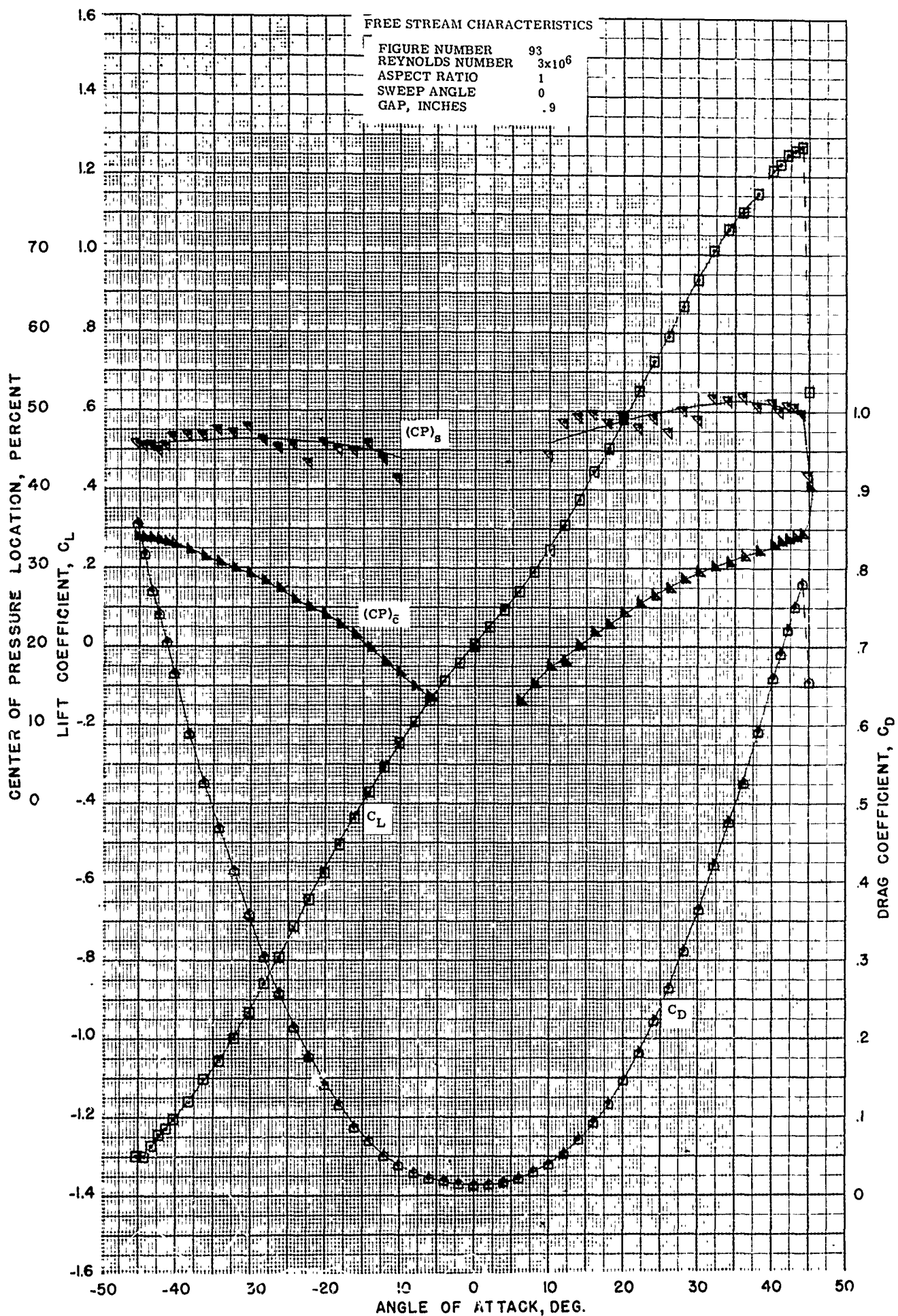
Free Stream Characteristics For Various
Gap Sizes

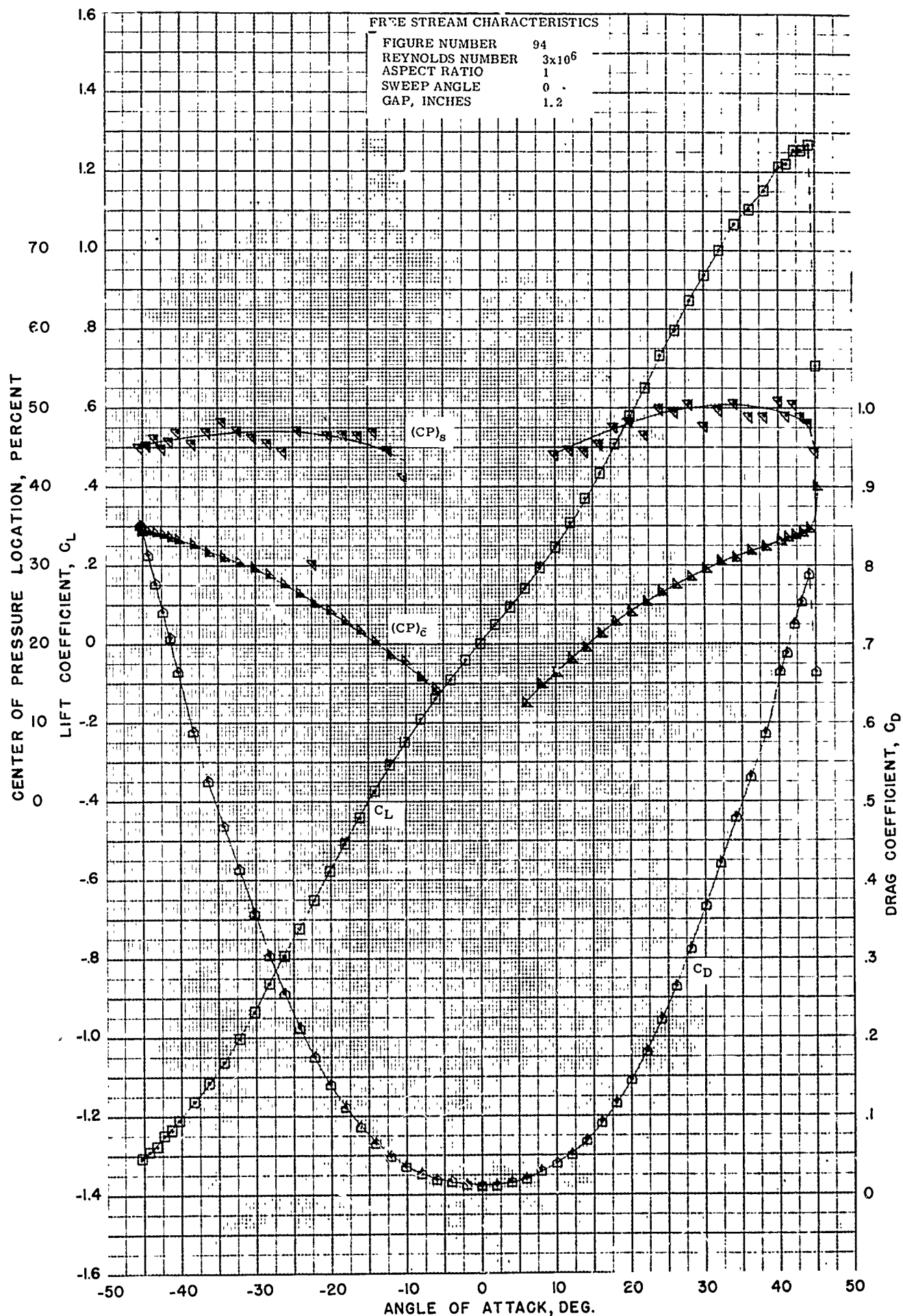


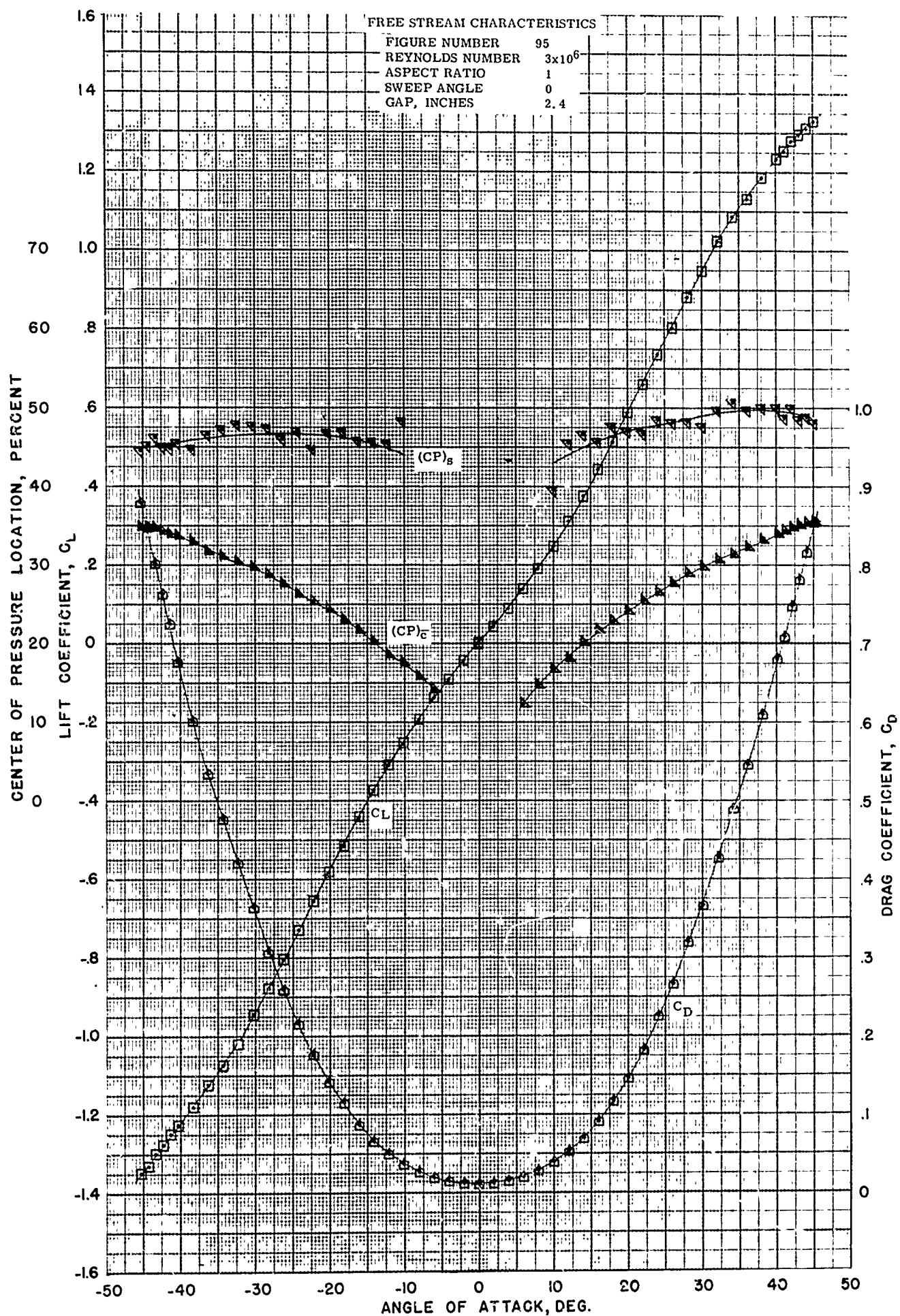


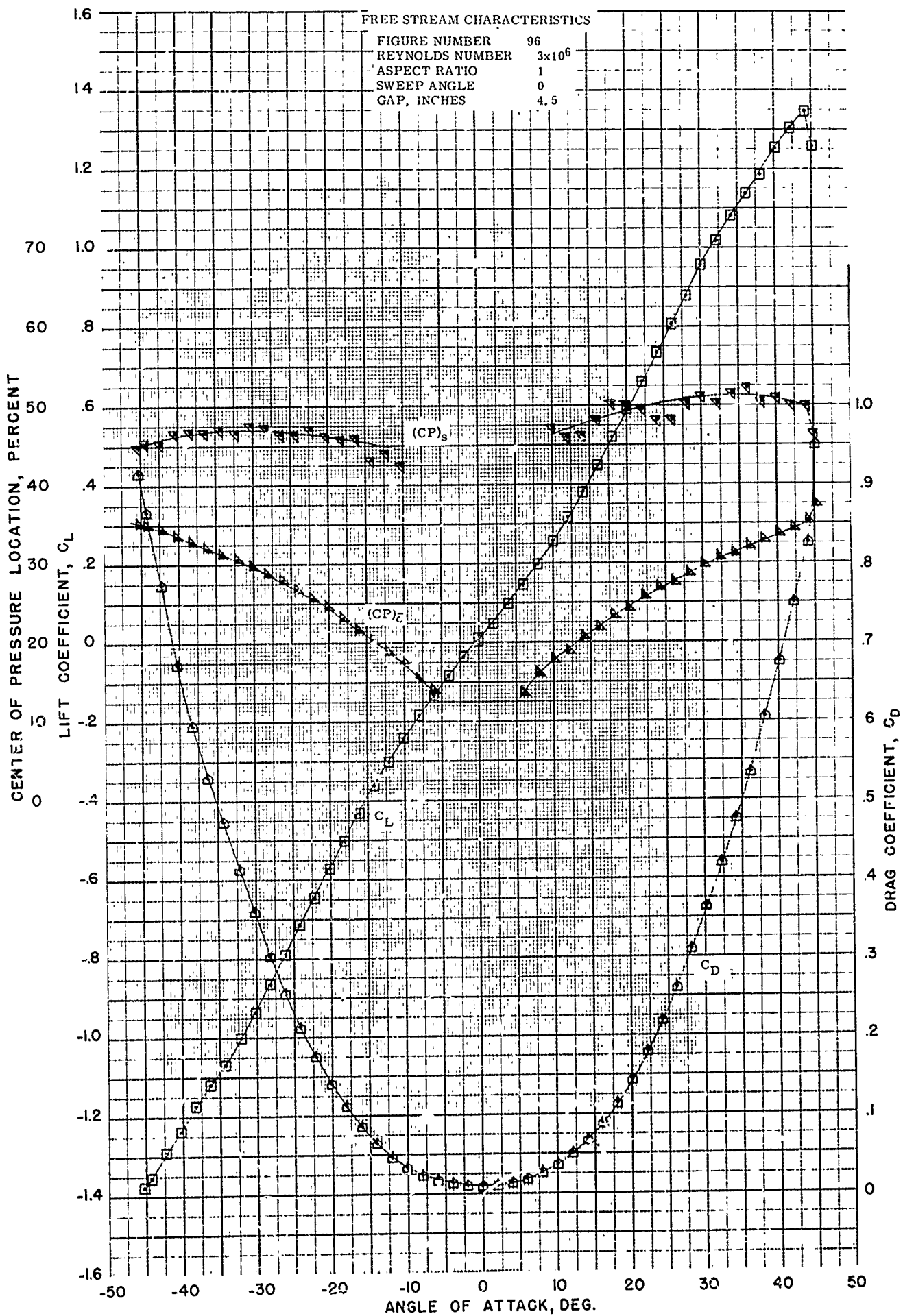


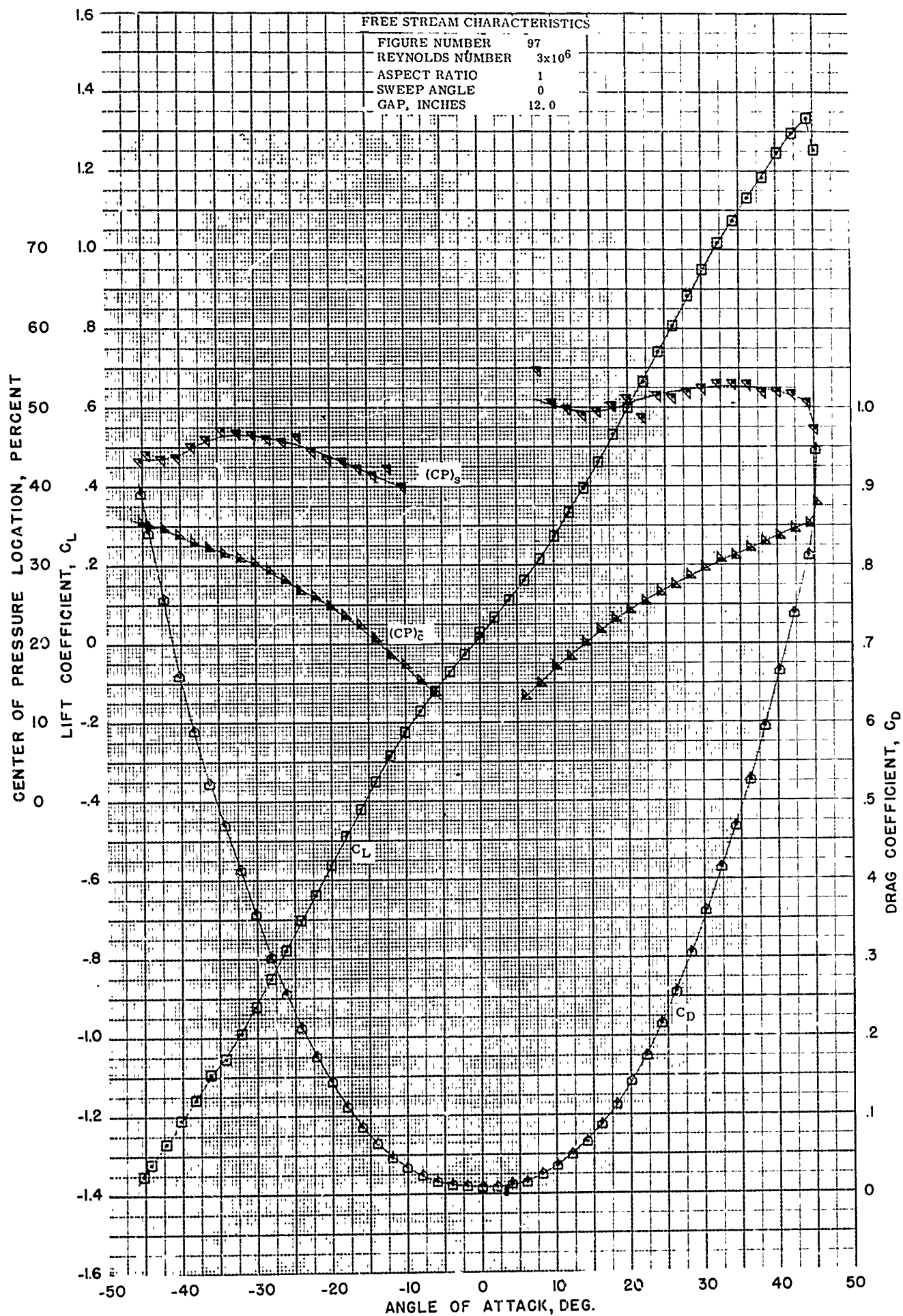


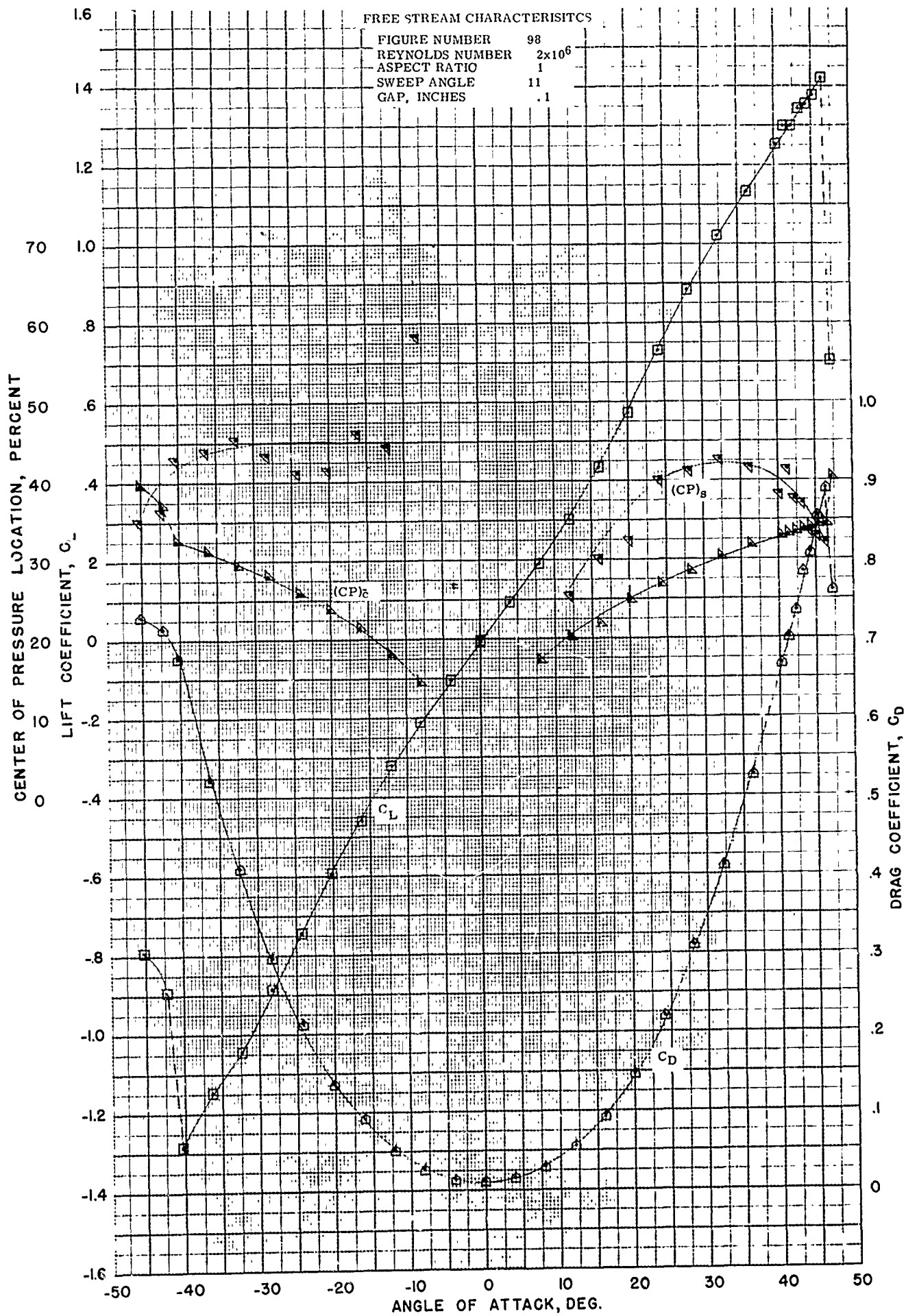


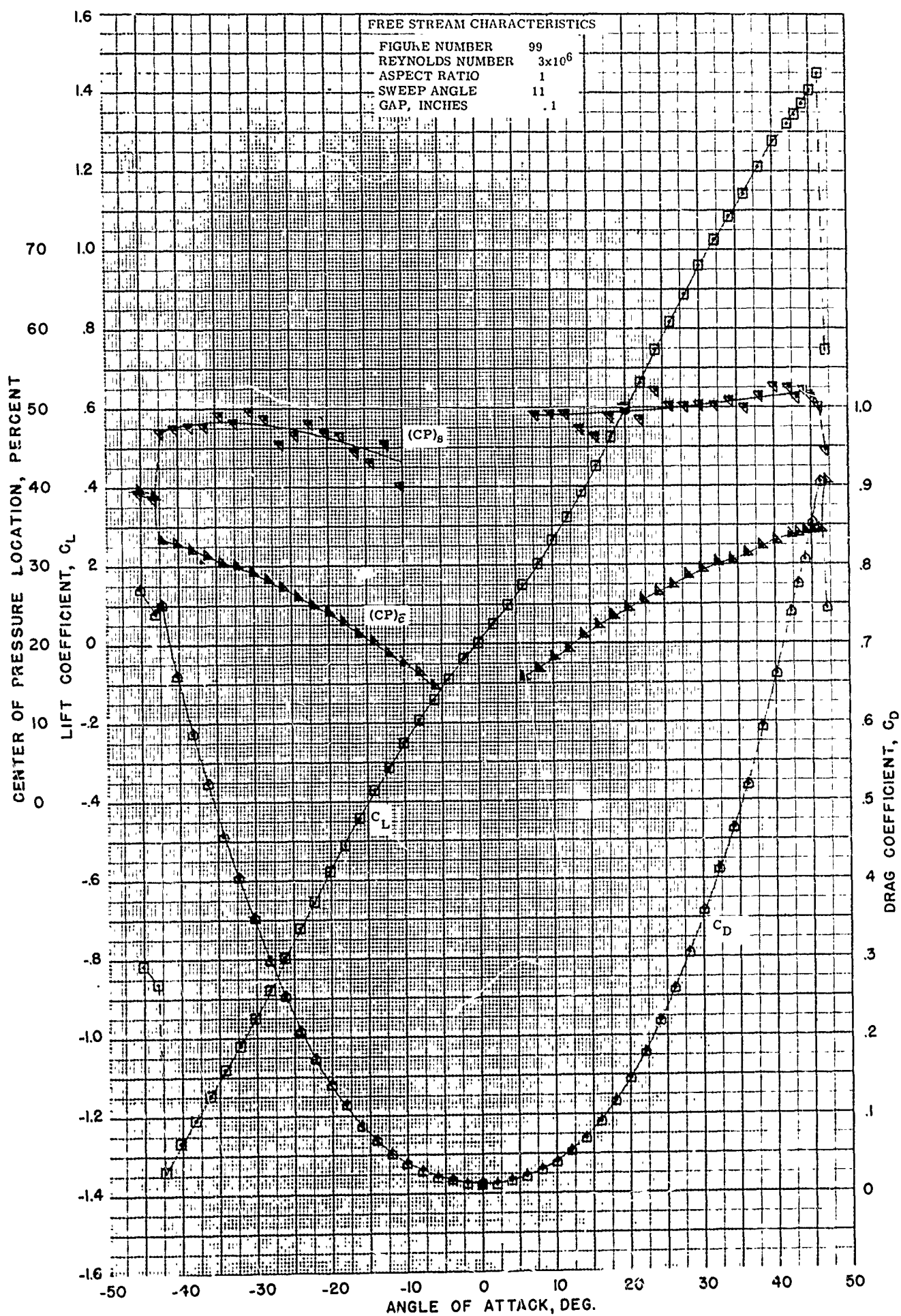


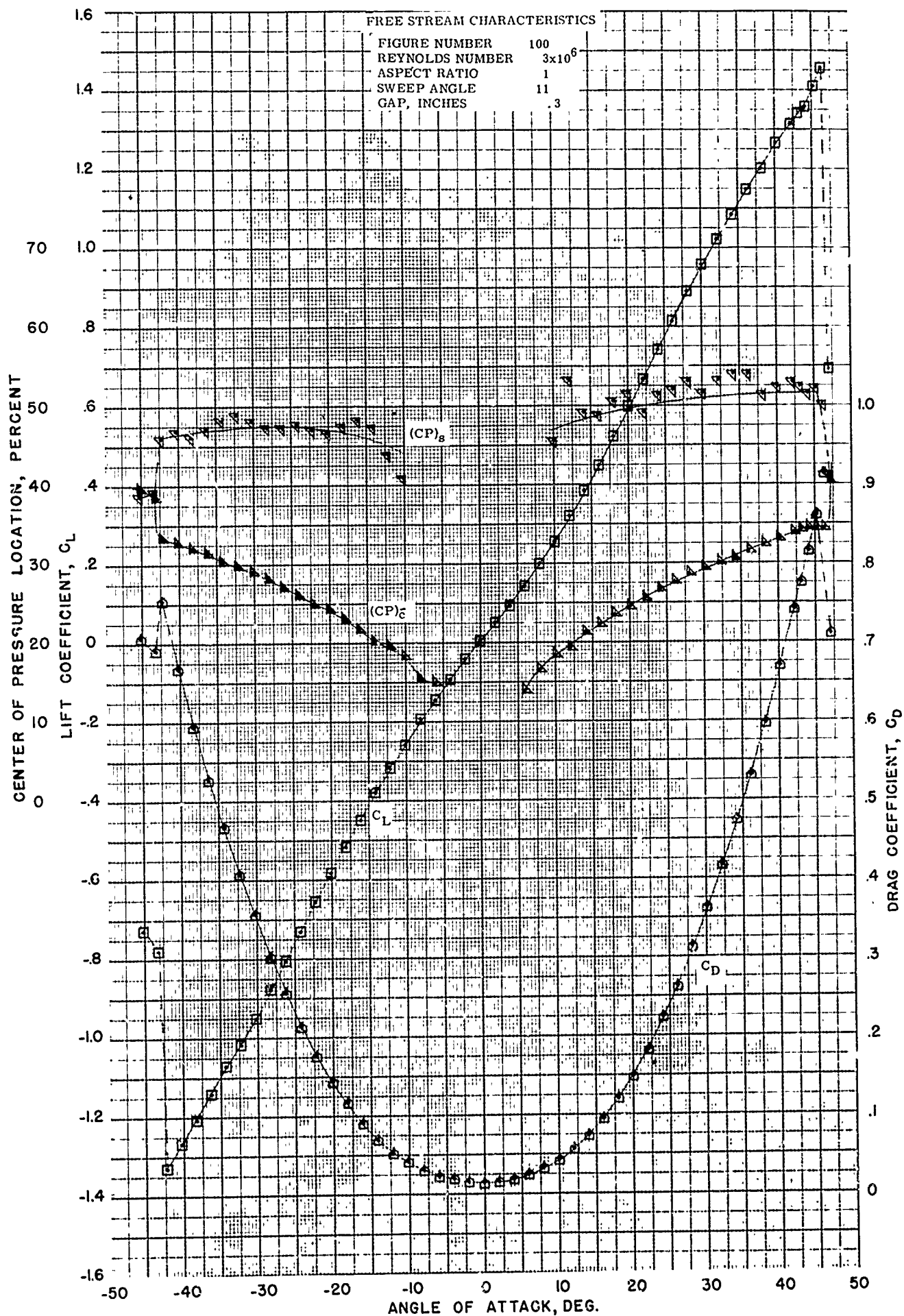


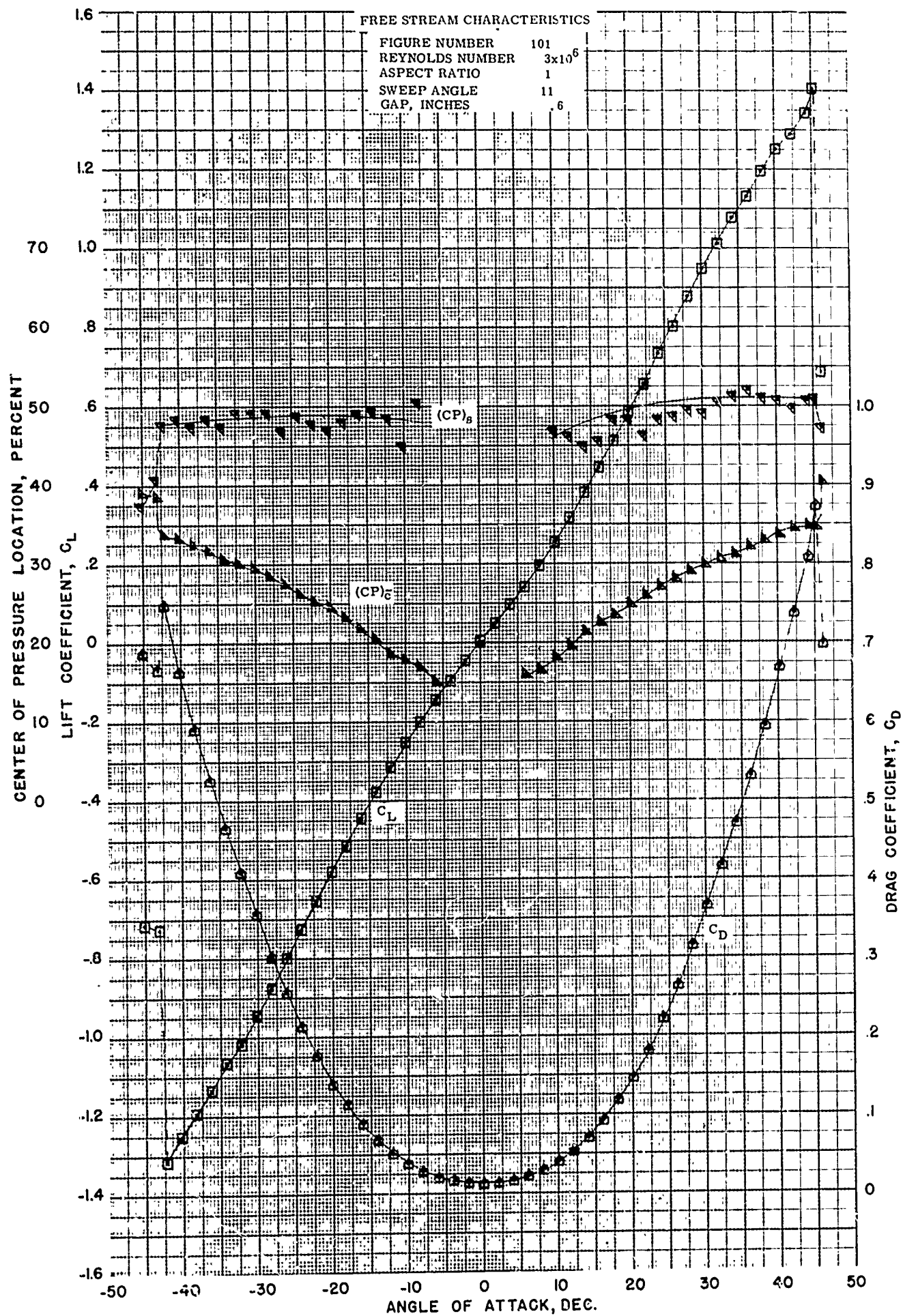


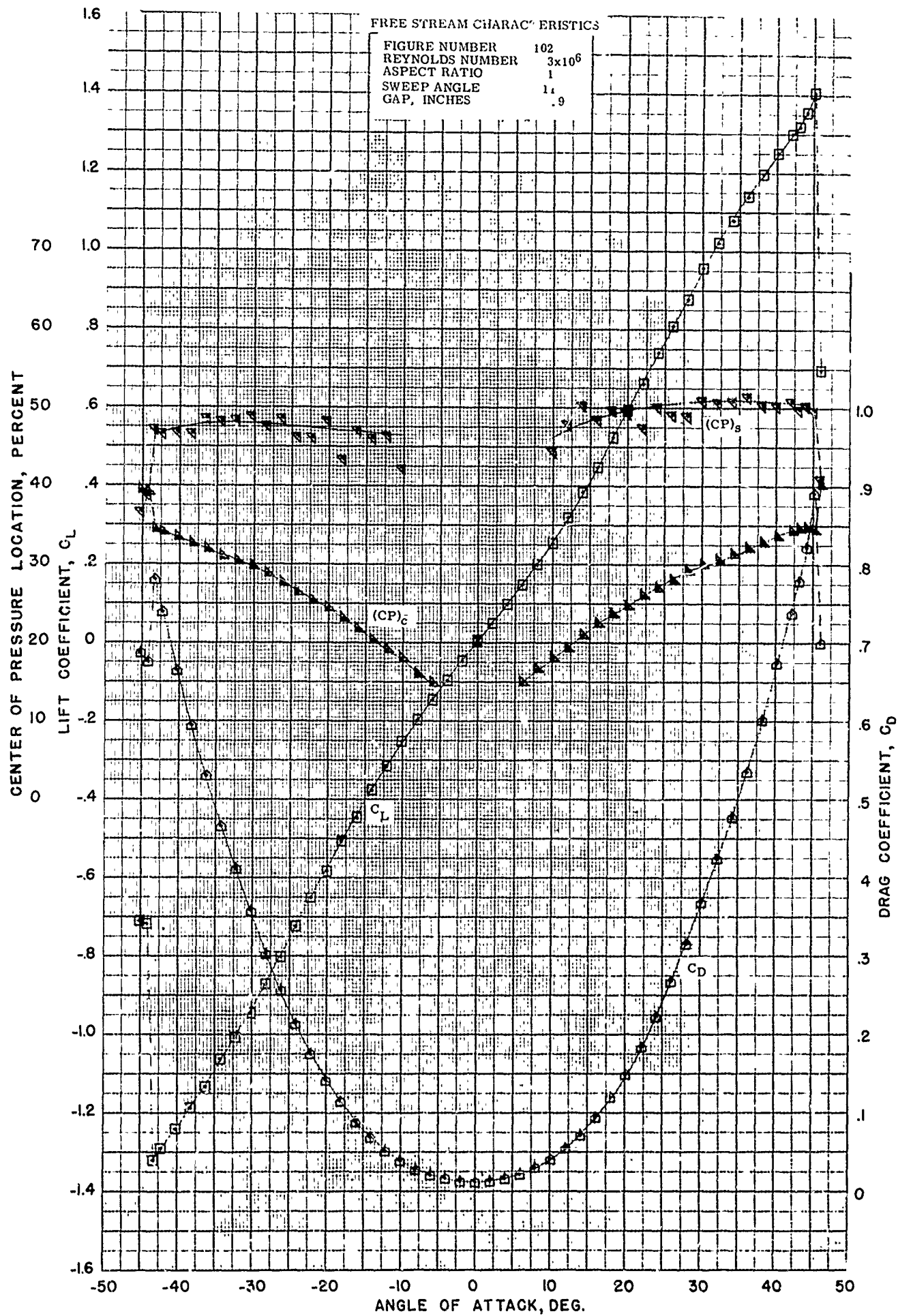


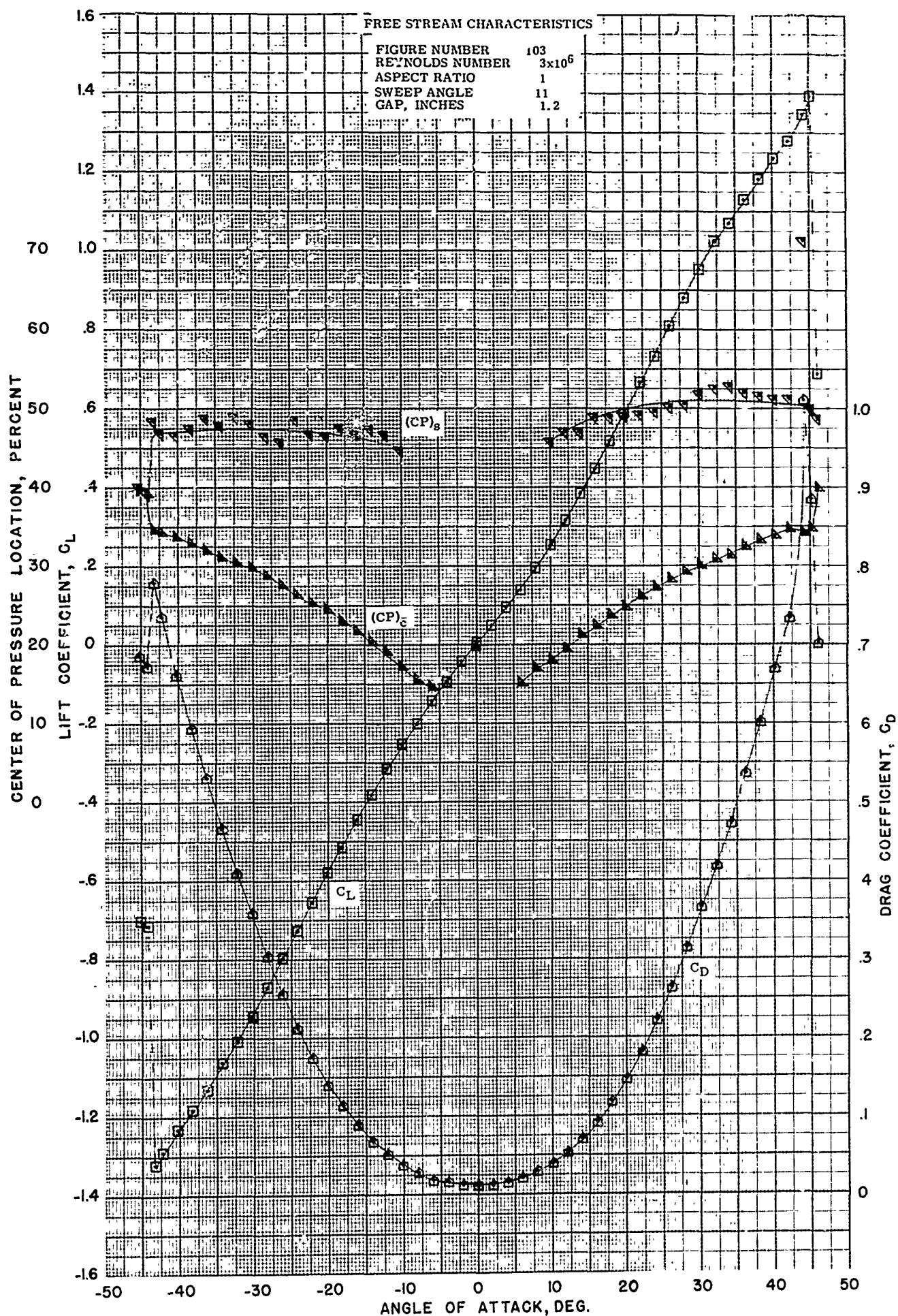


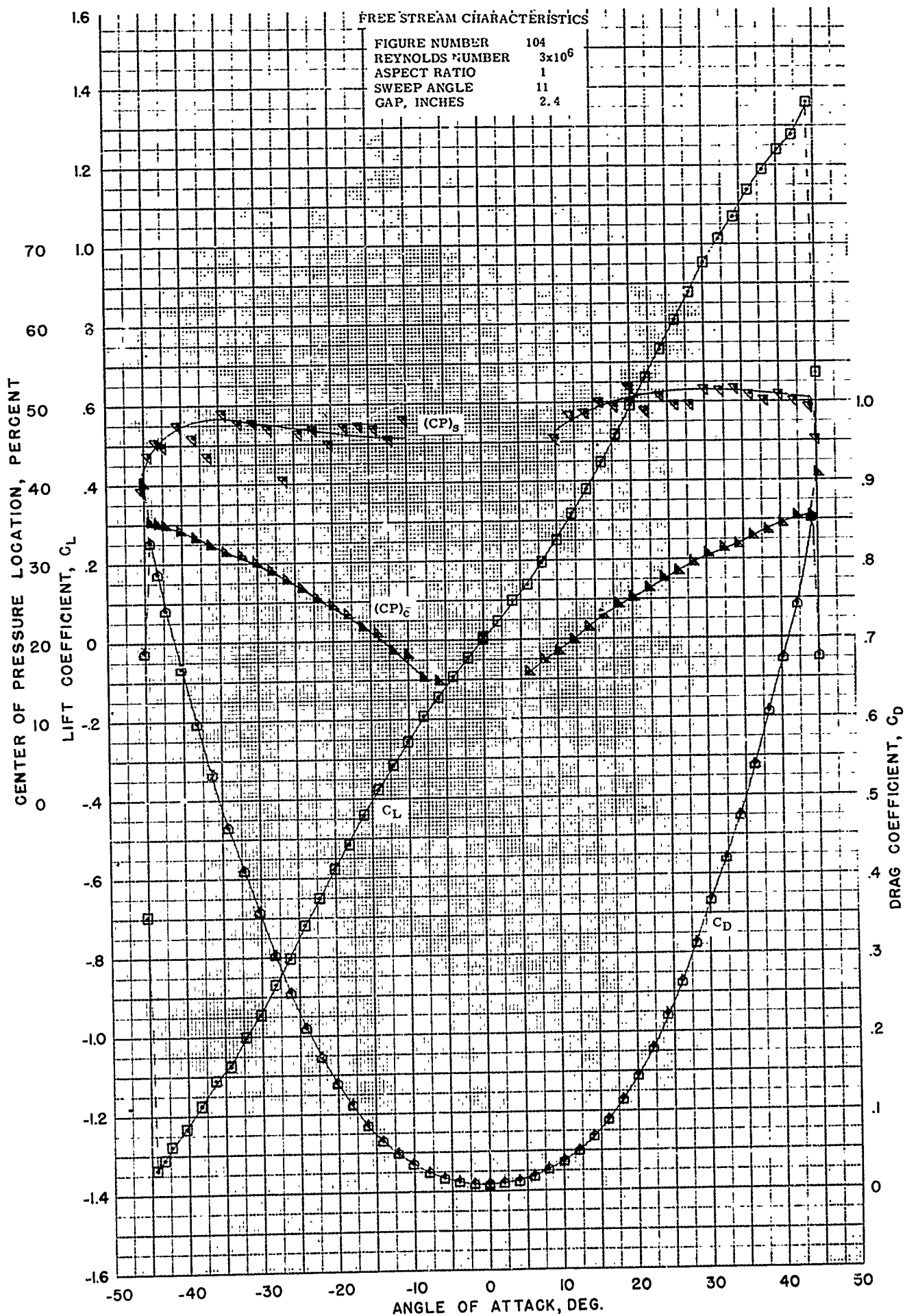


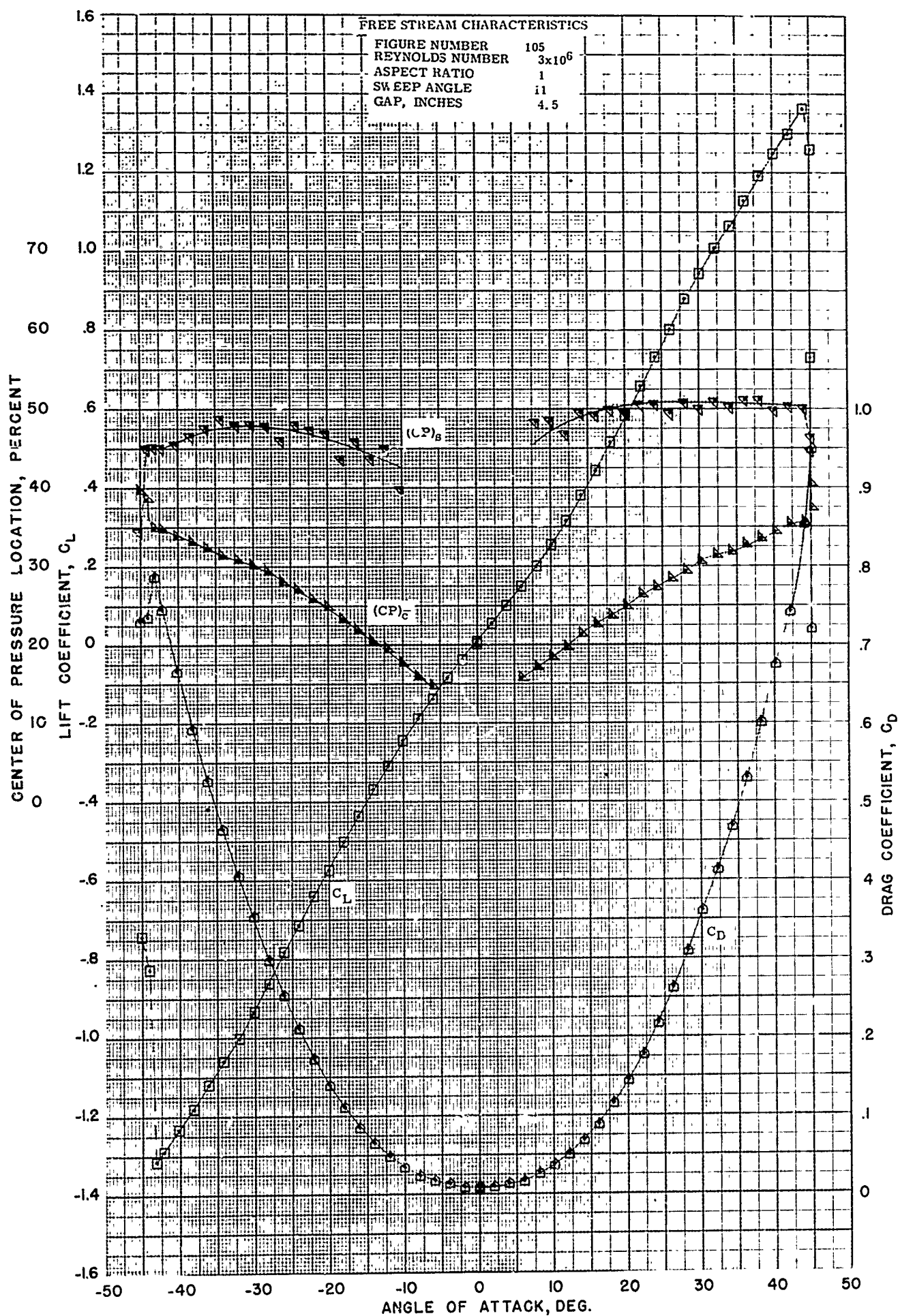


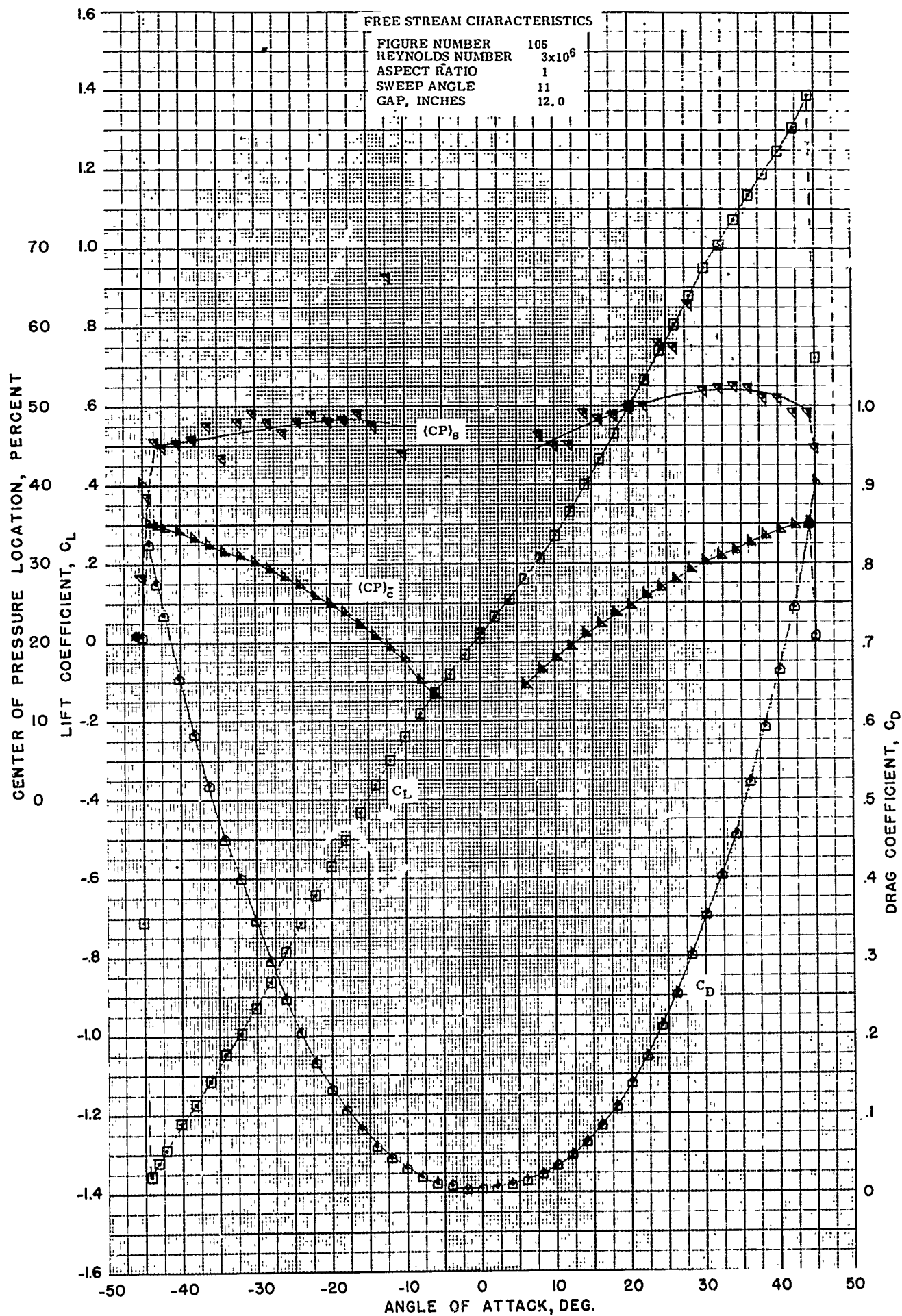


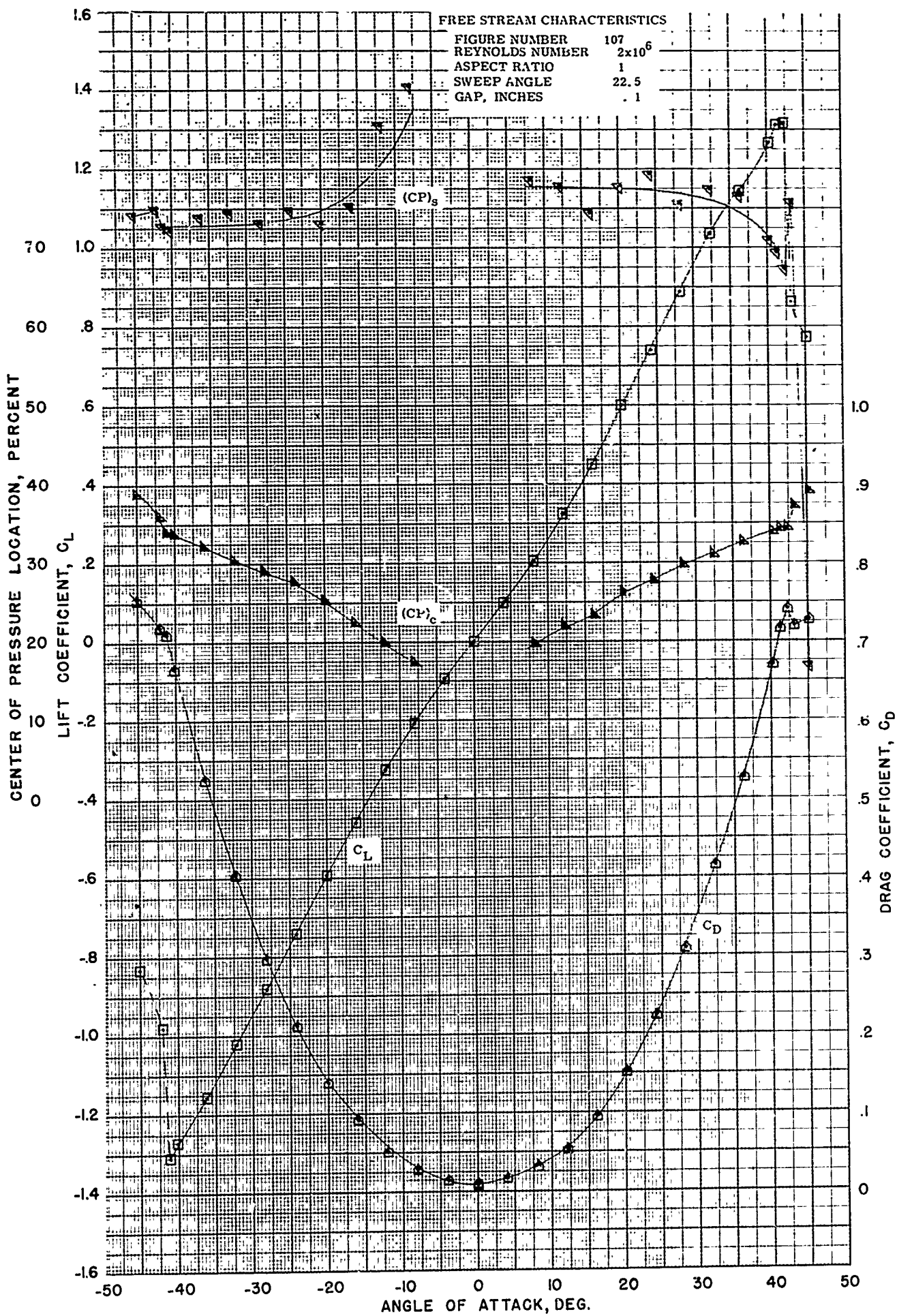


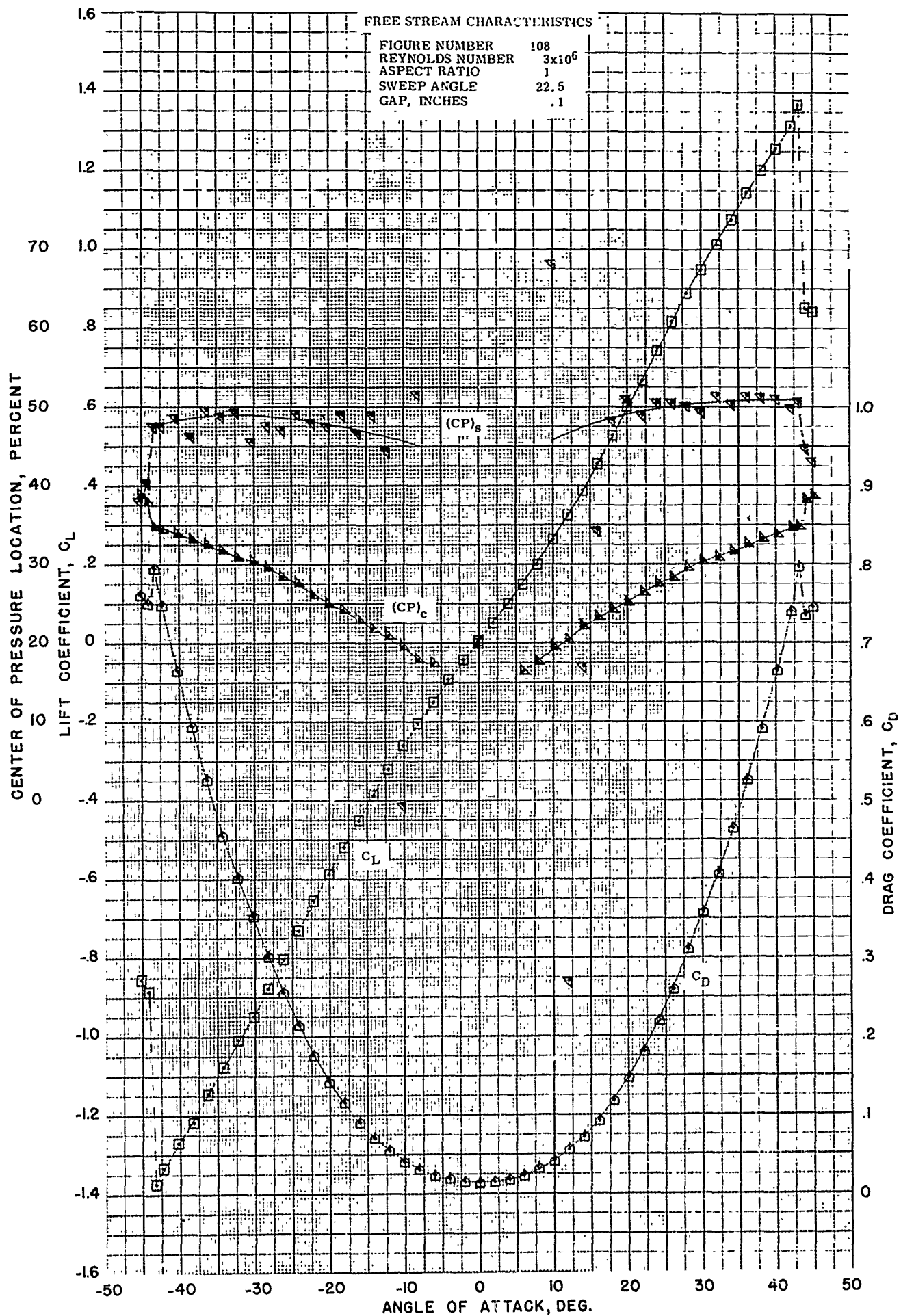


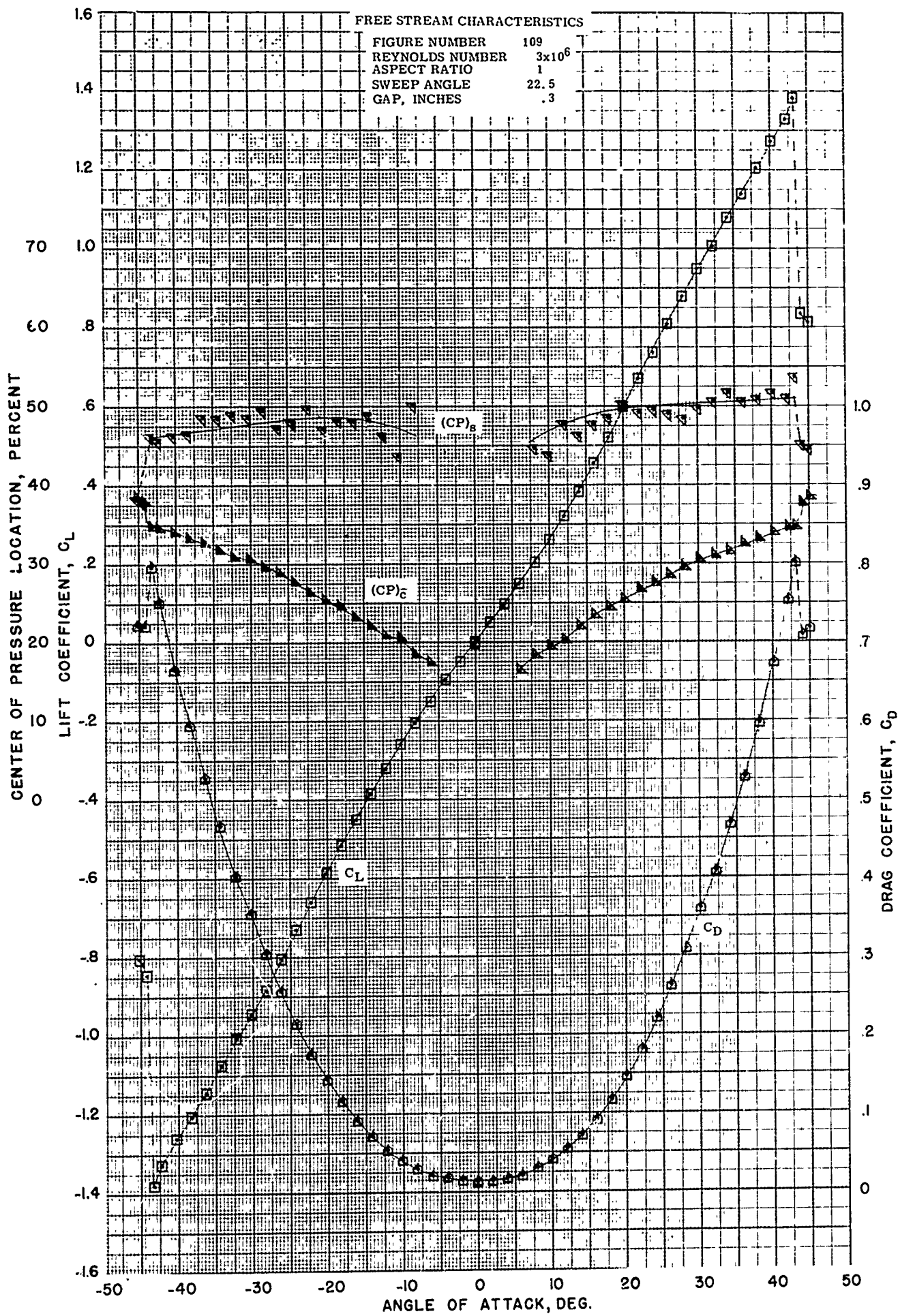


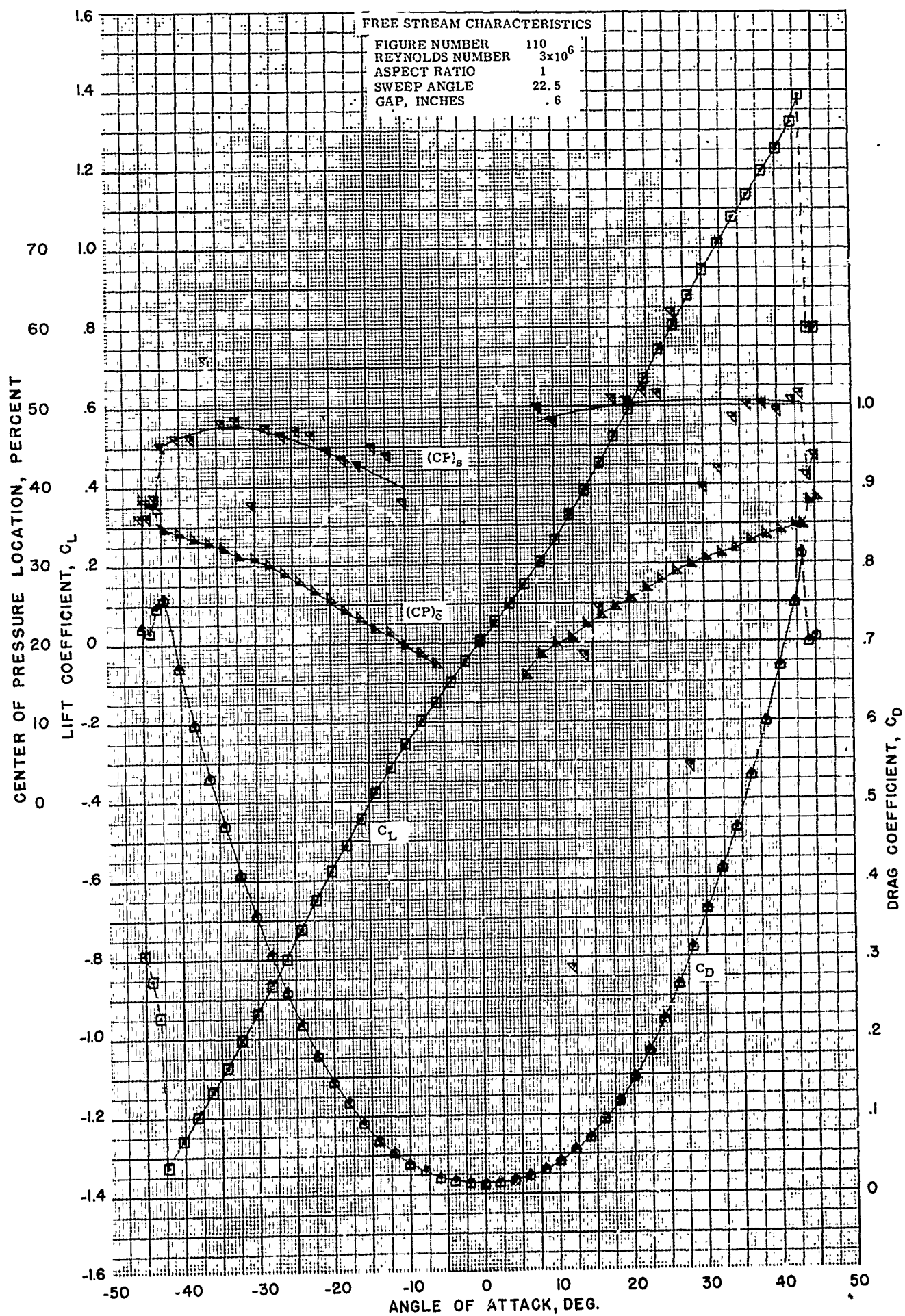


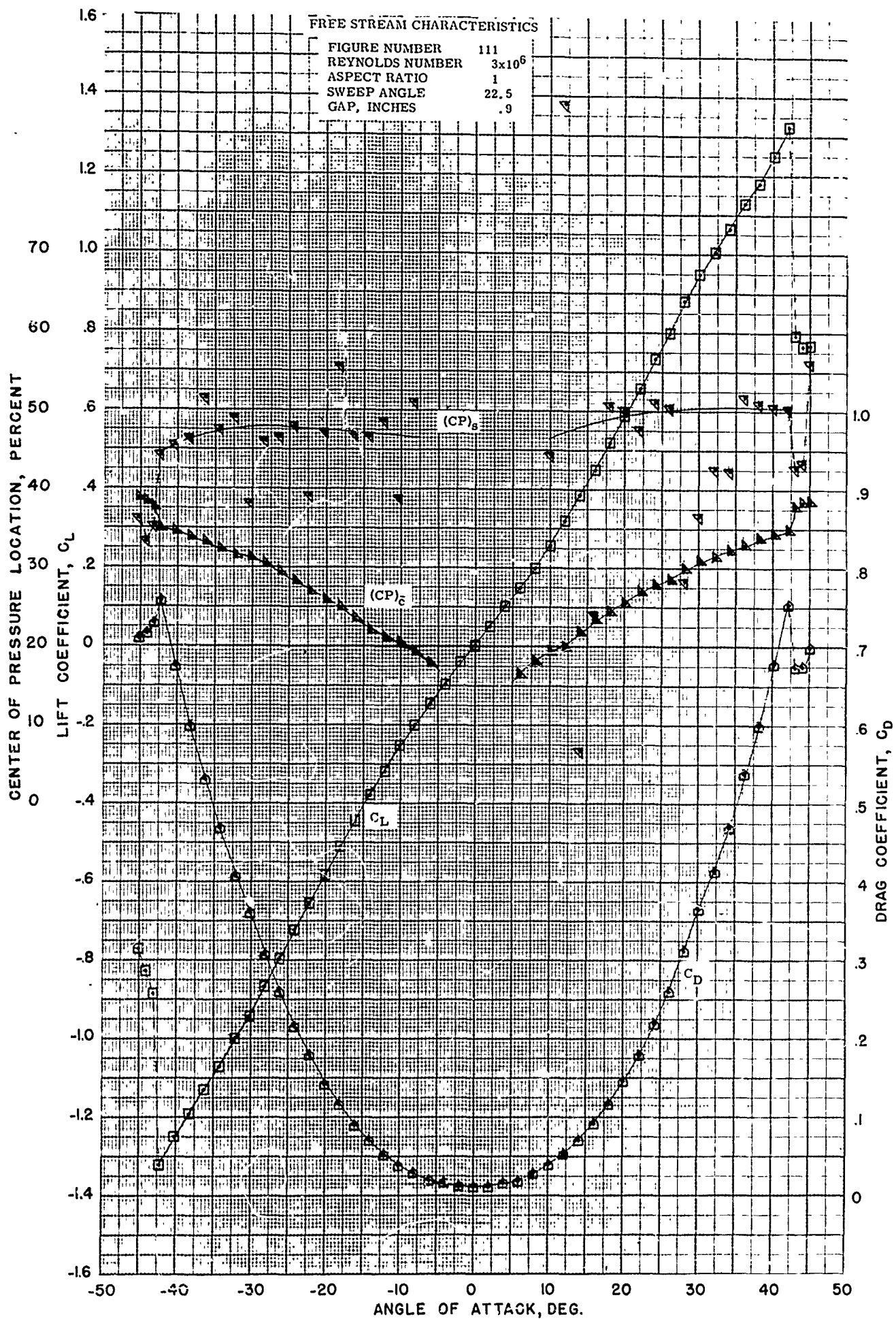


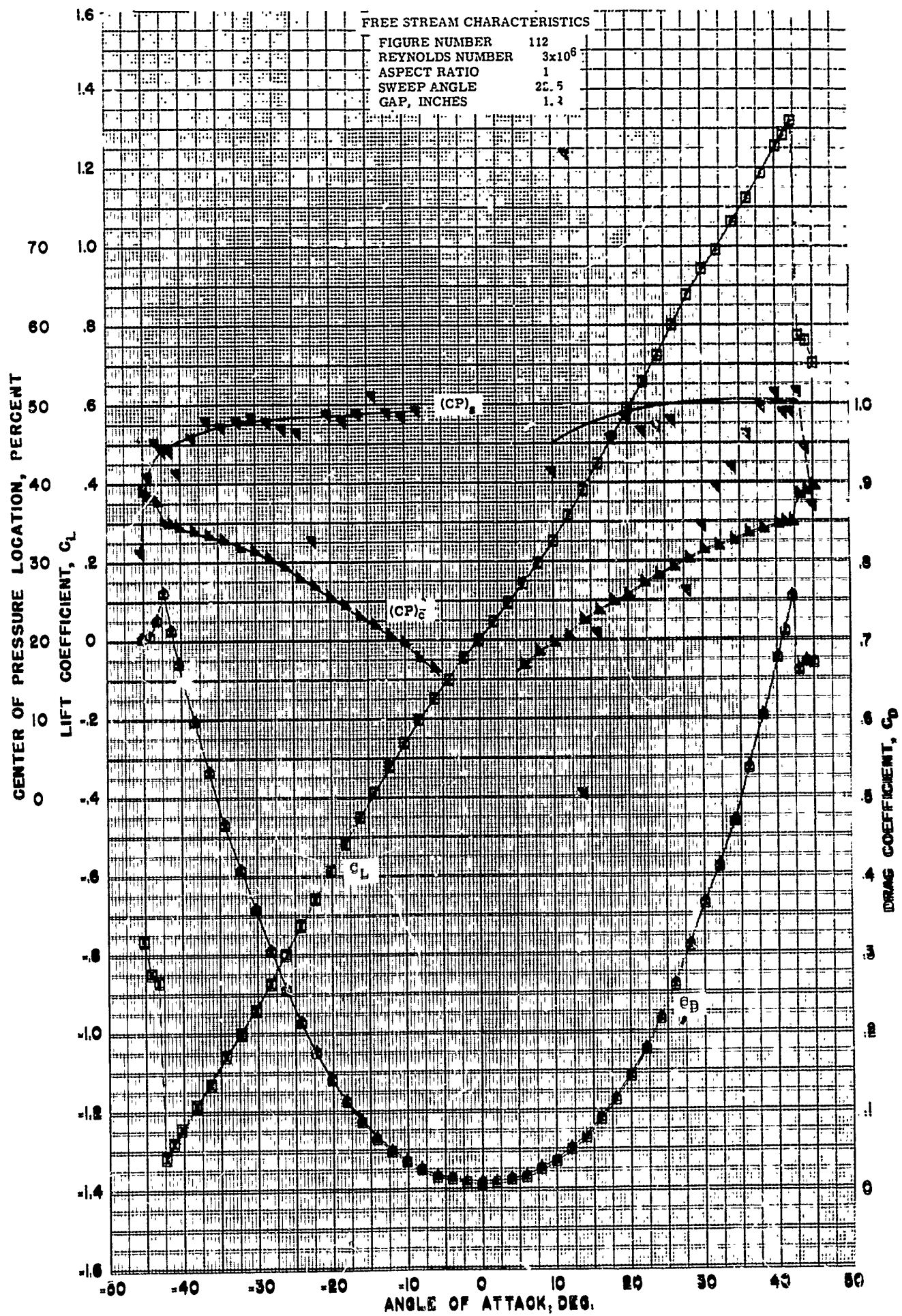


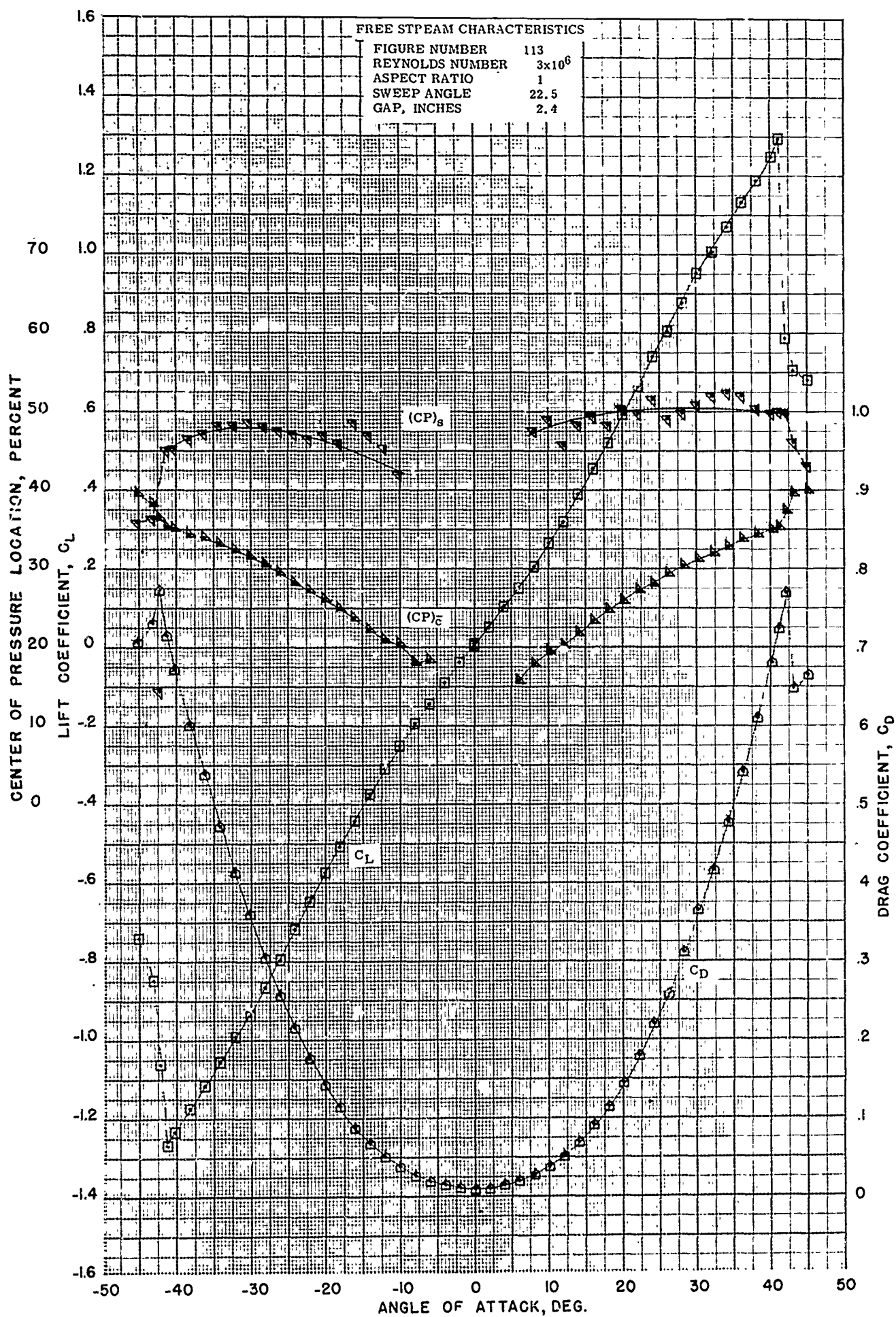


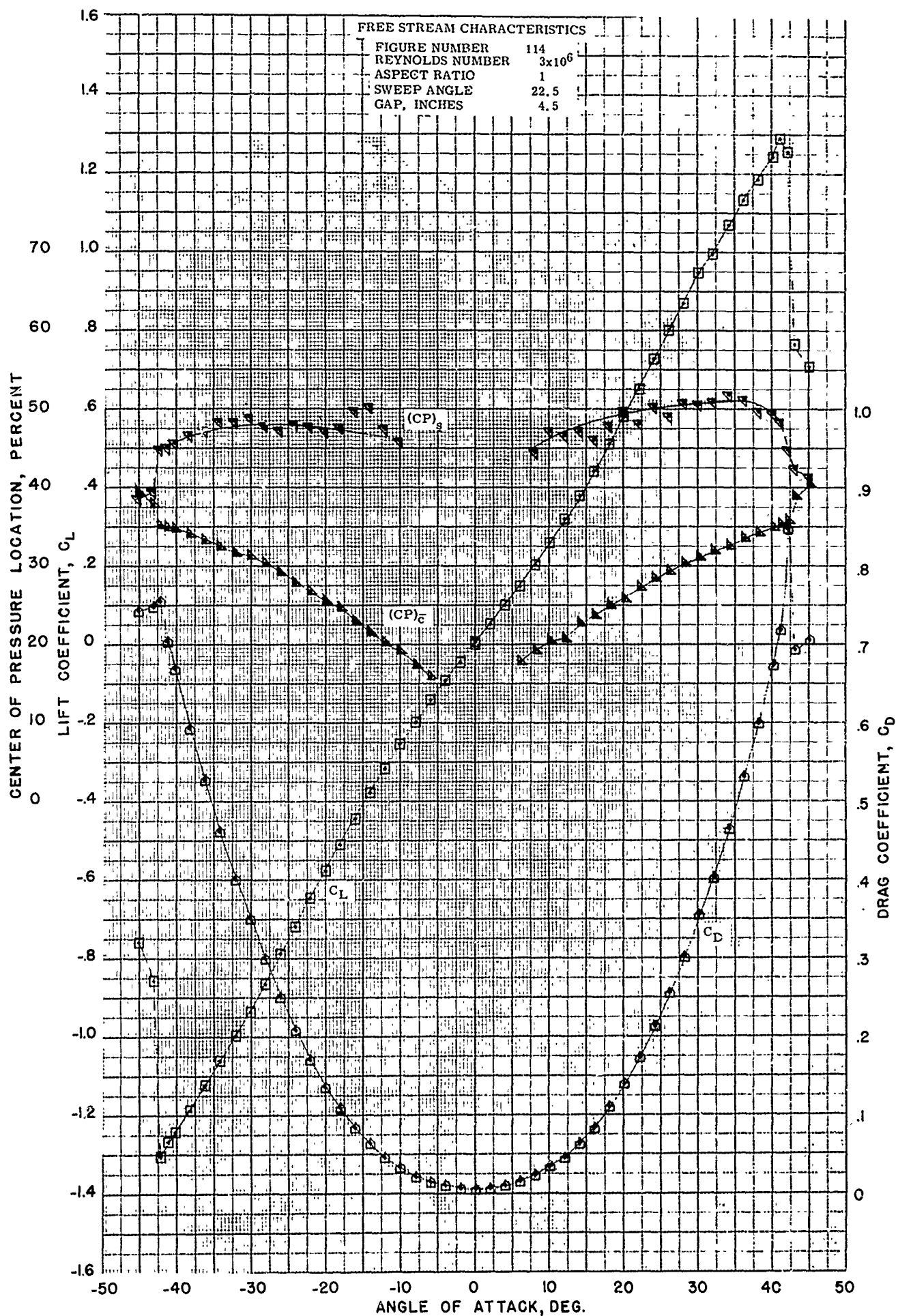


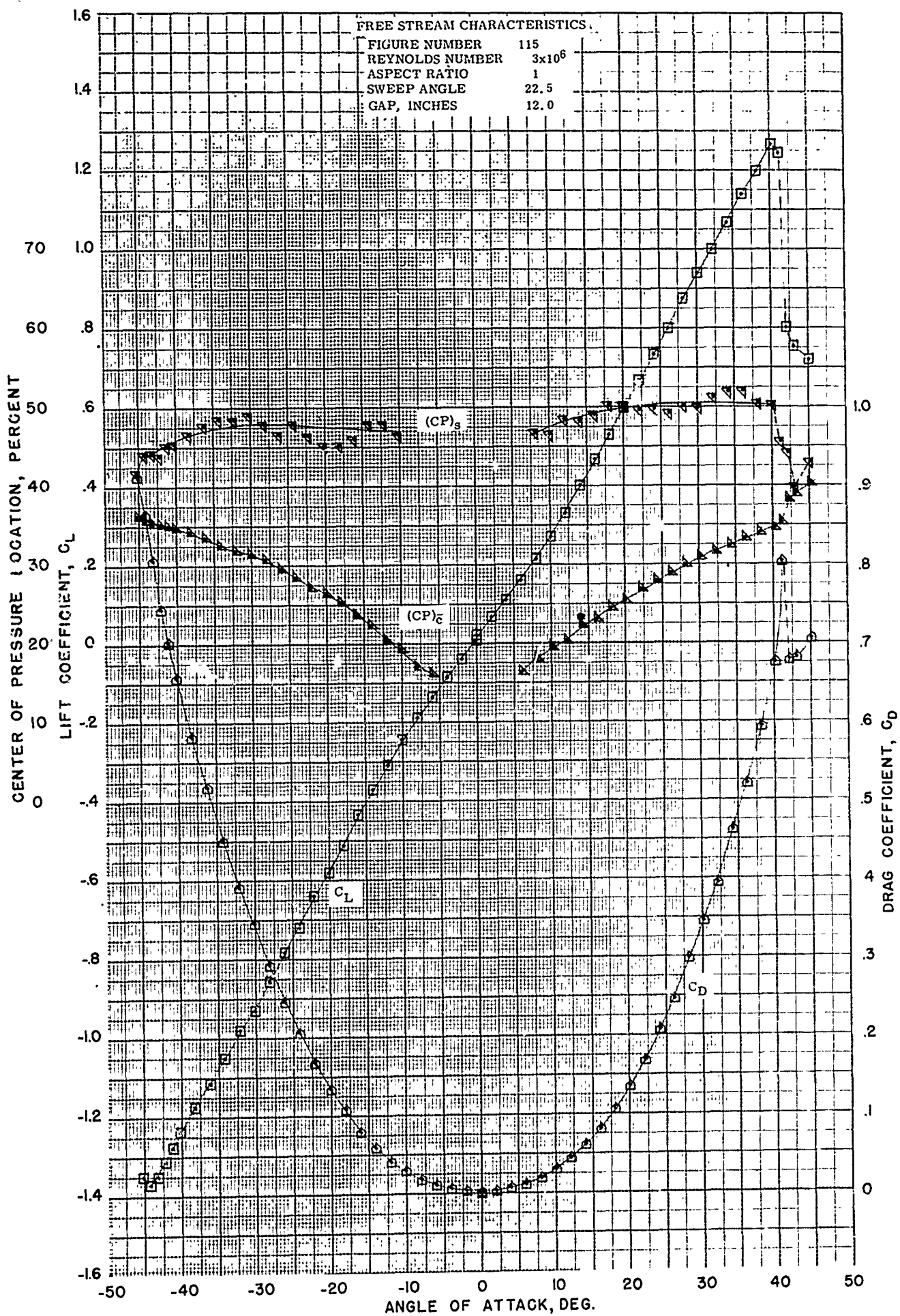


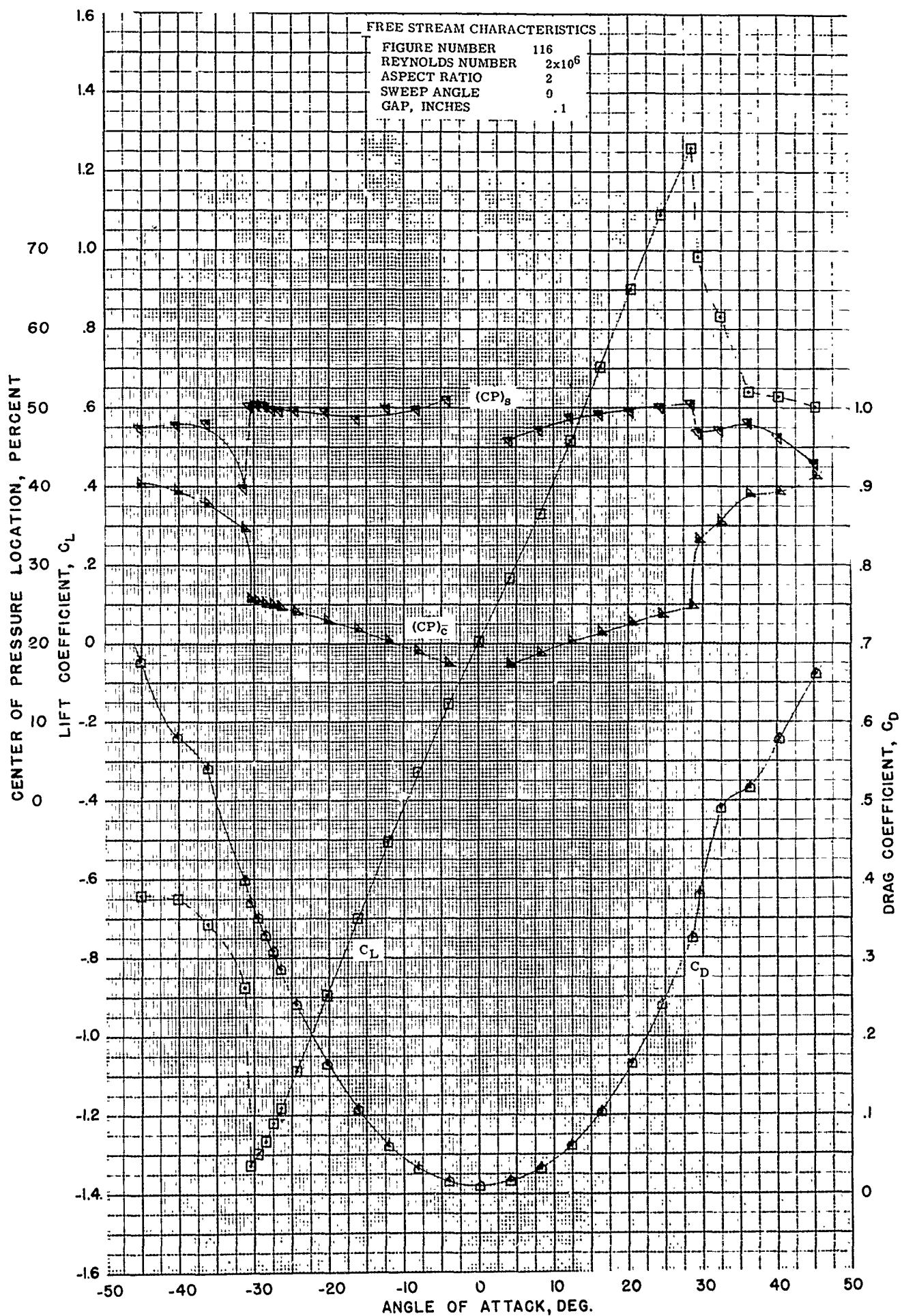


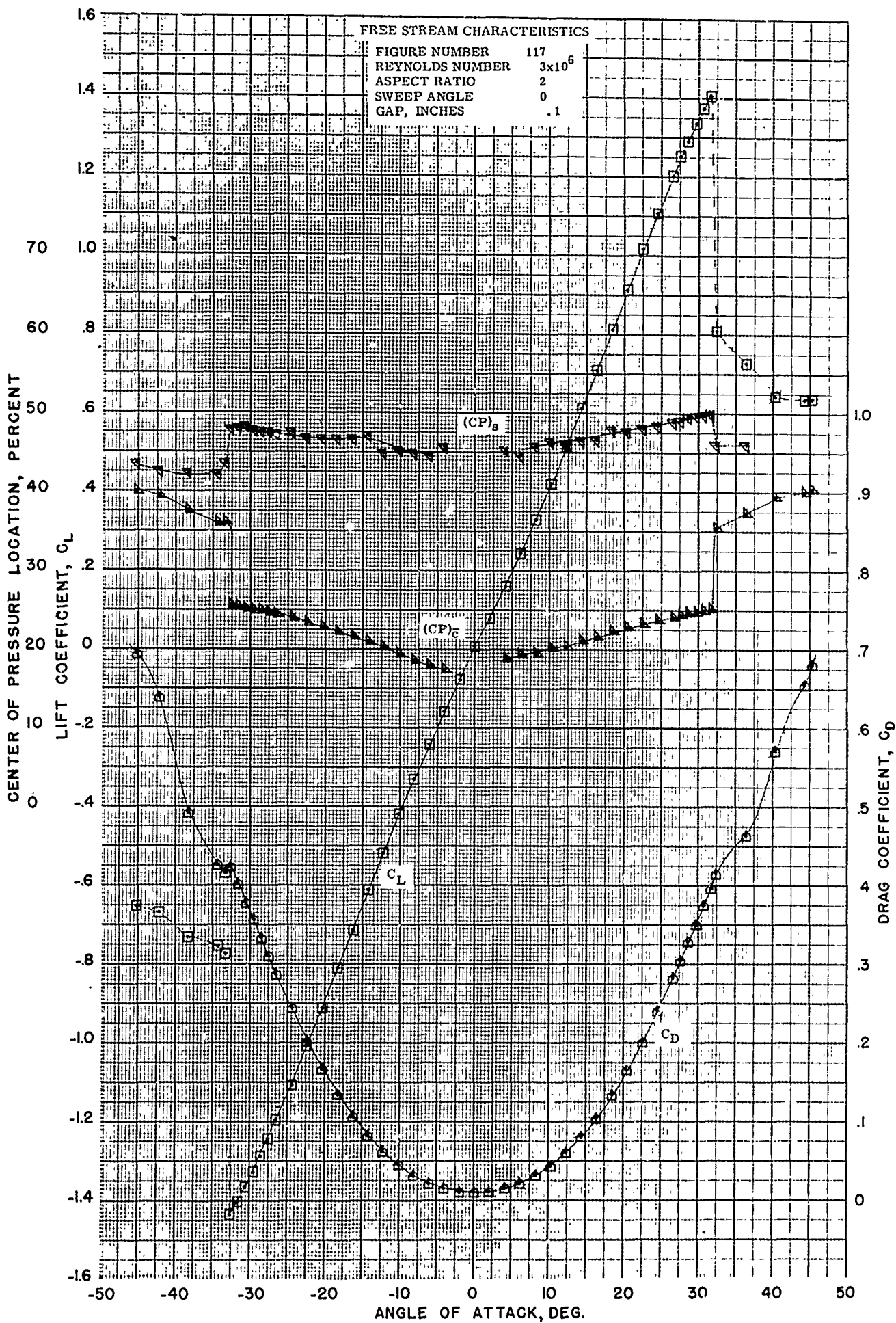


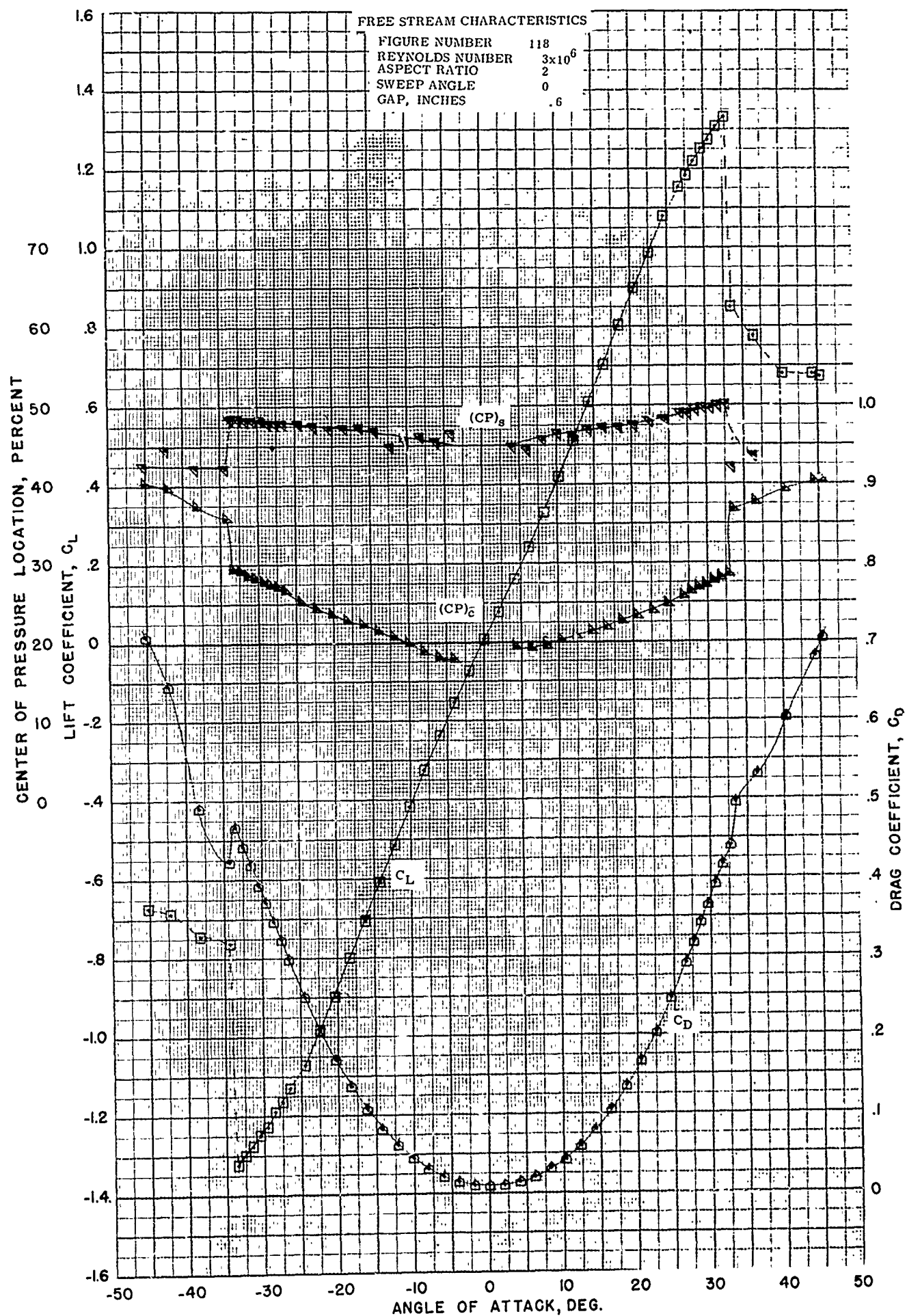


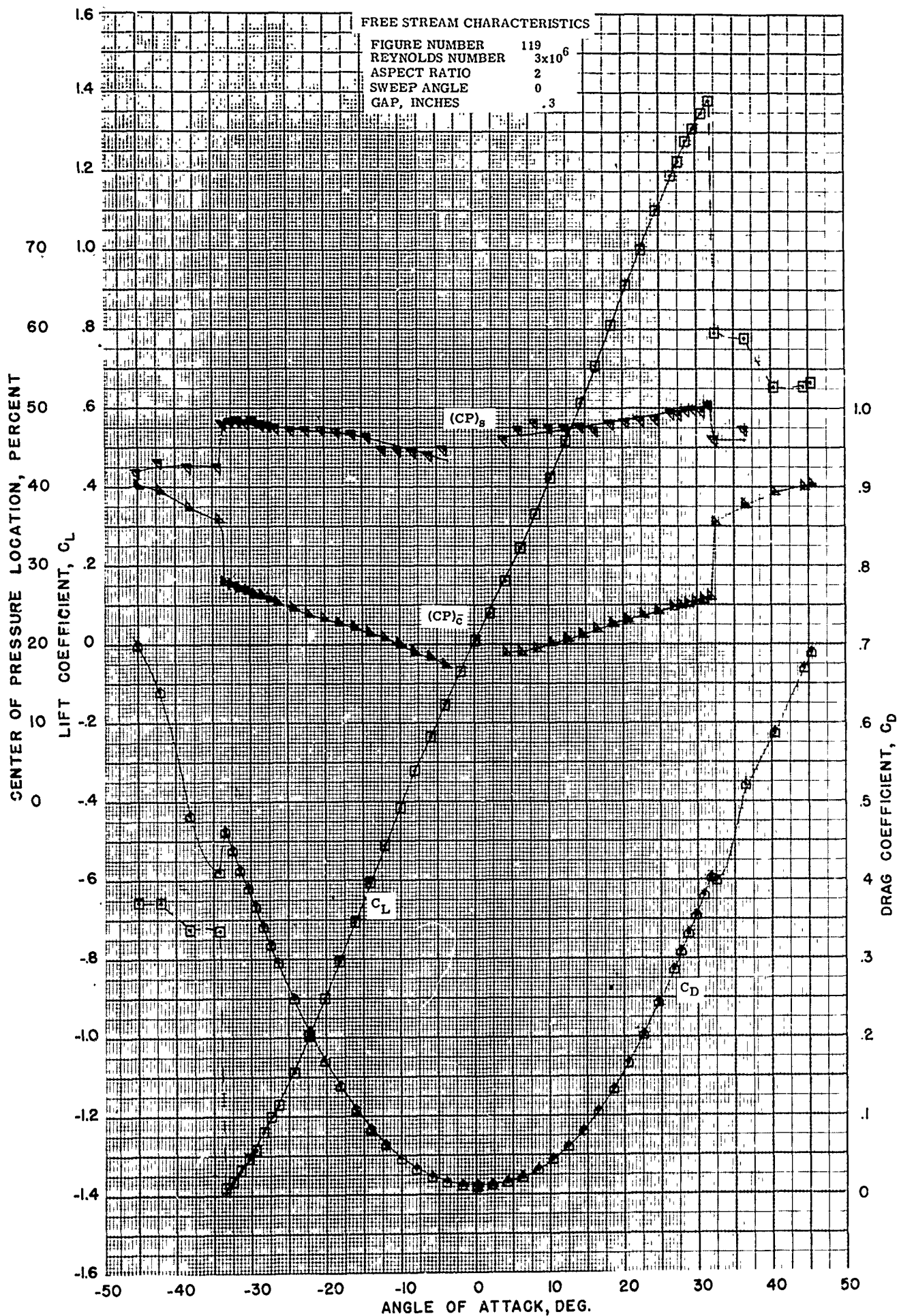


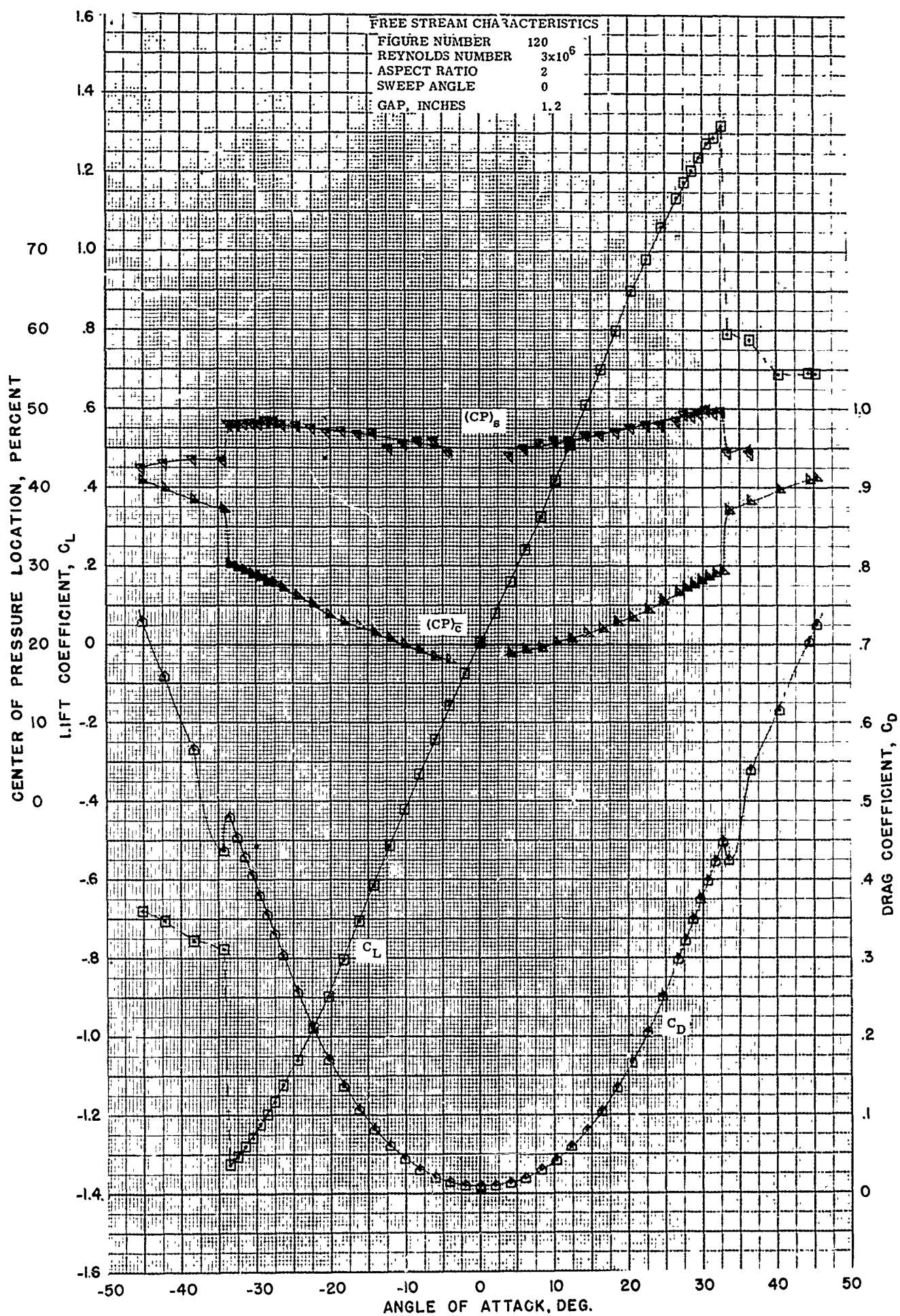


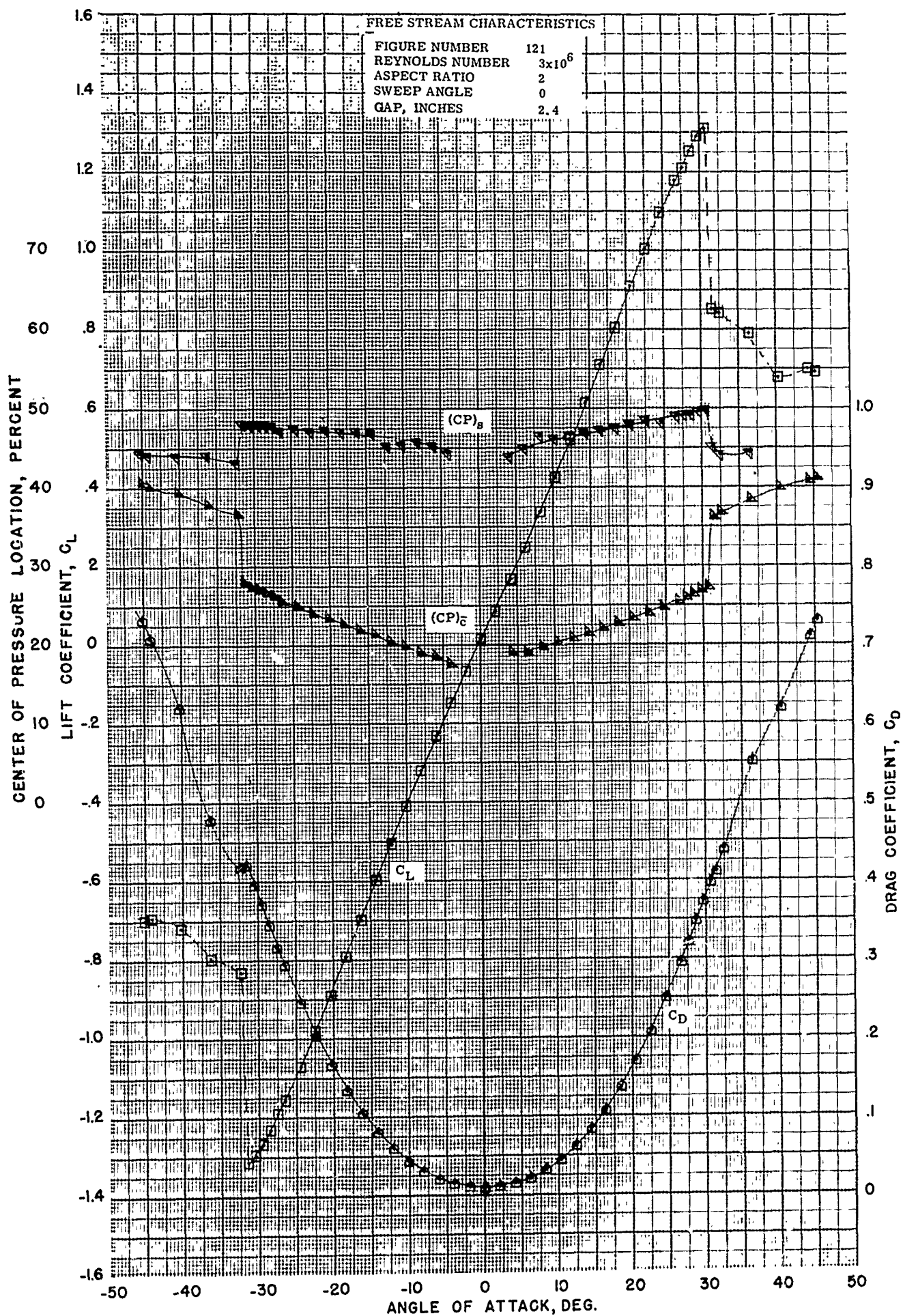


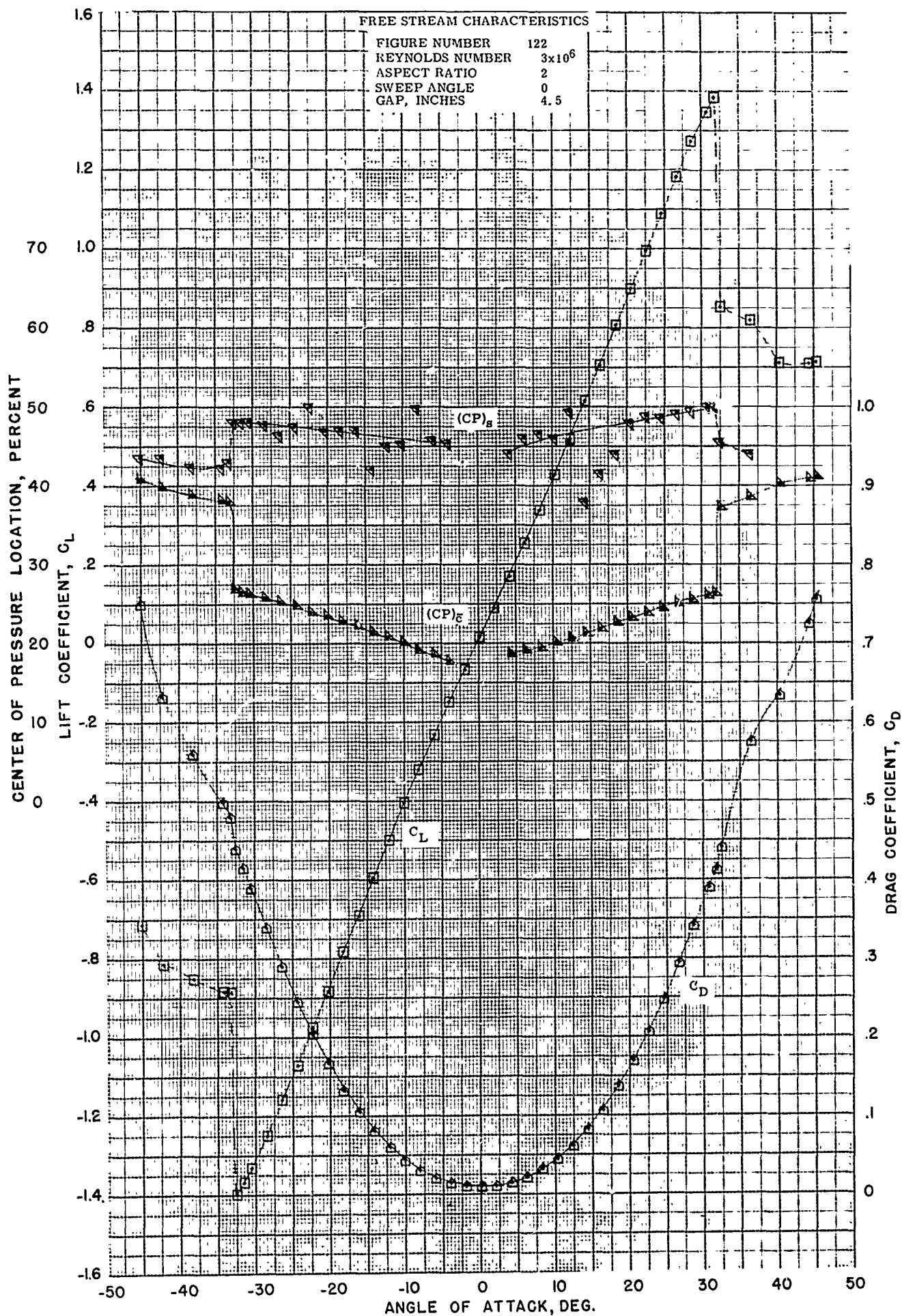


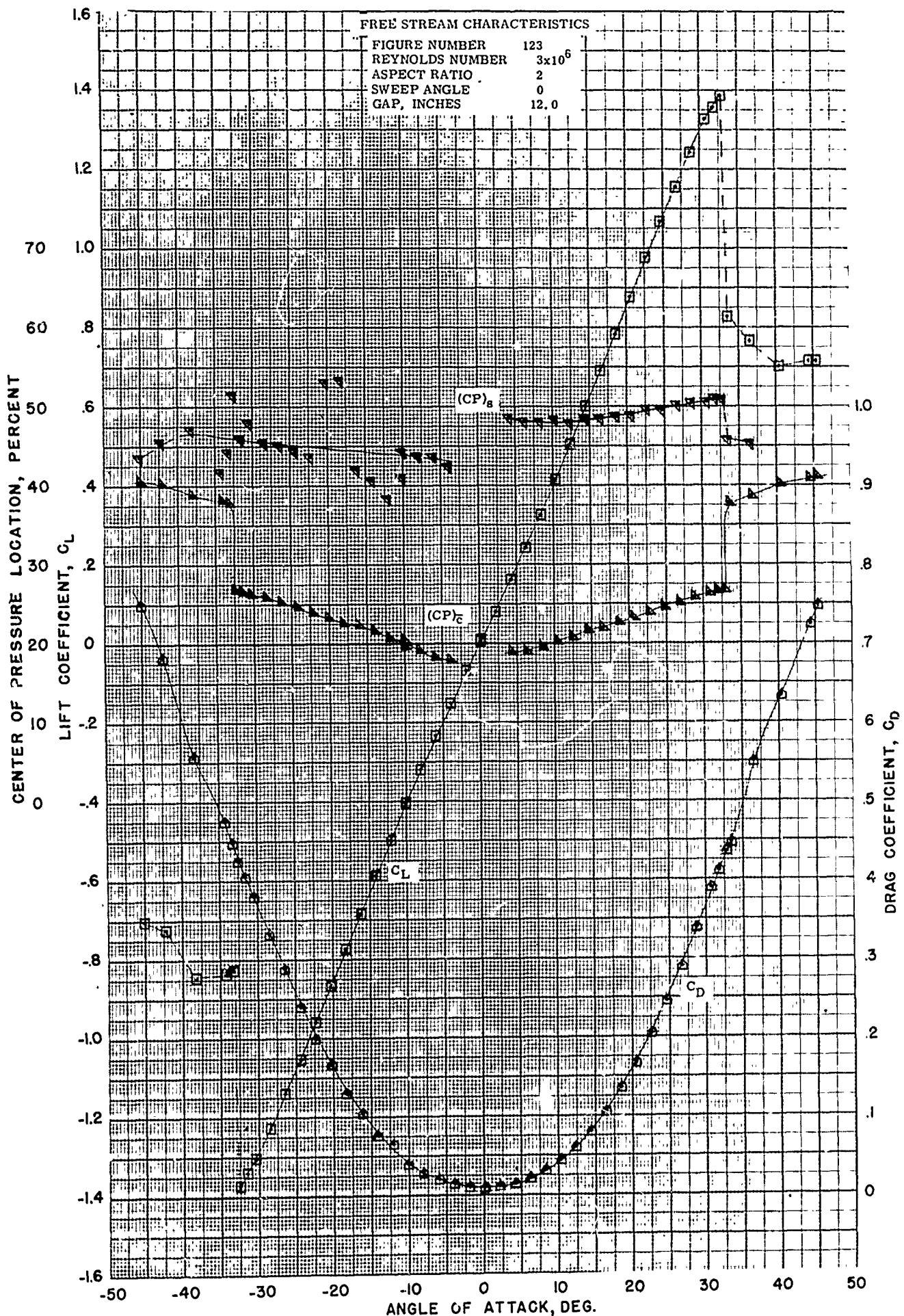


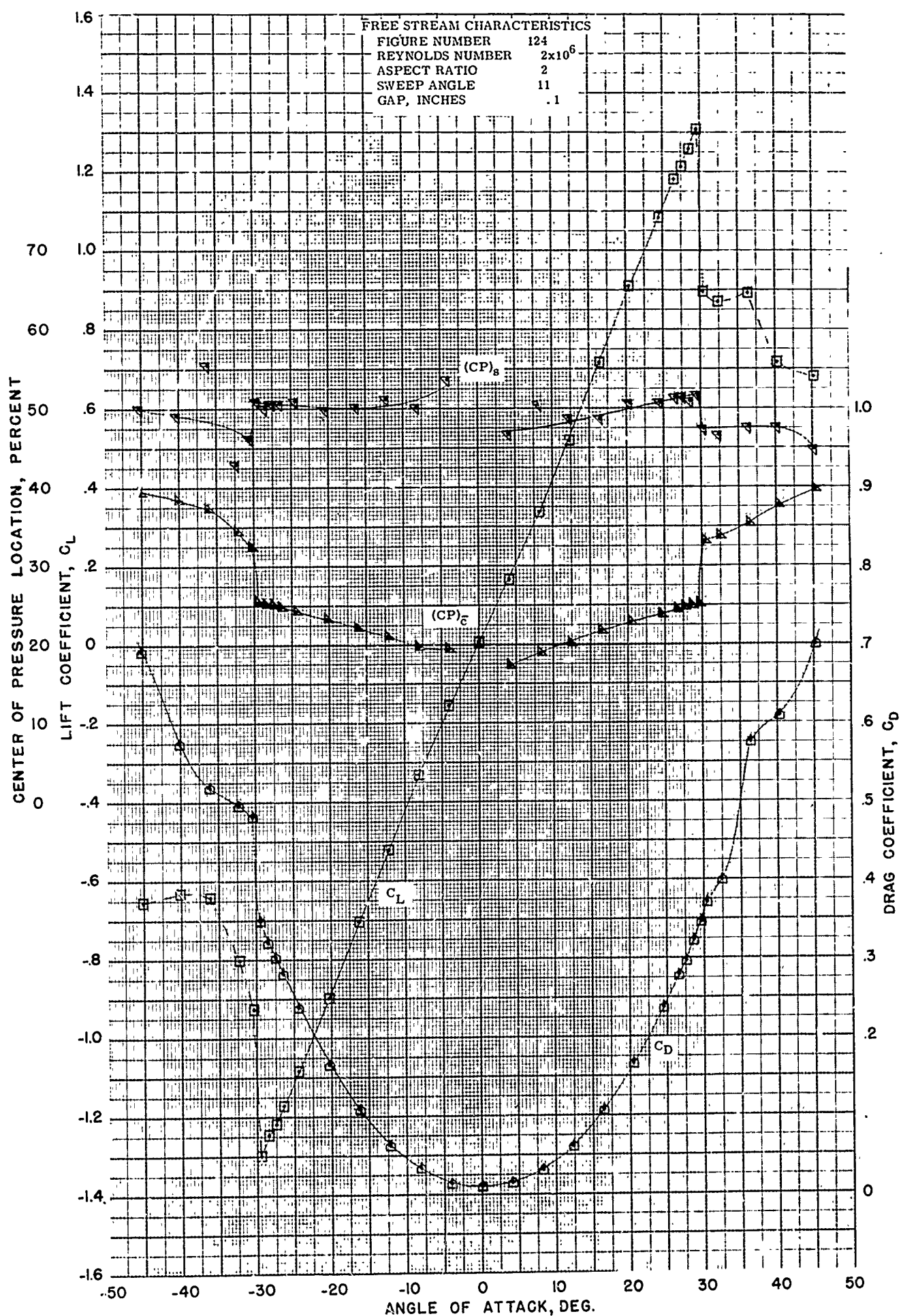


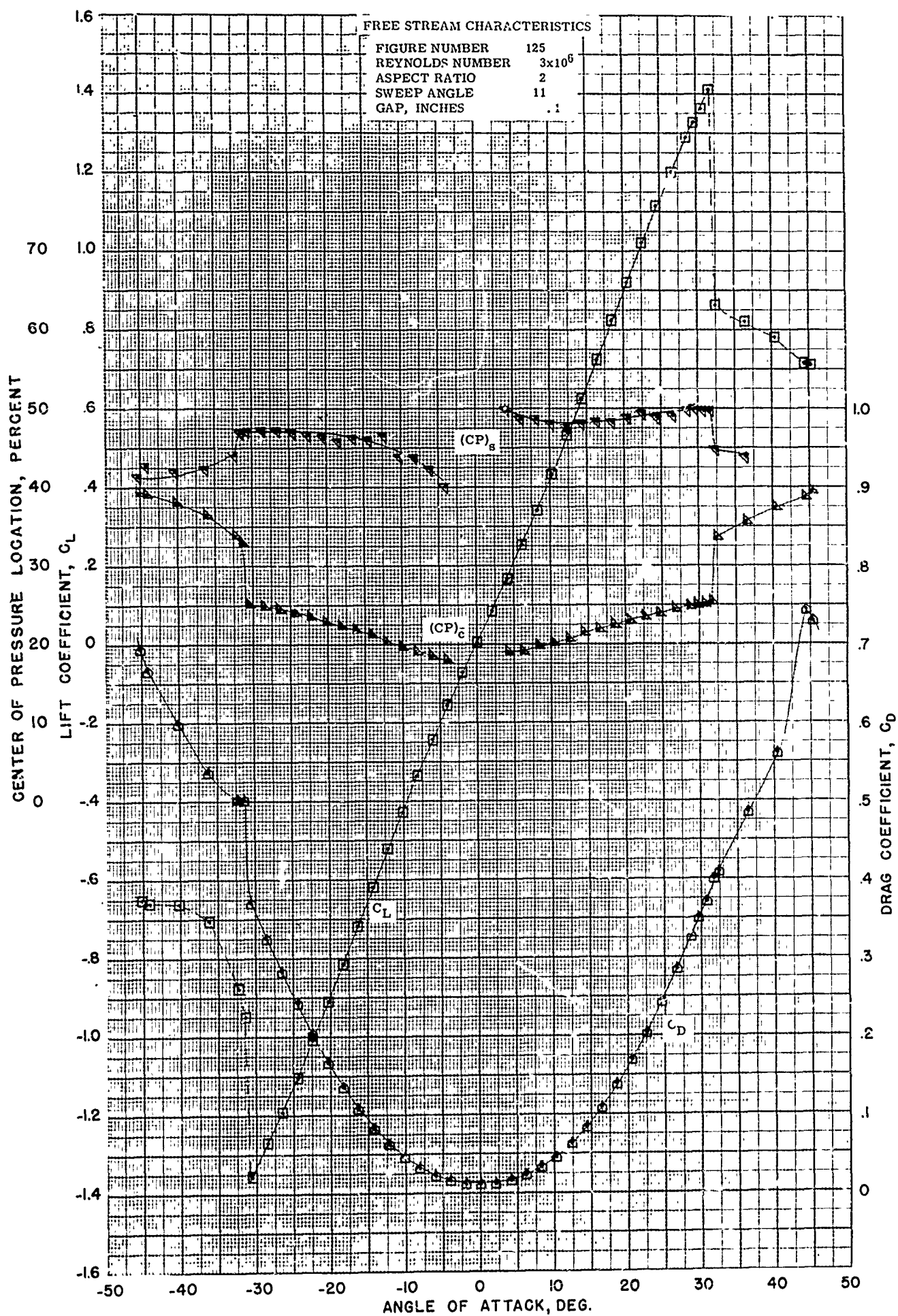


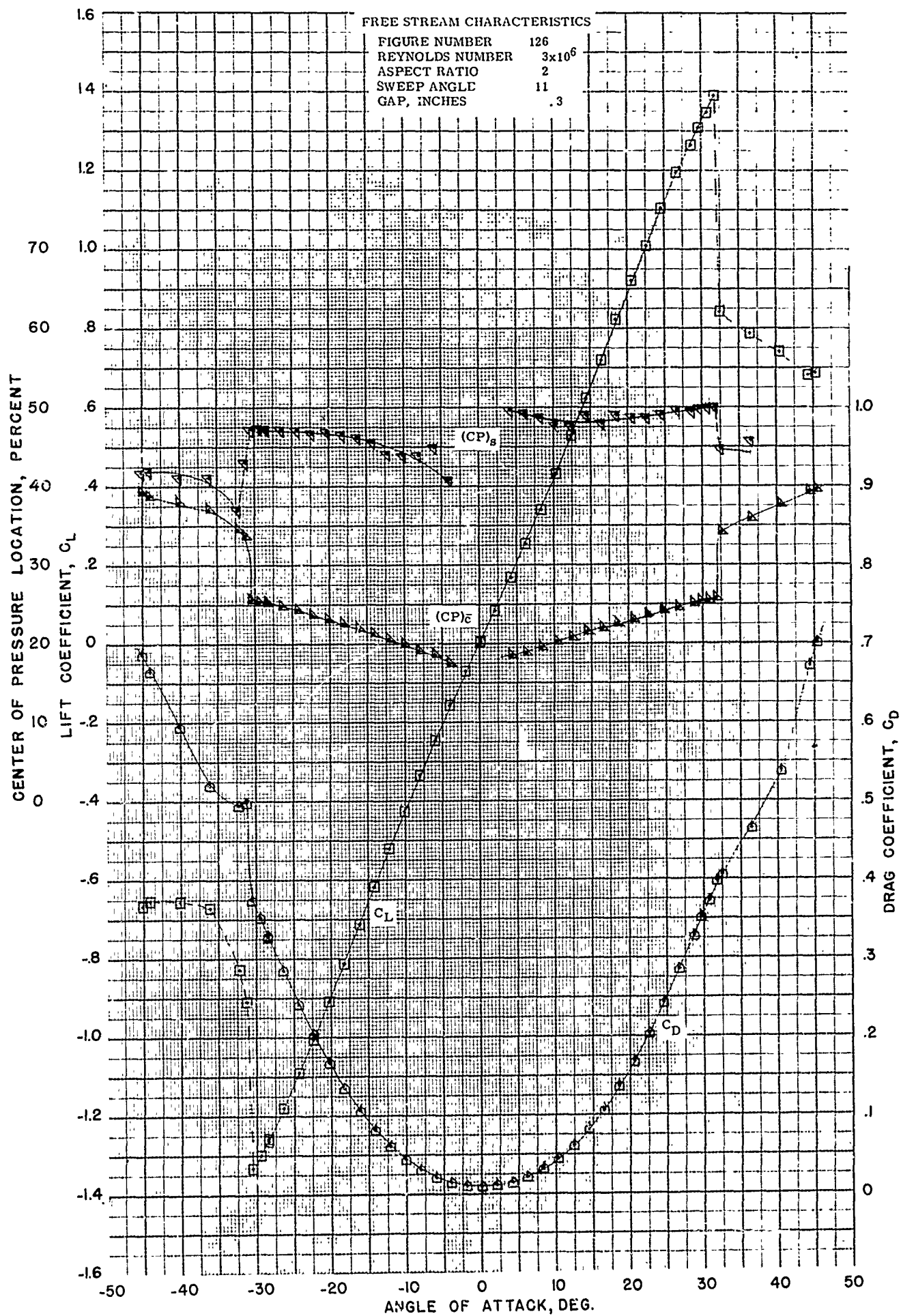


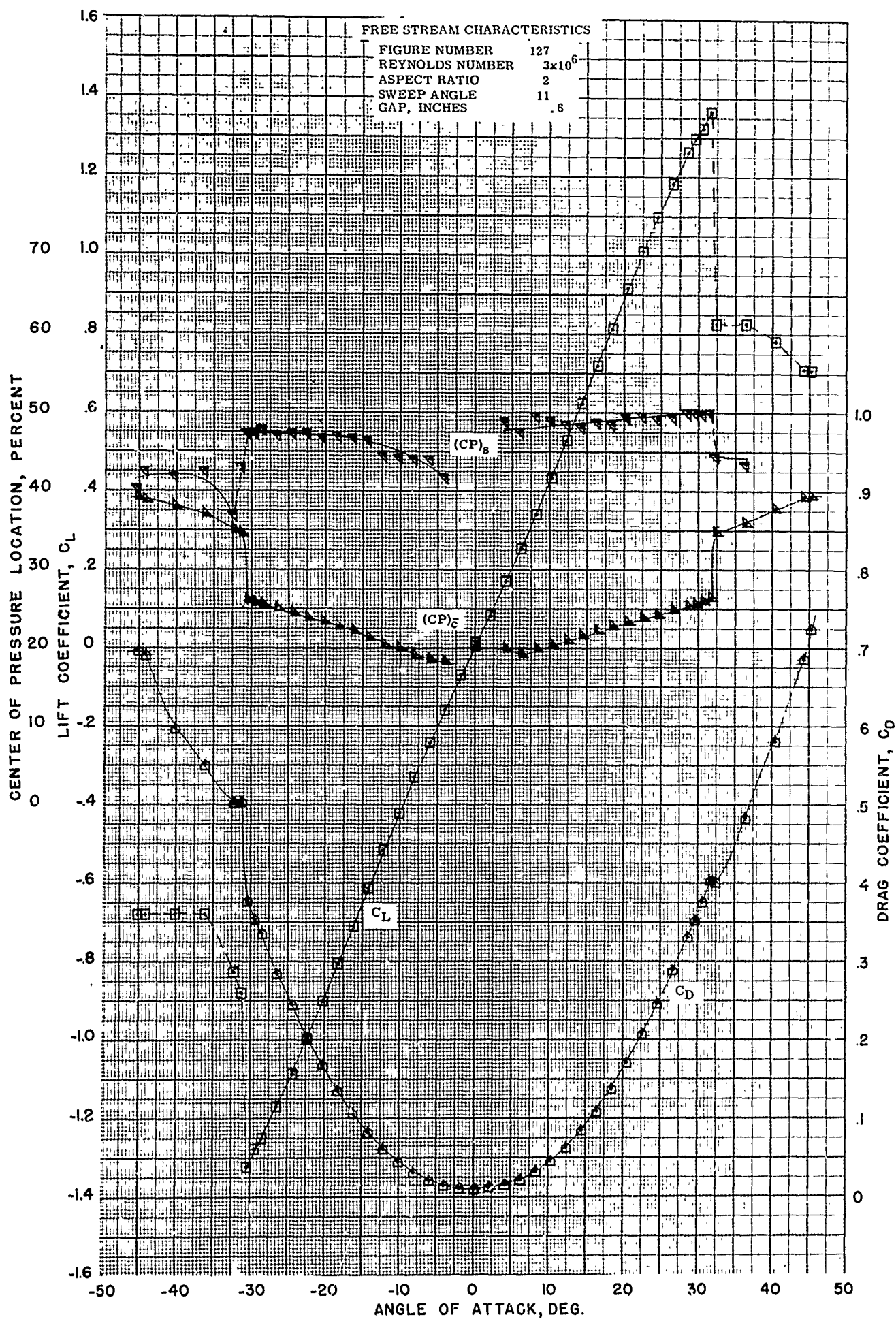


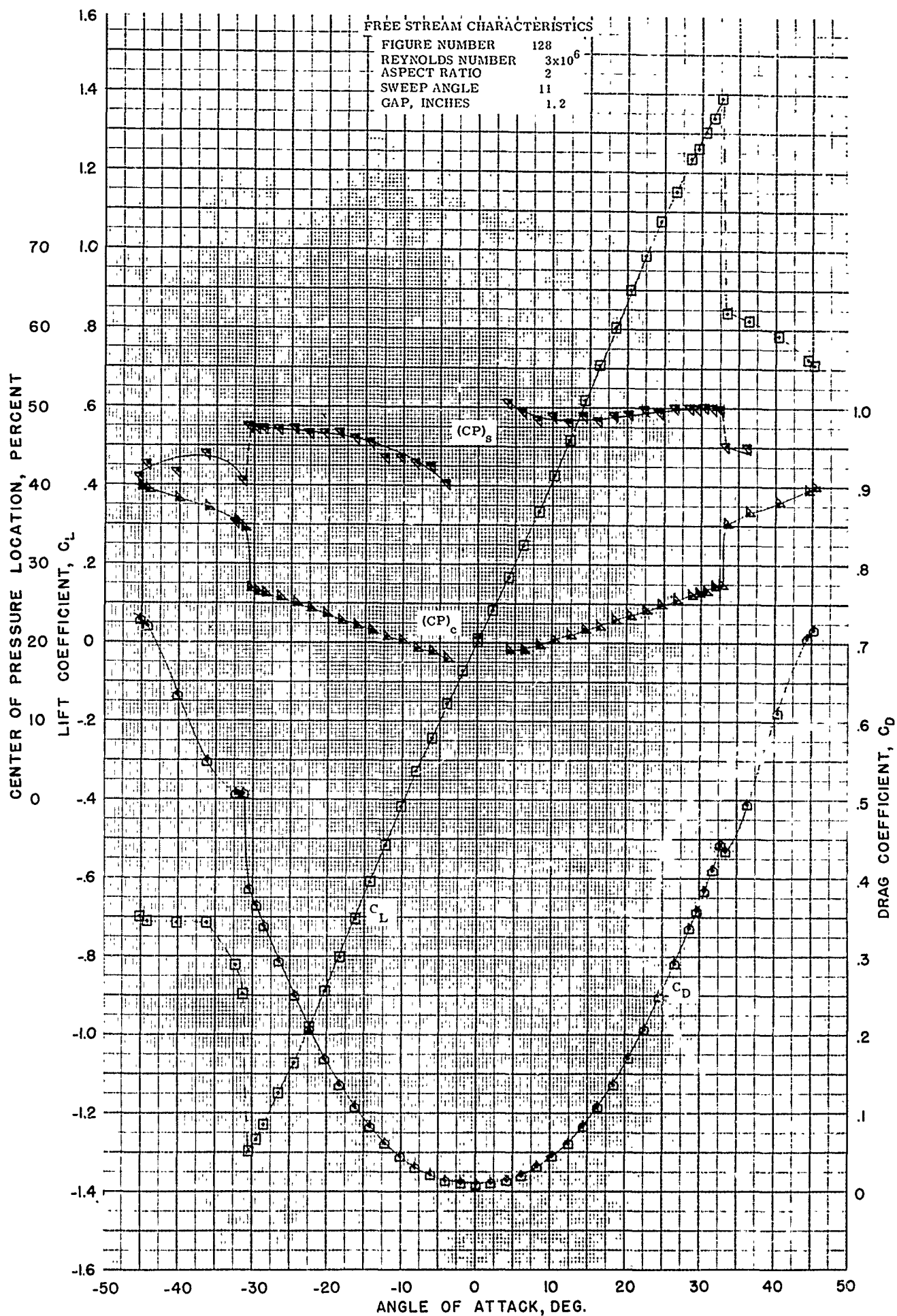


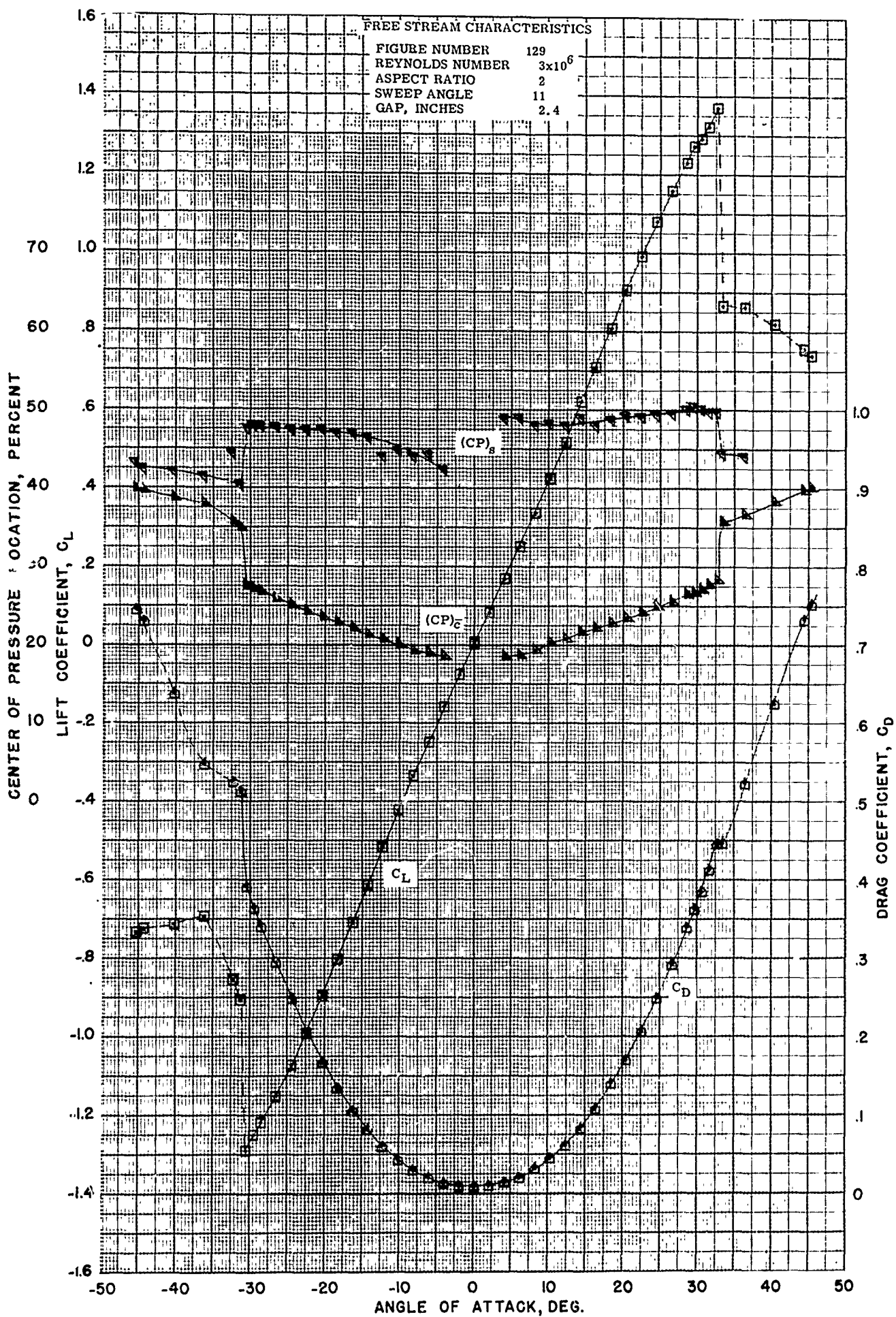


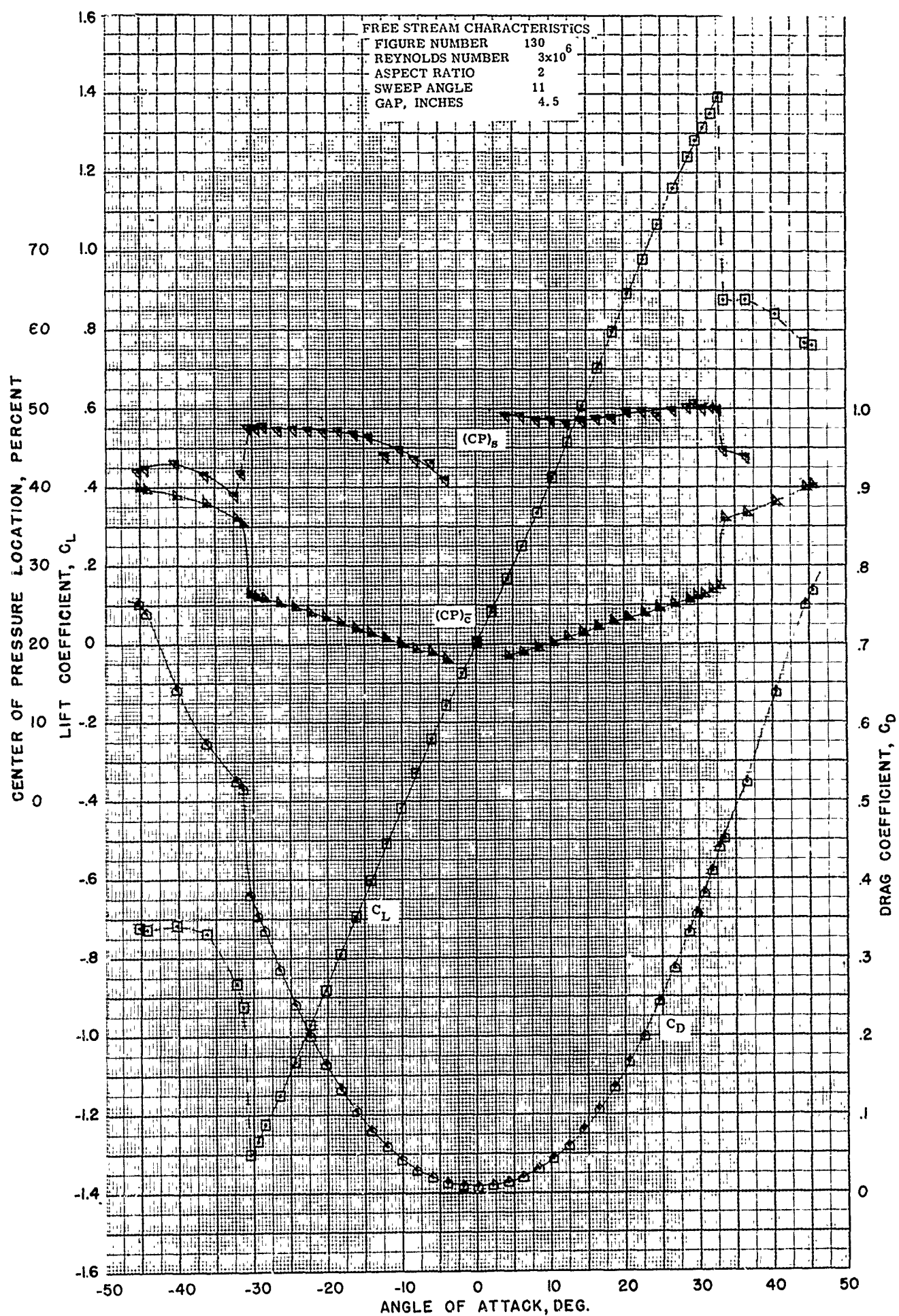


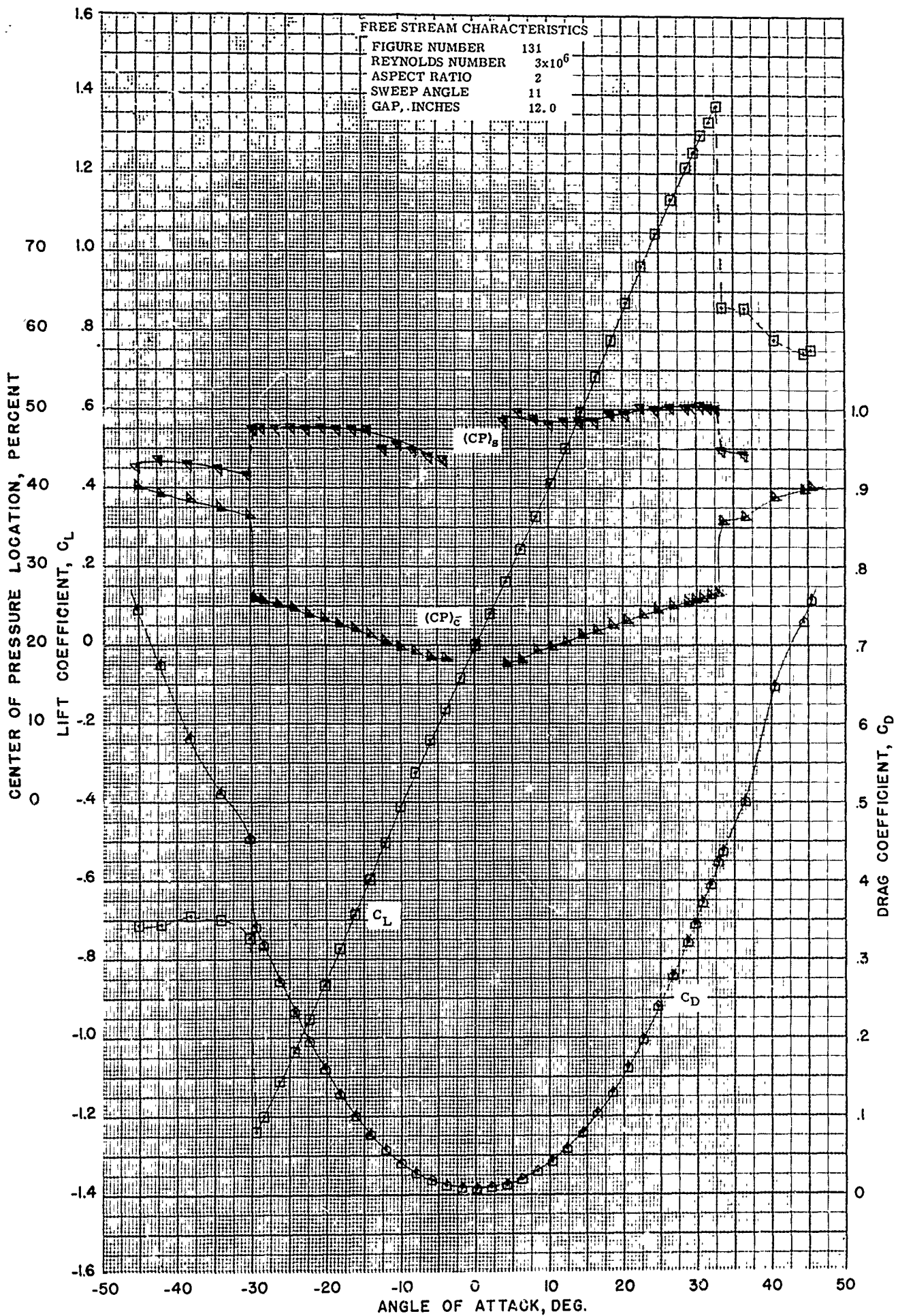


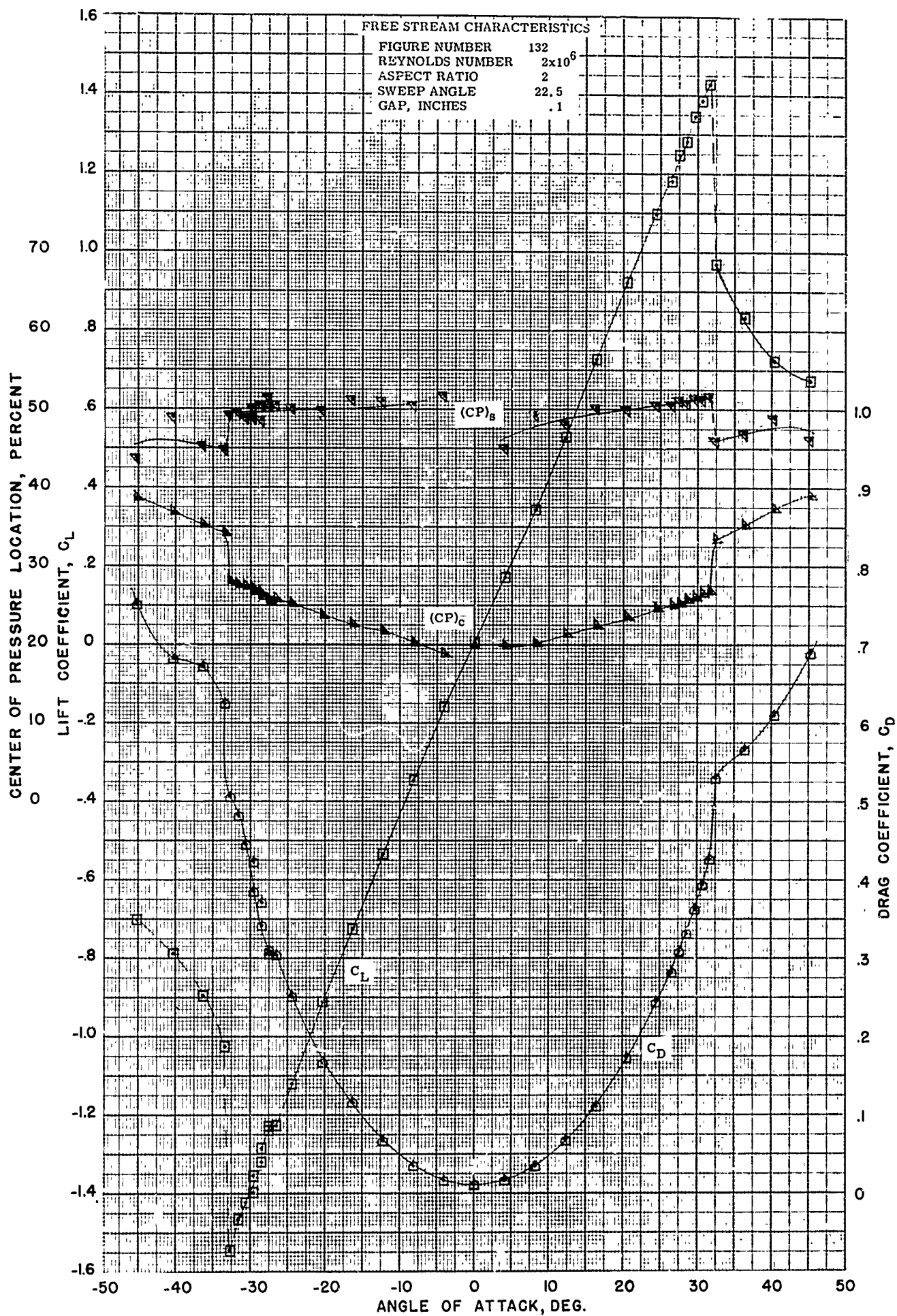


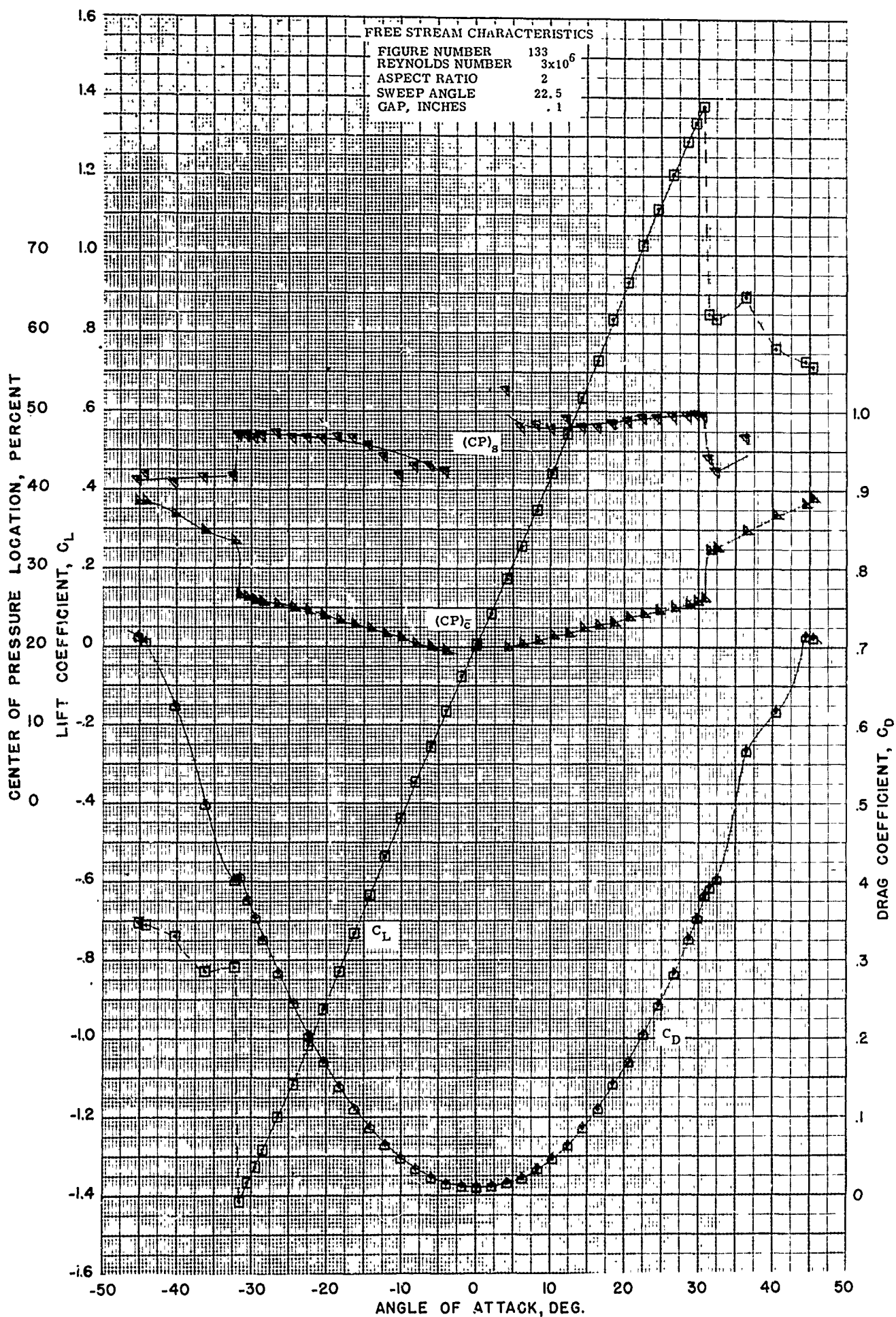


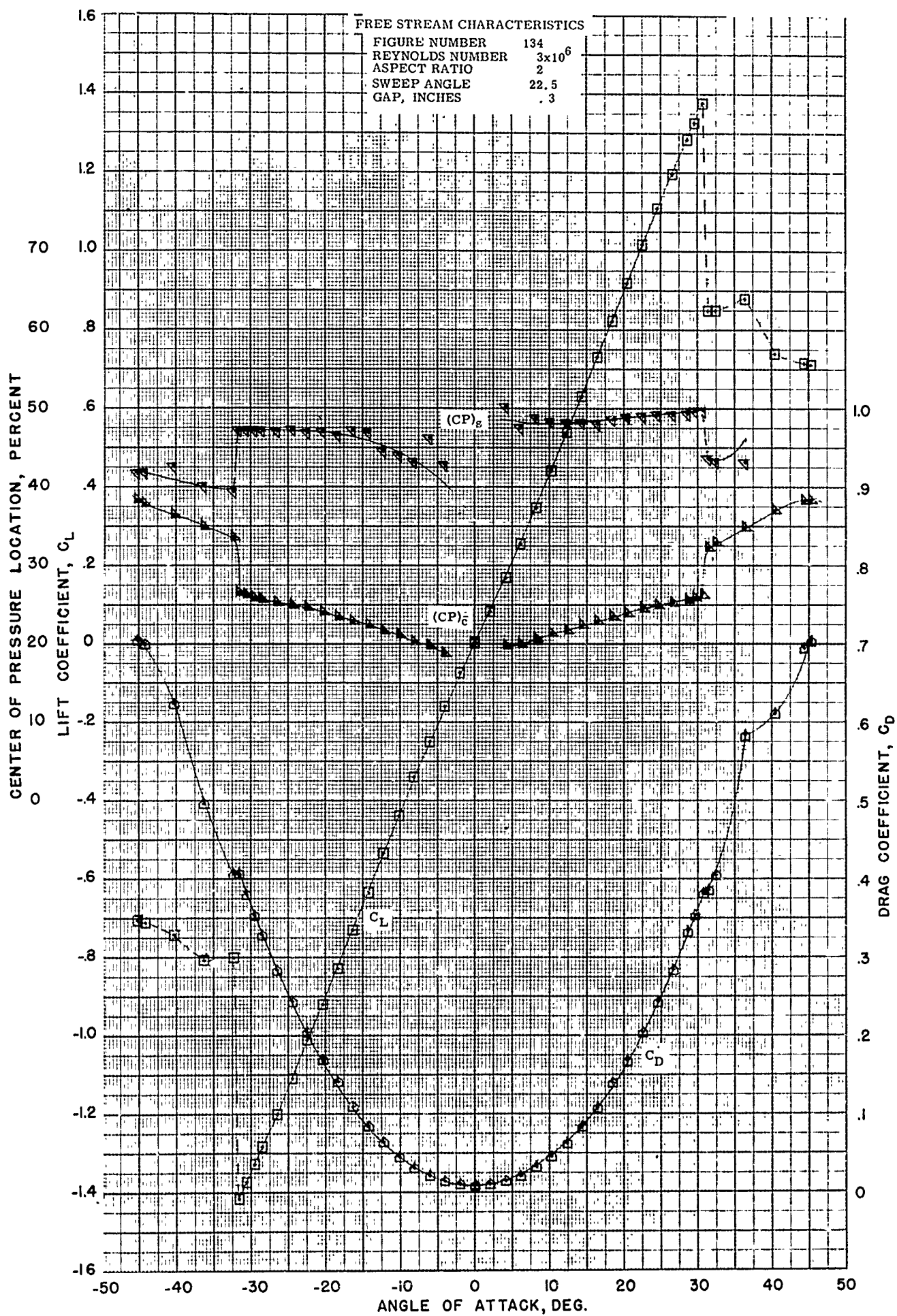


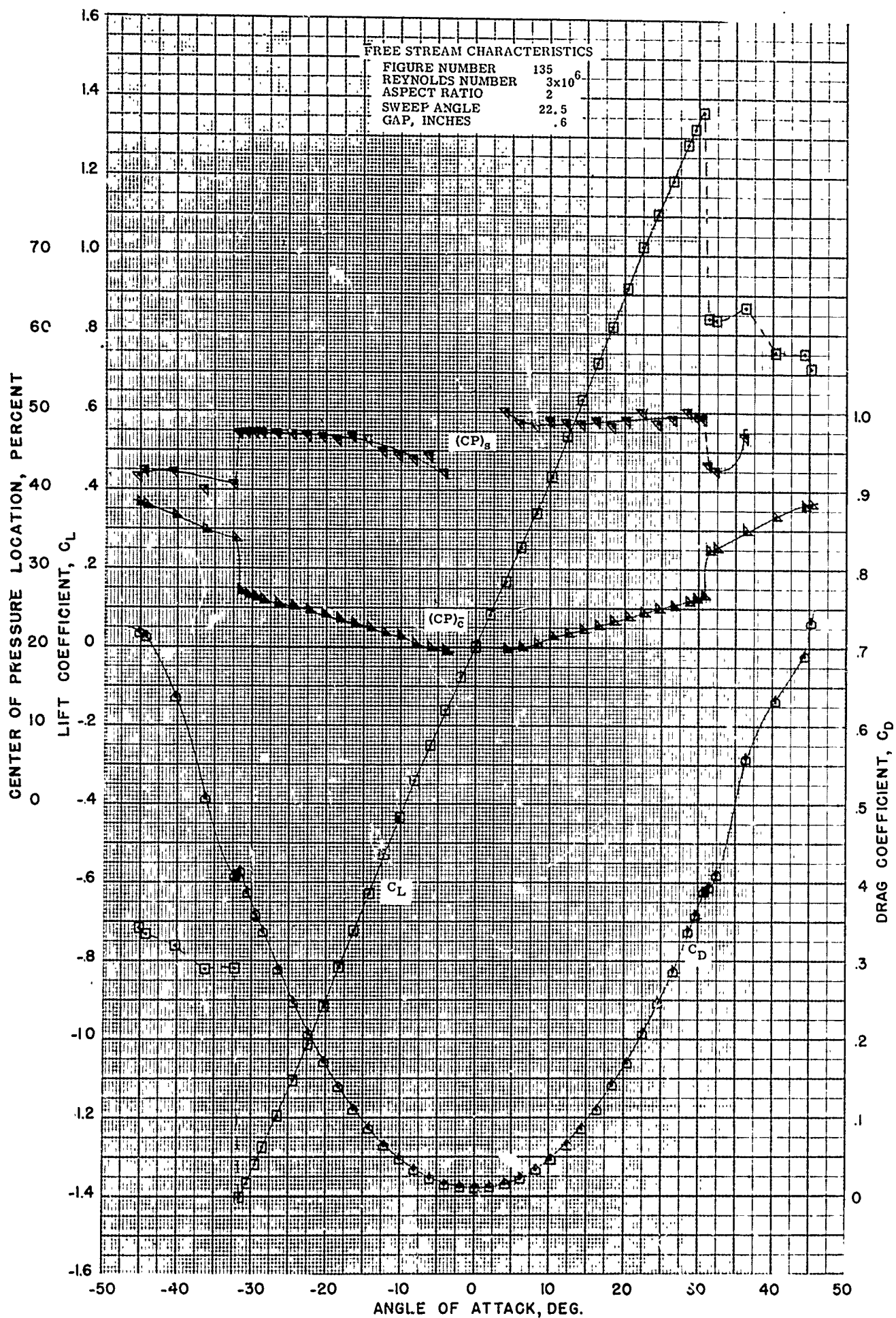


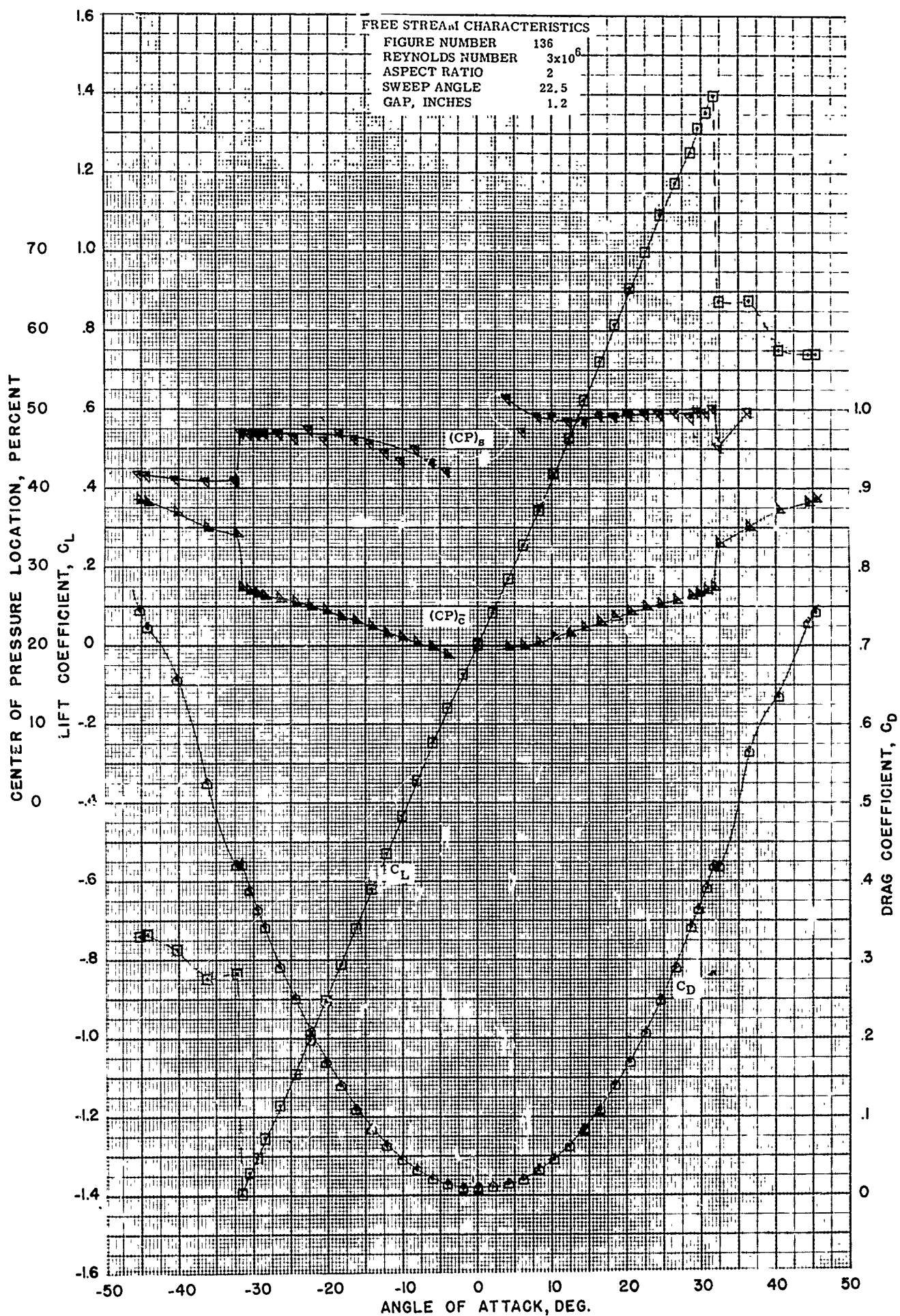


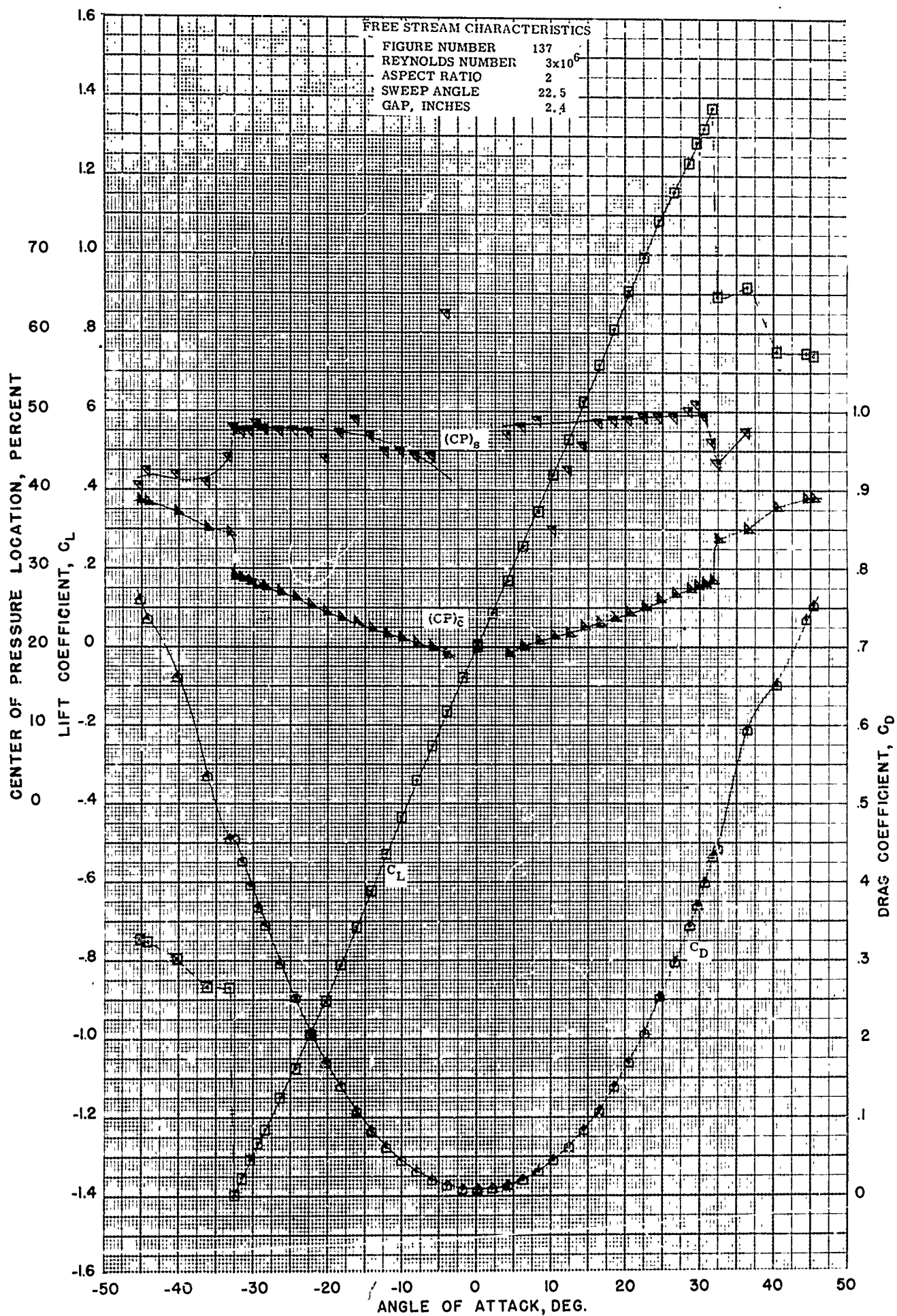


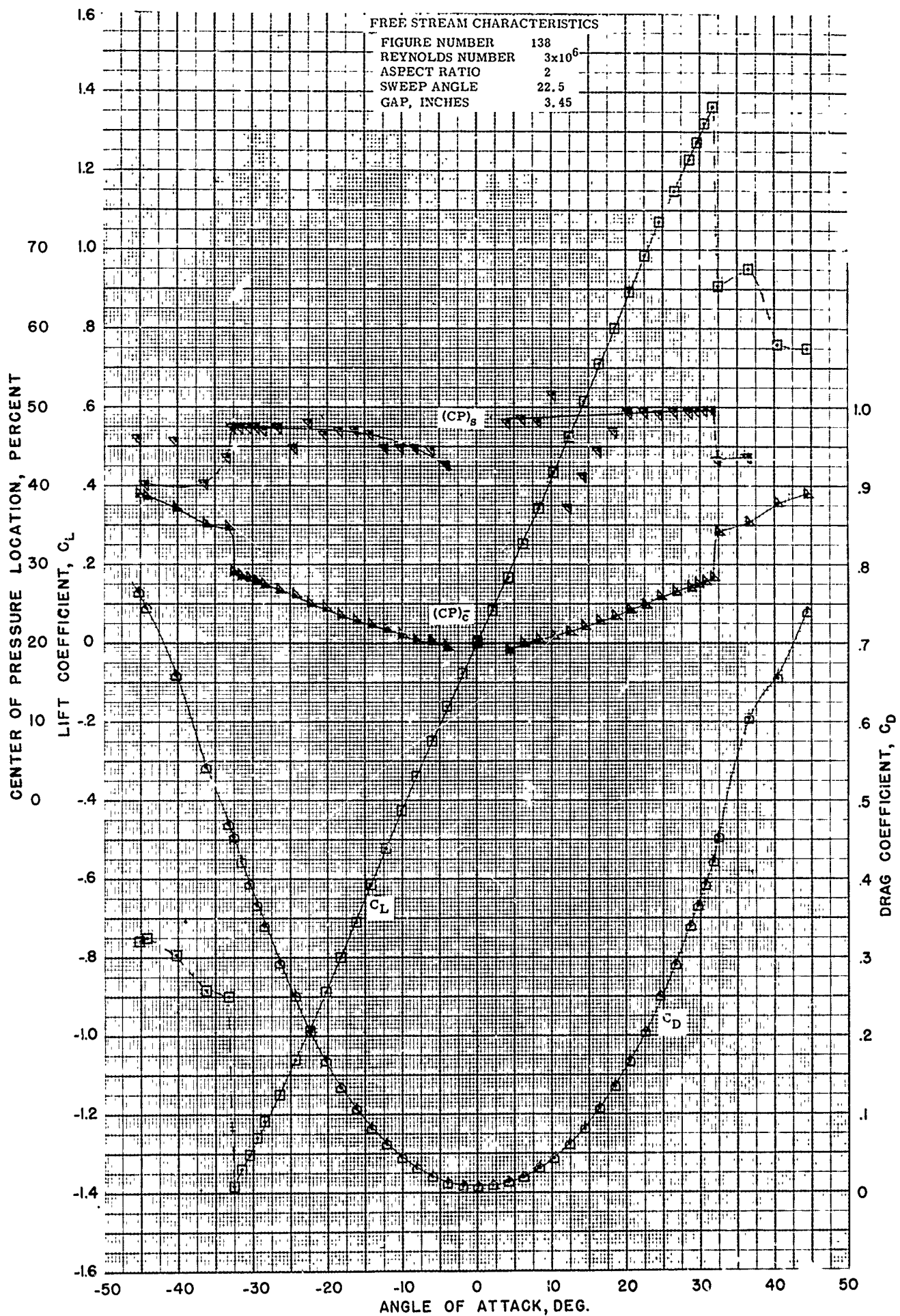


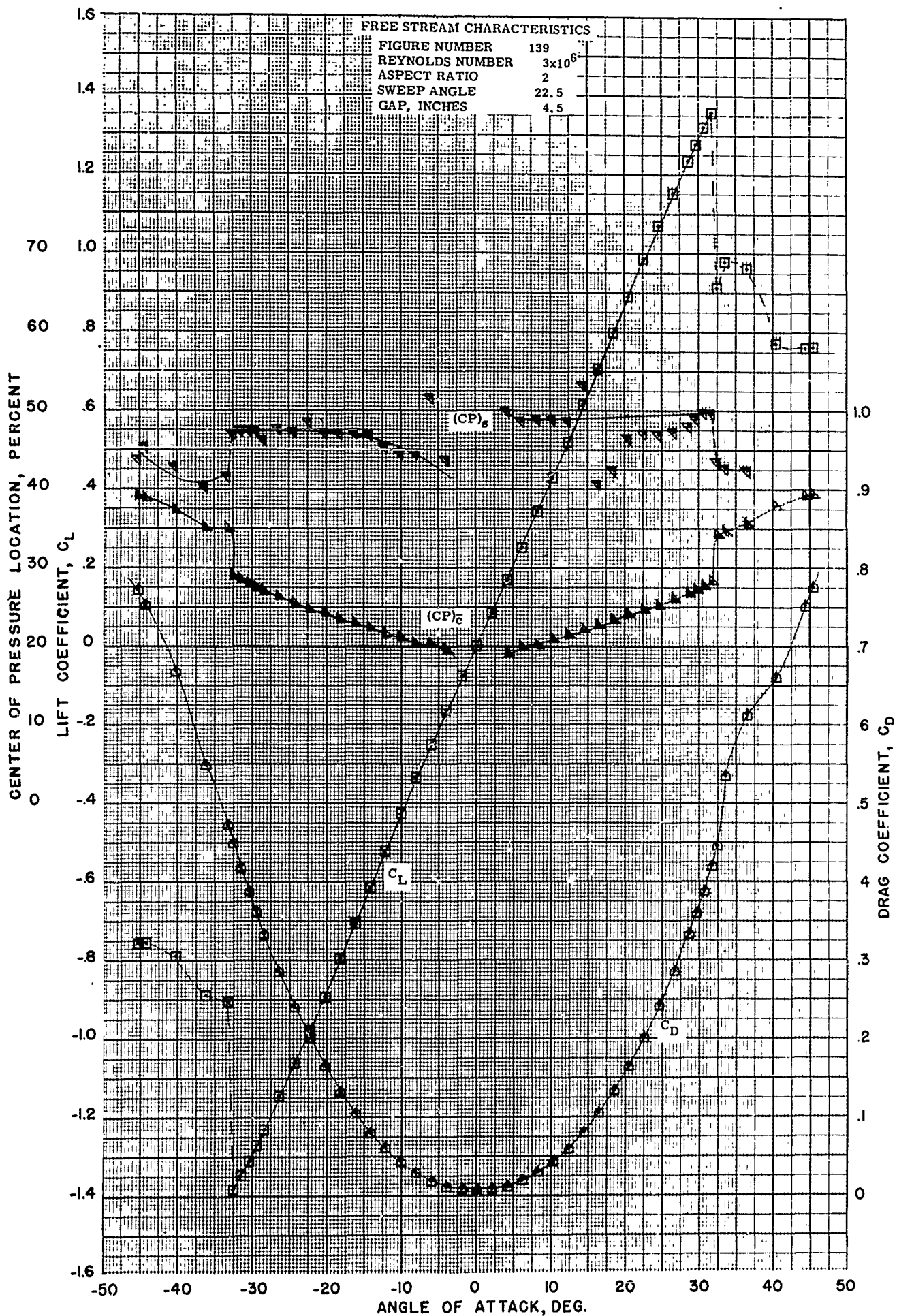


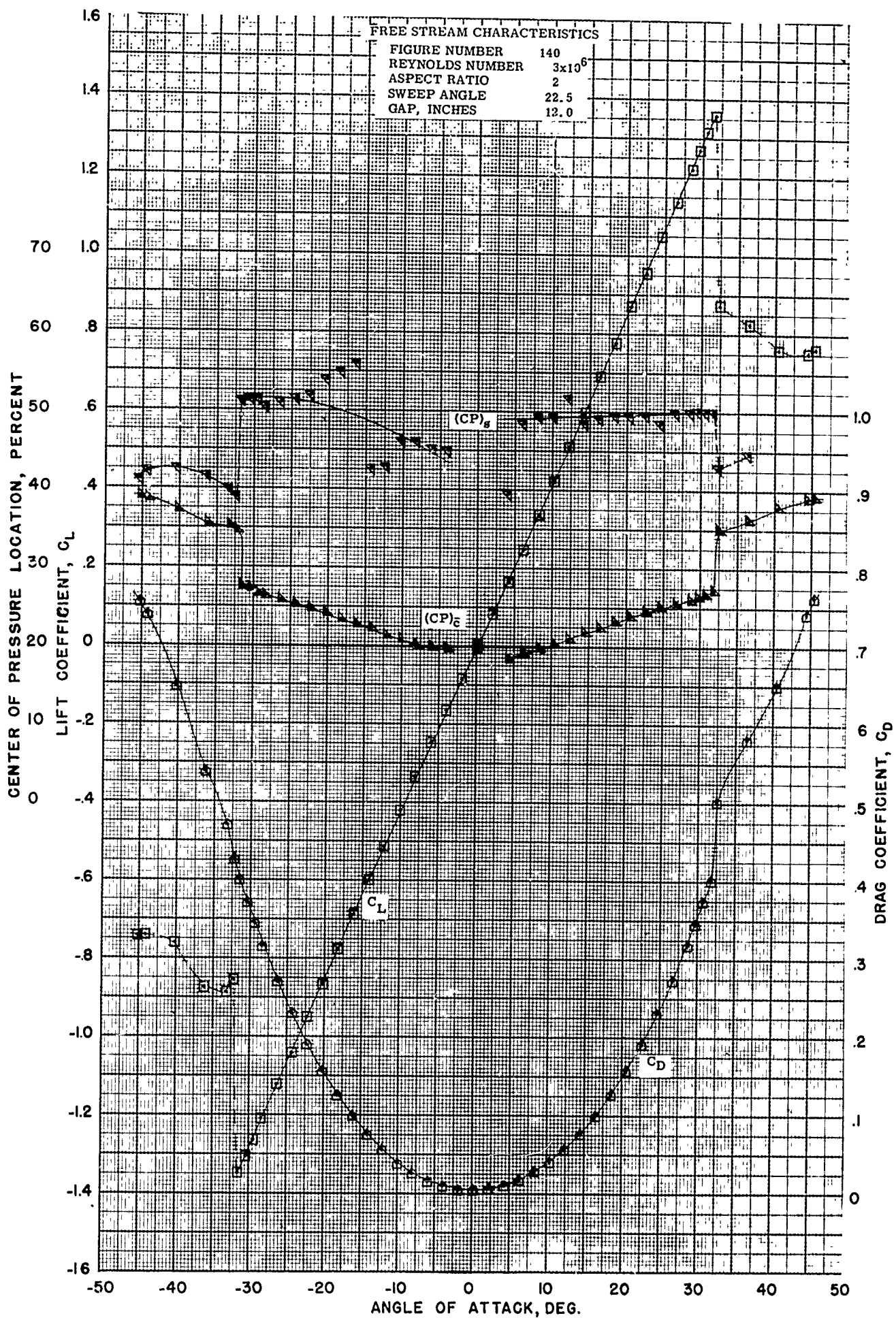


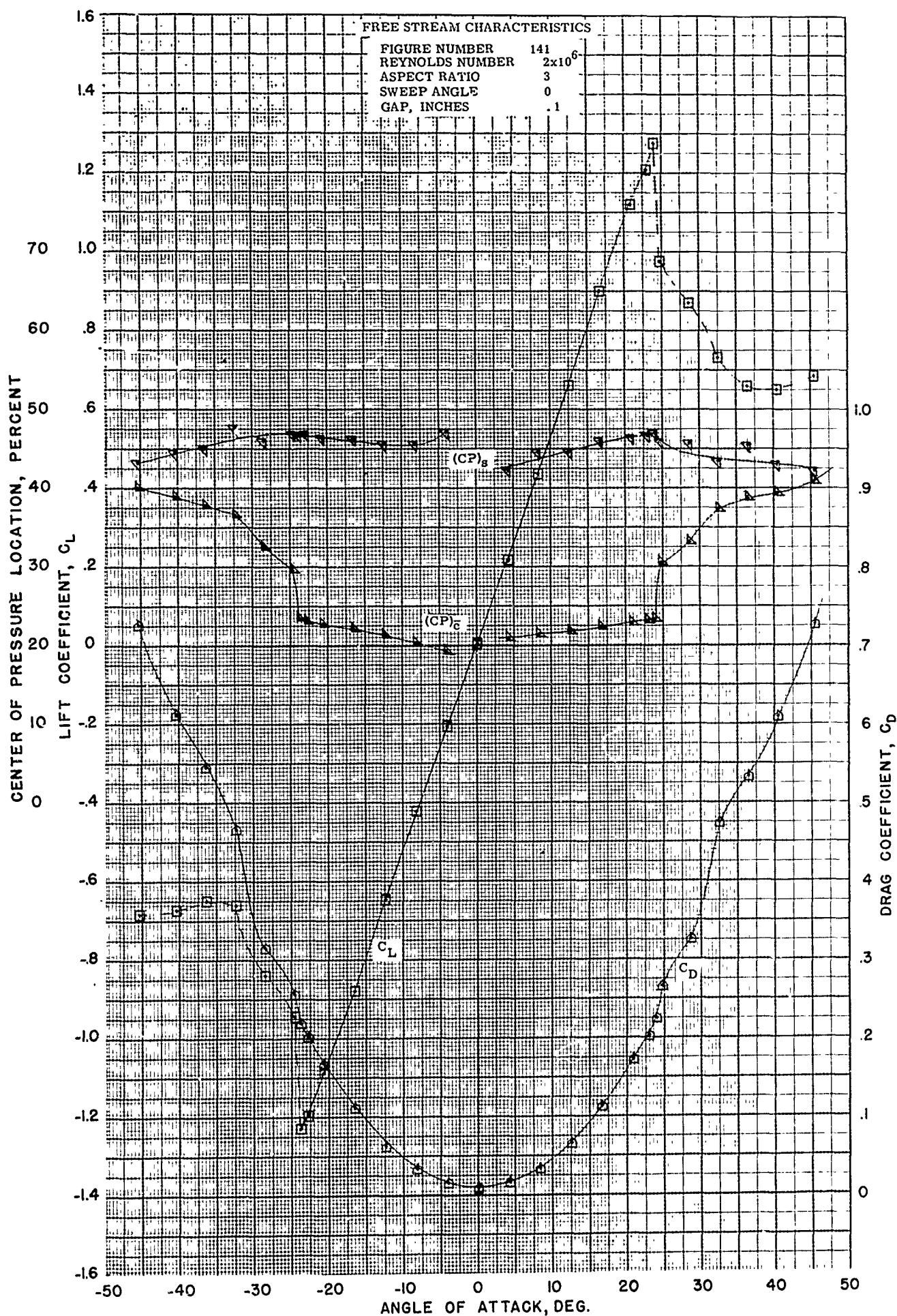


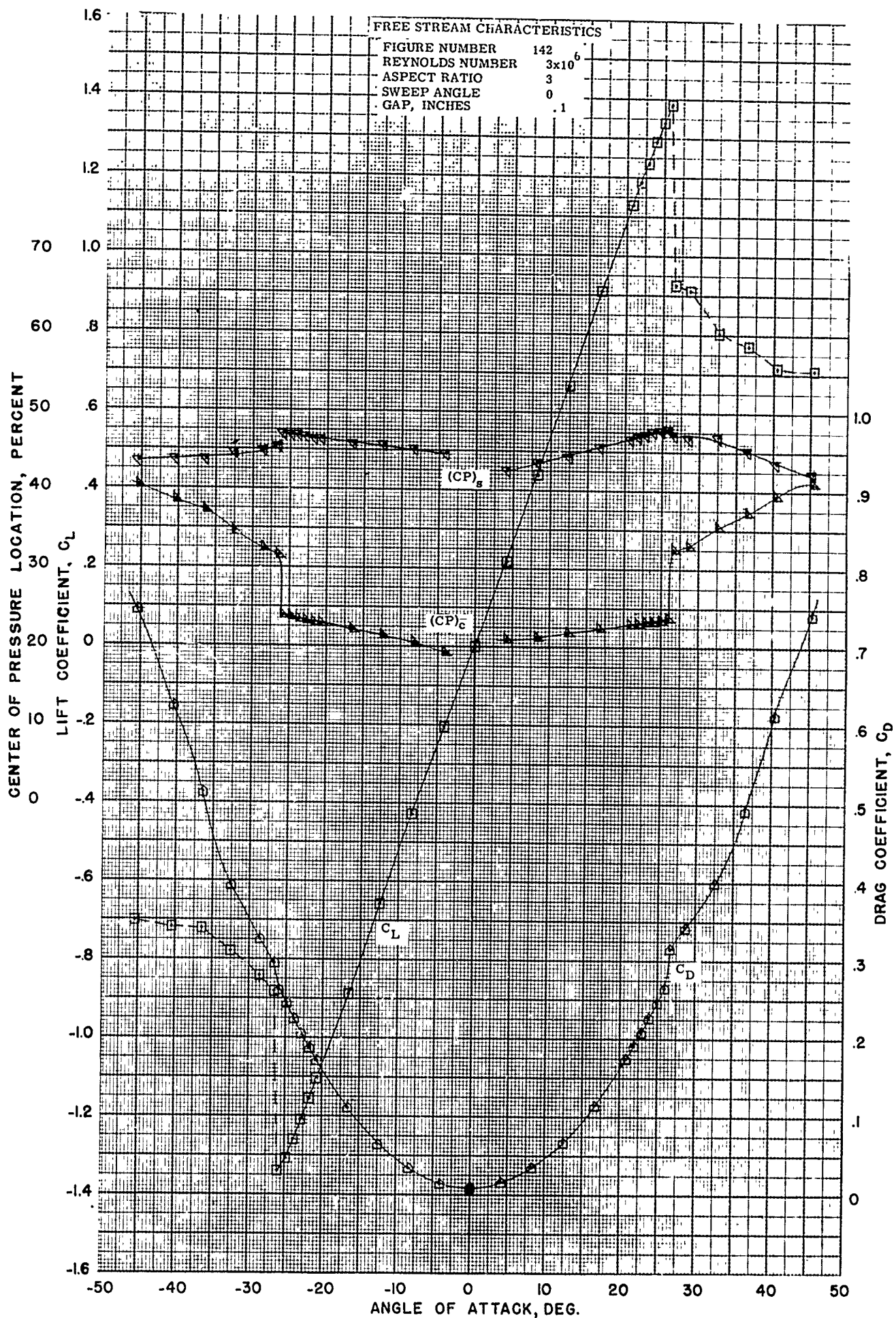


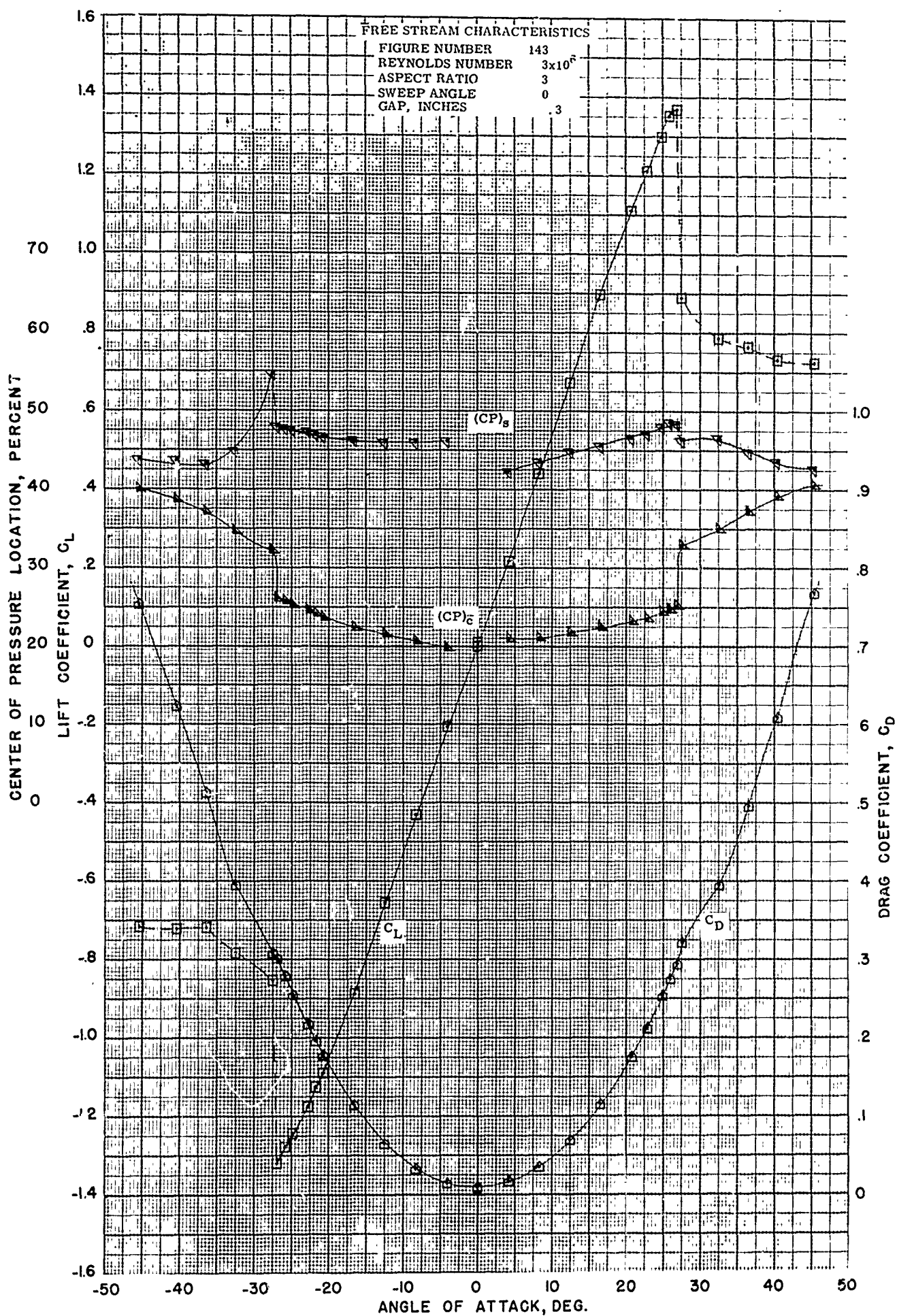


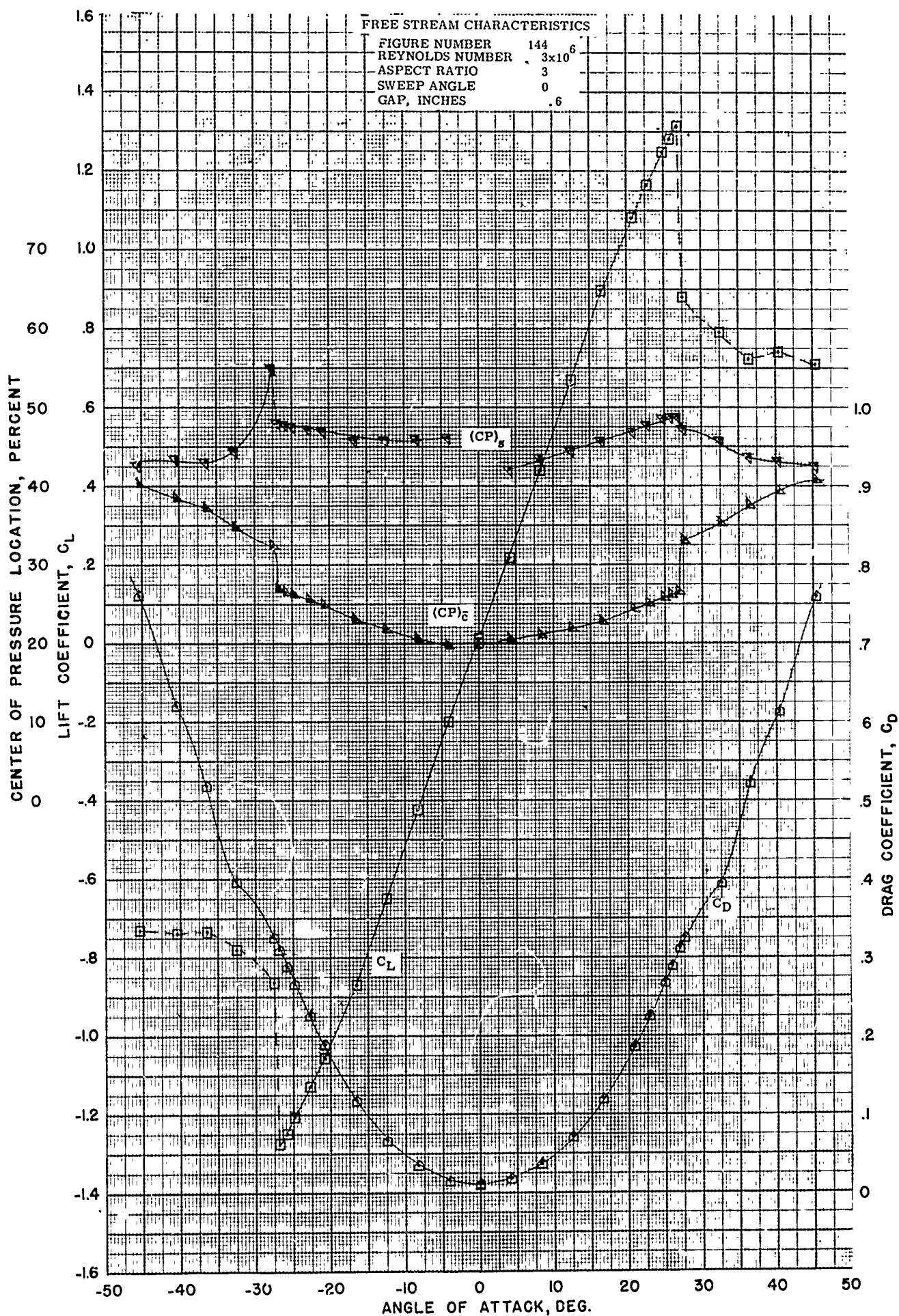


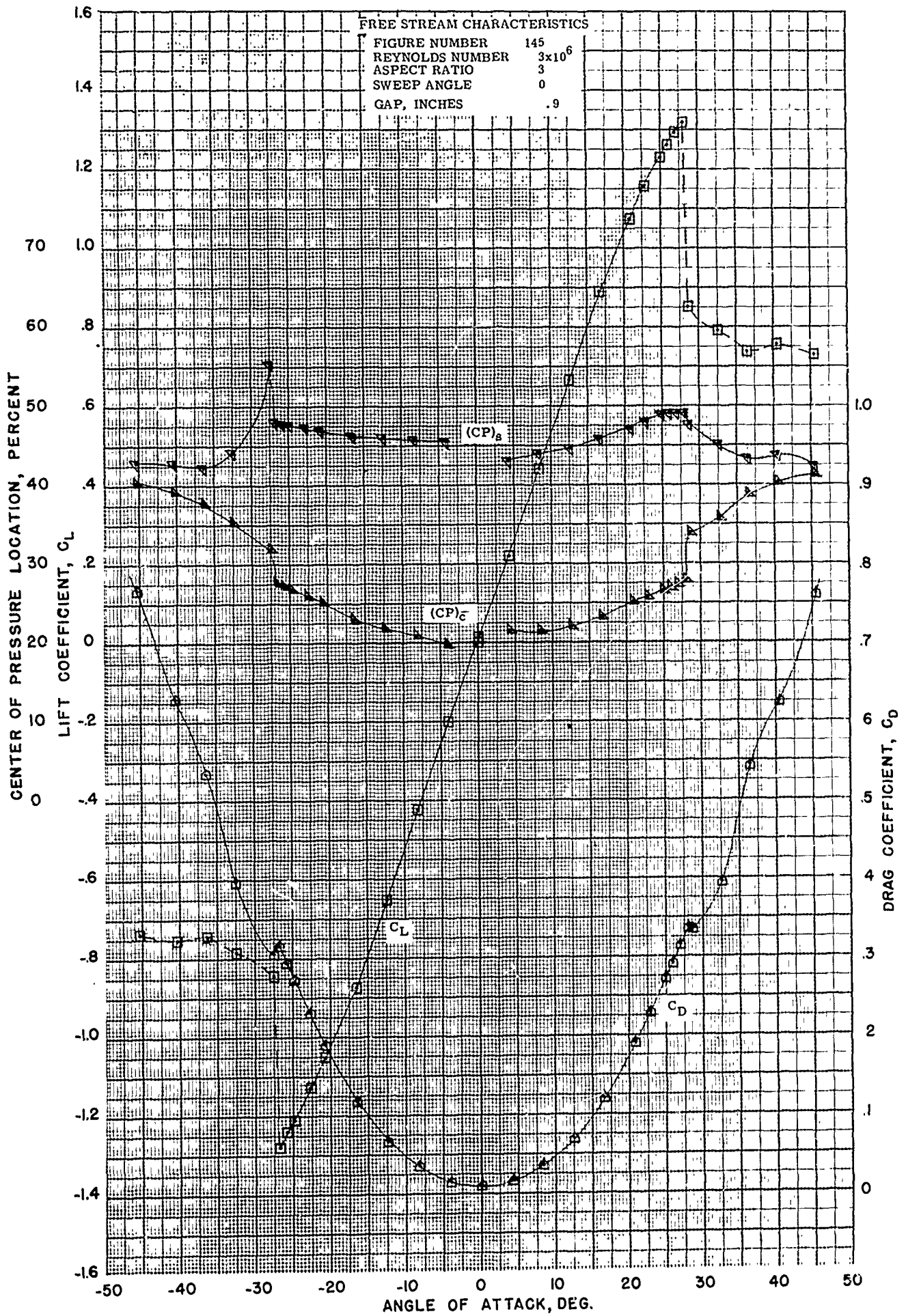


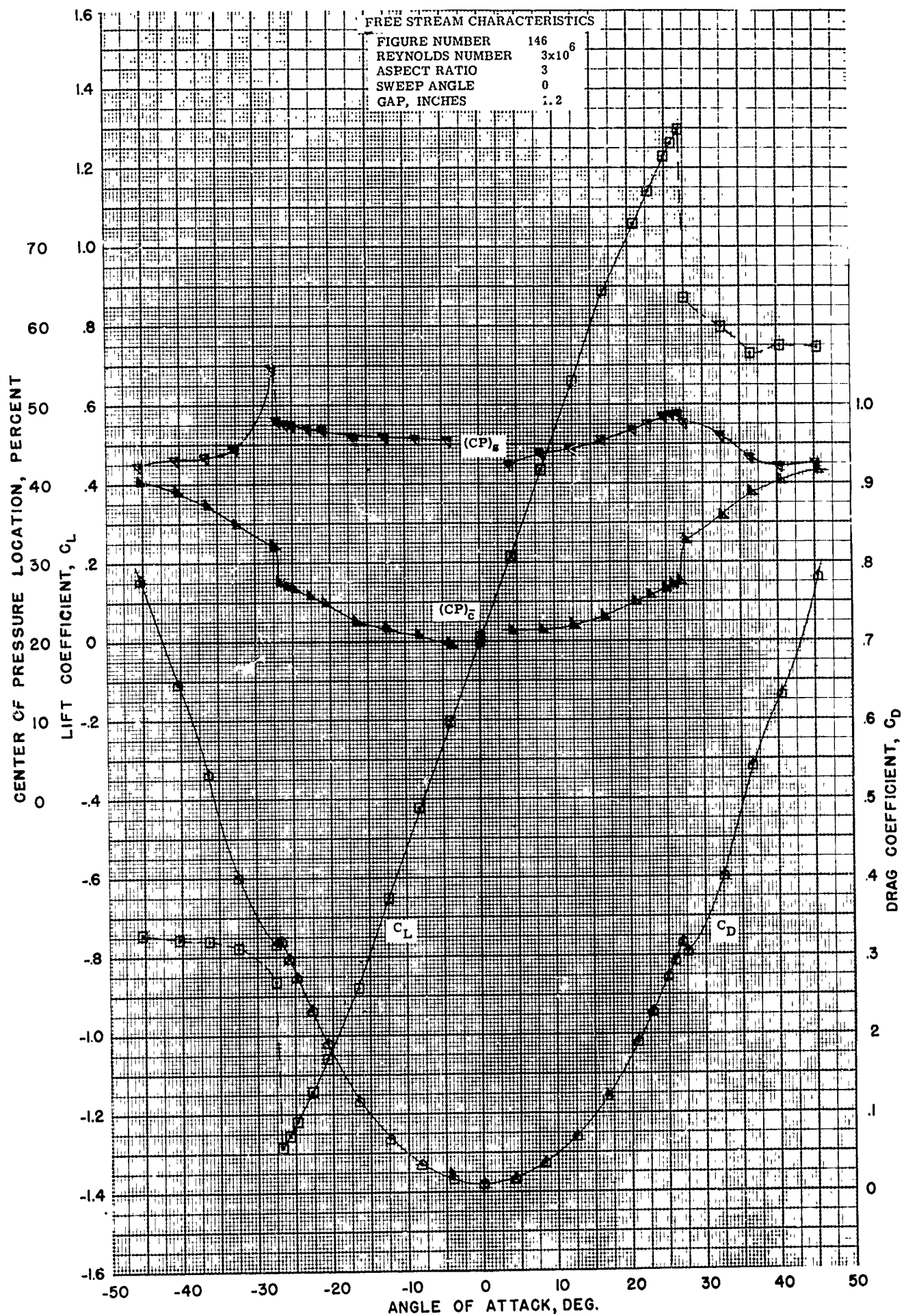


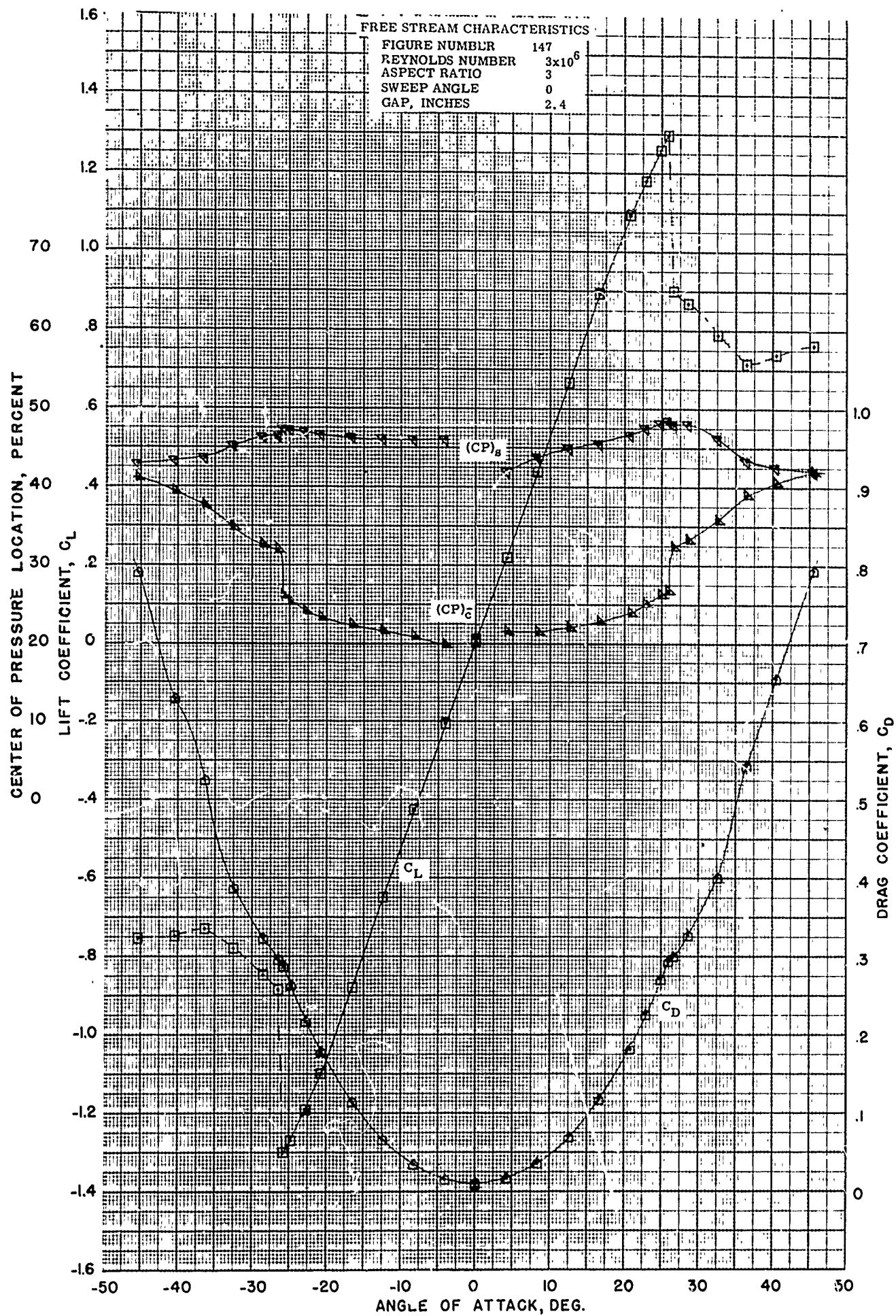


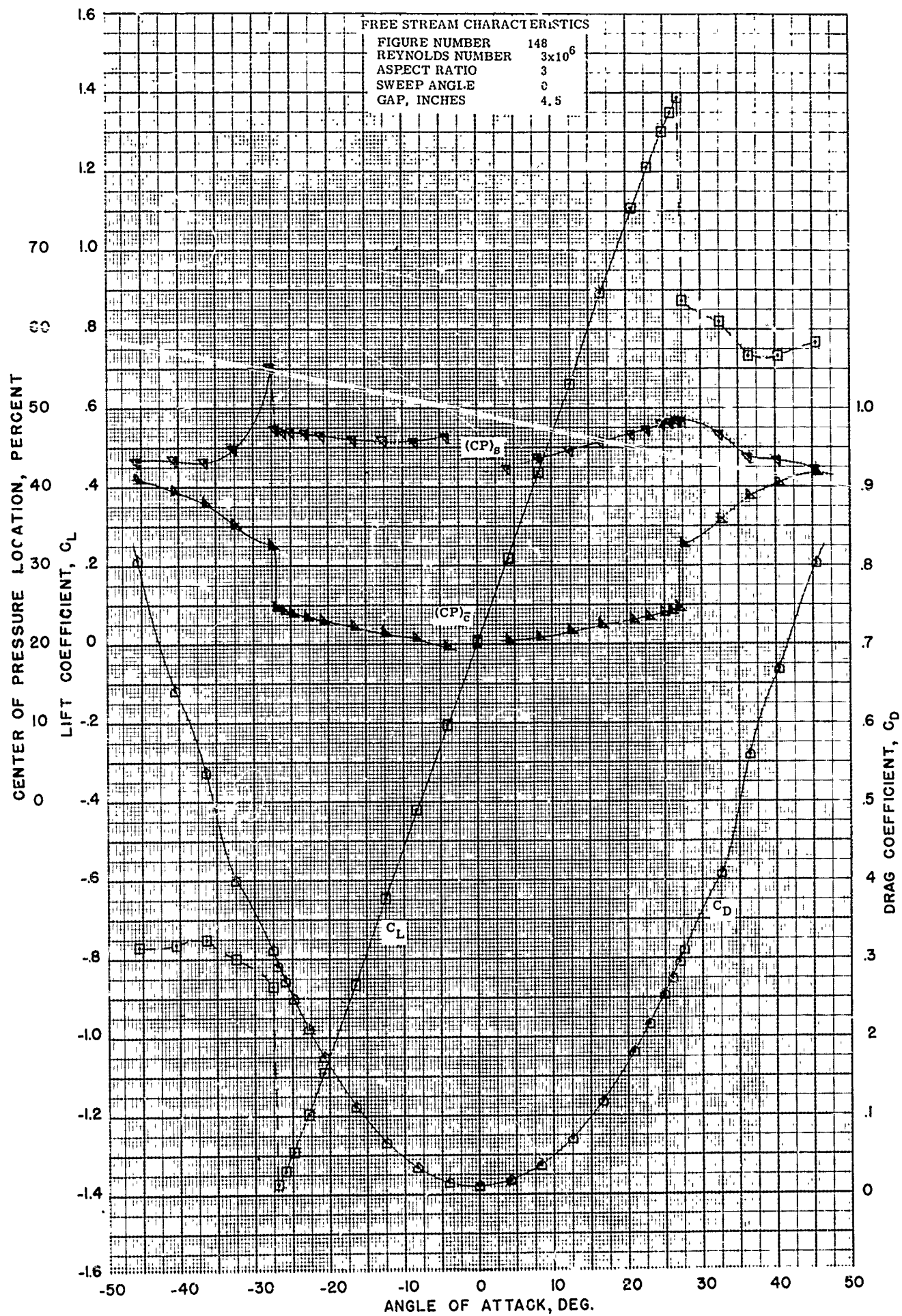


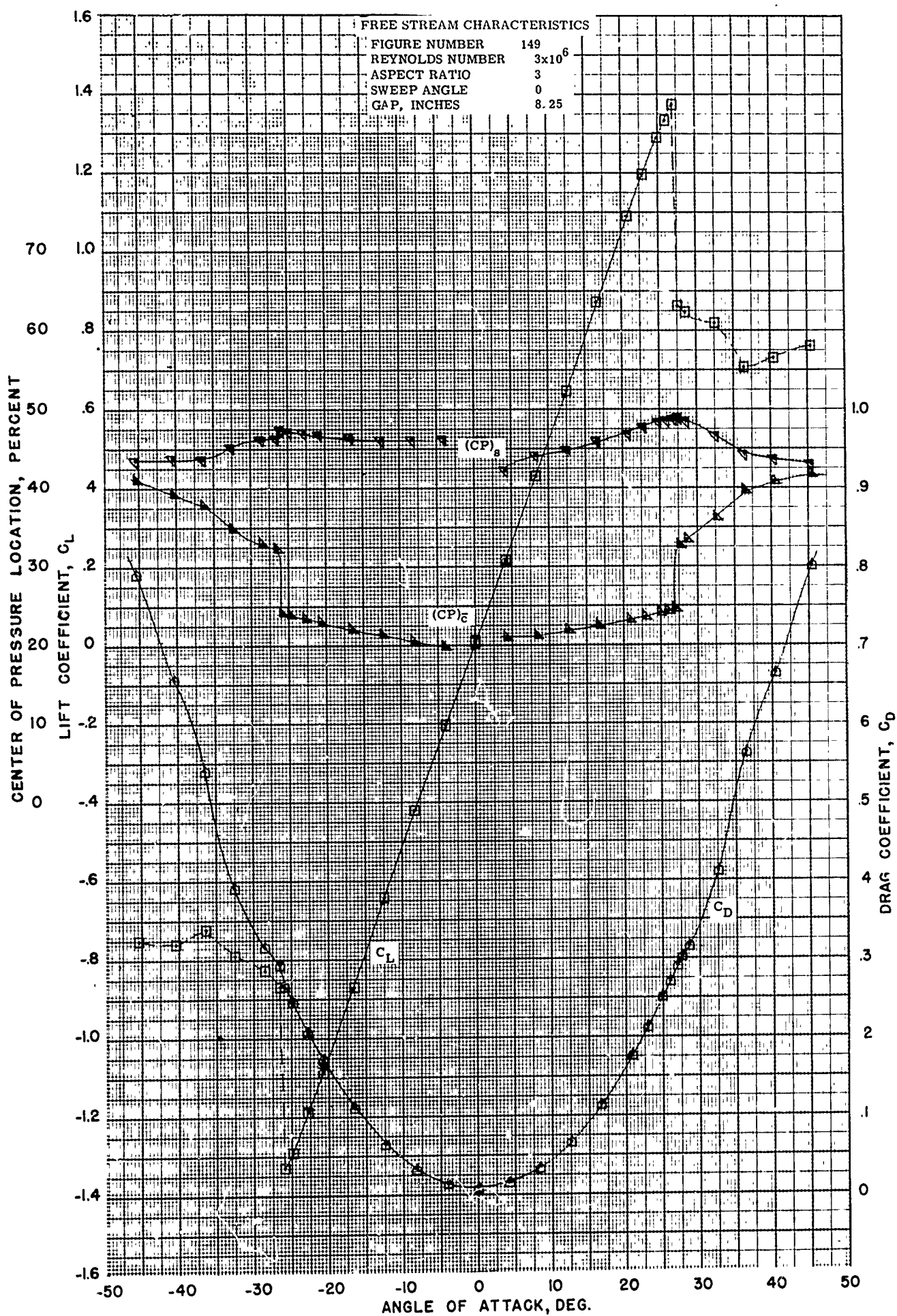


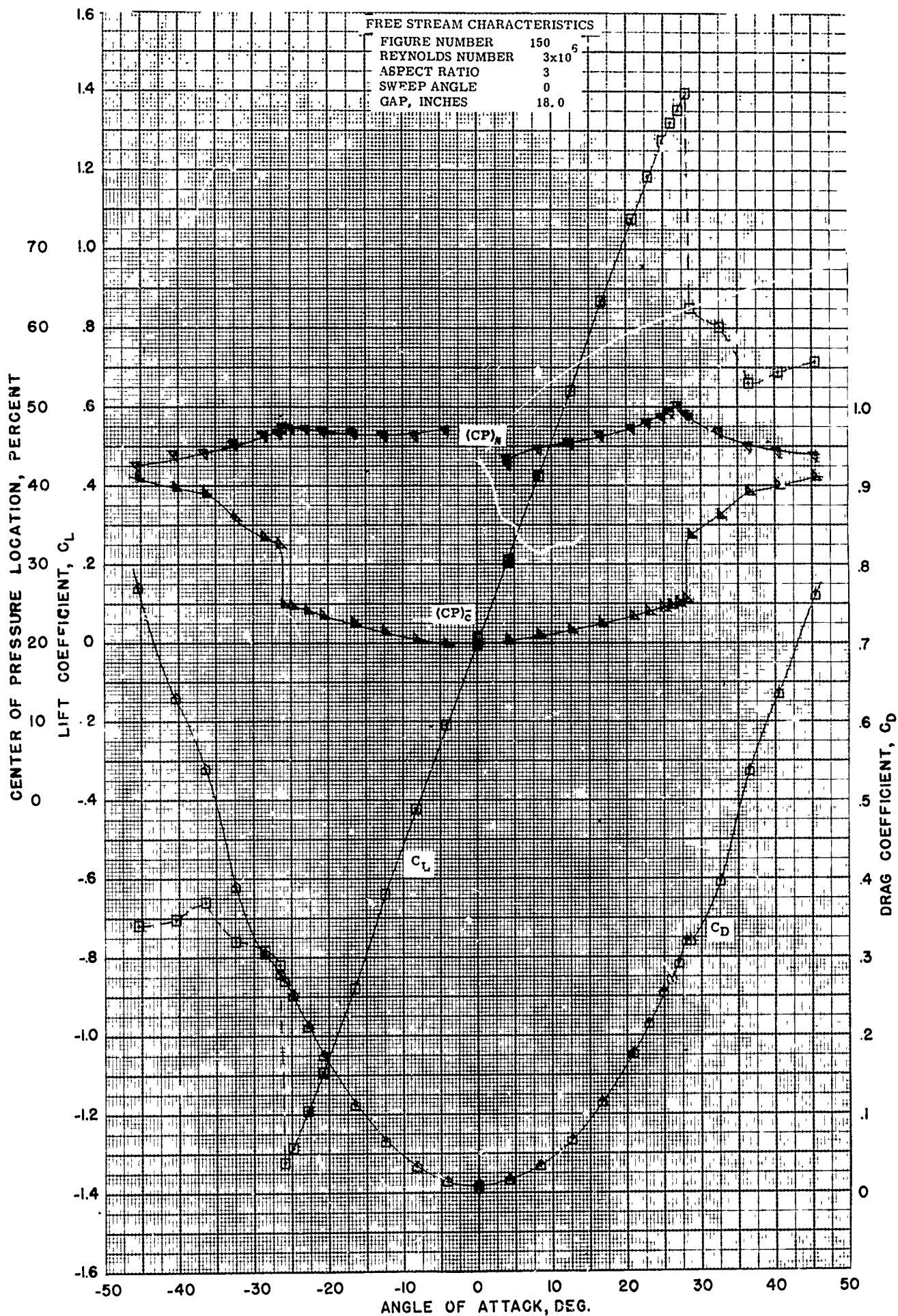


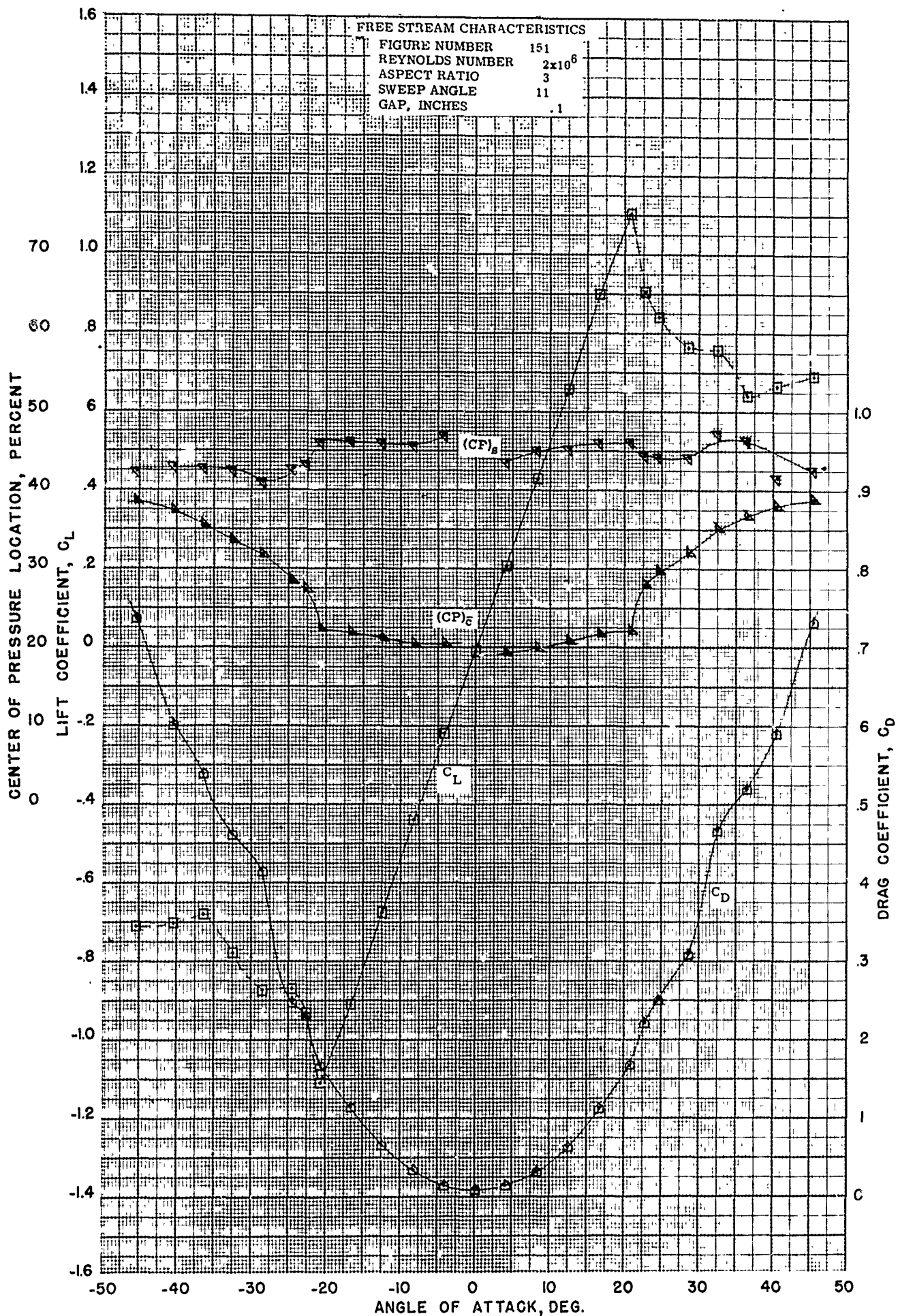


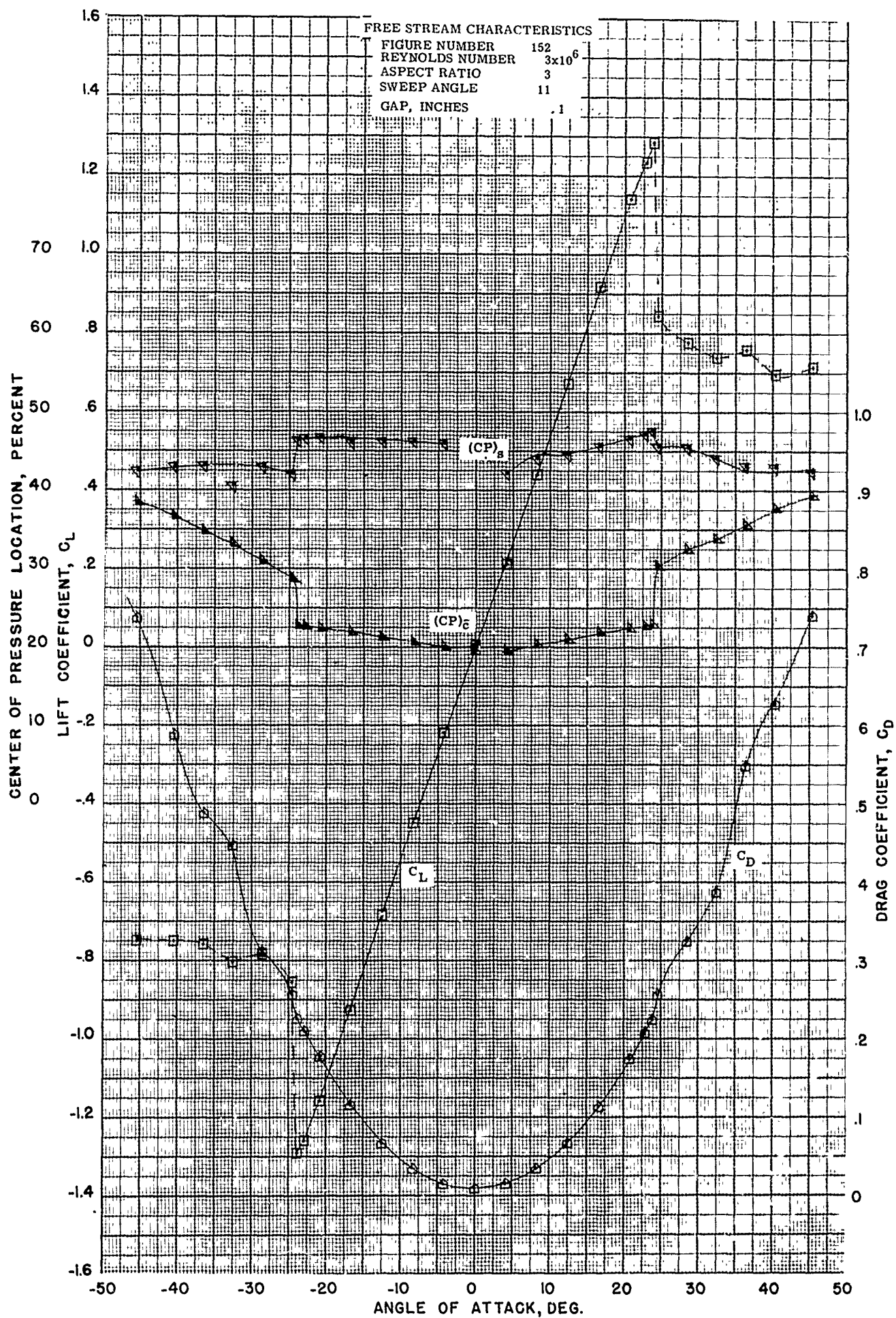


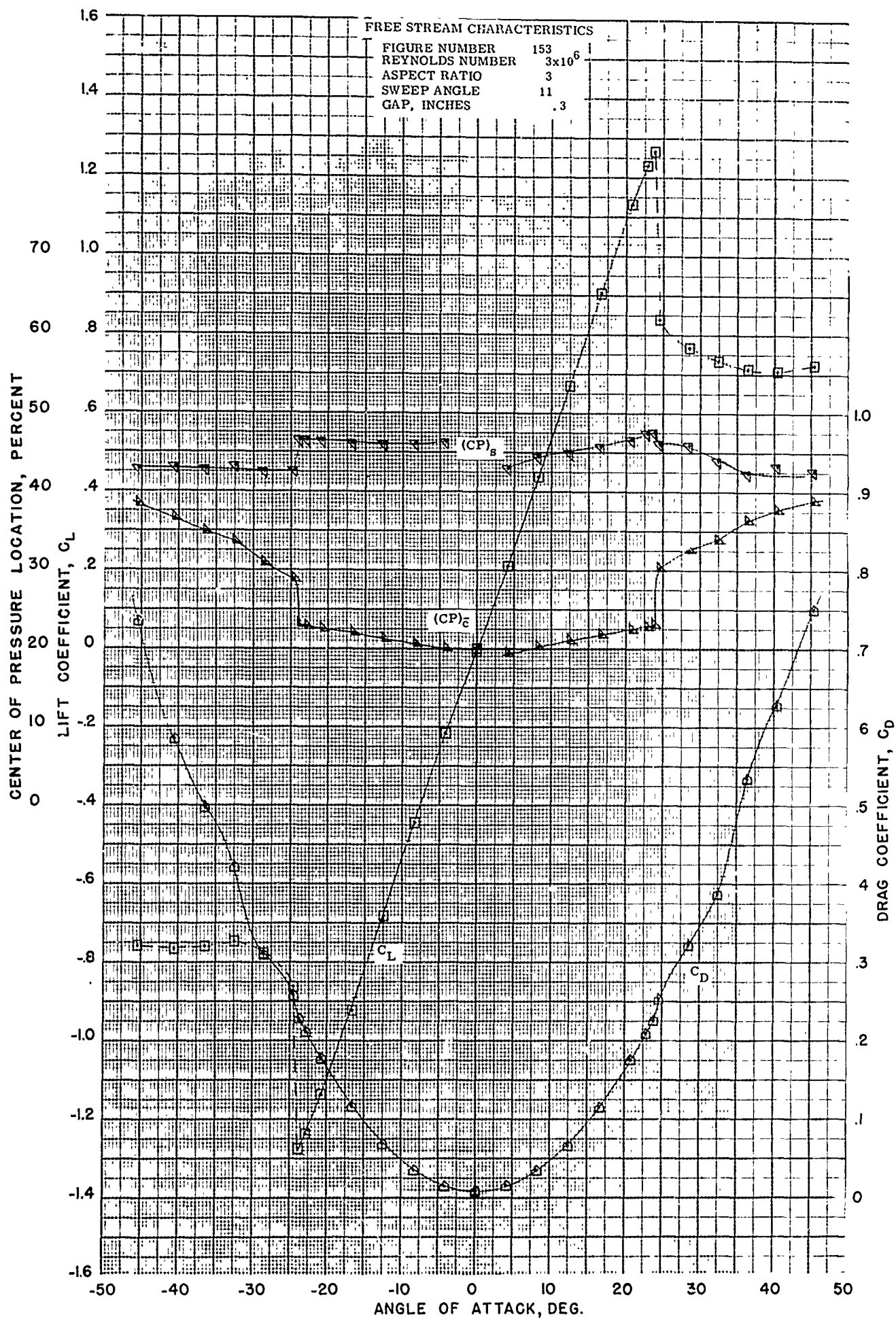


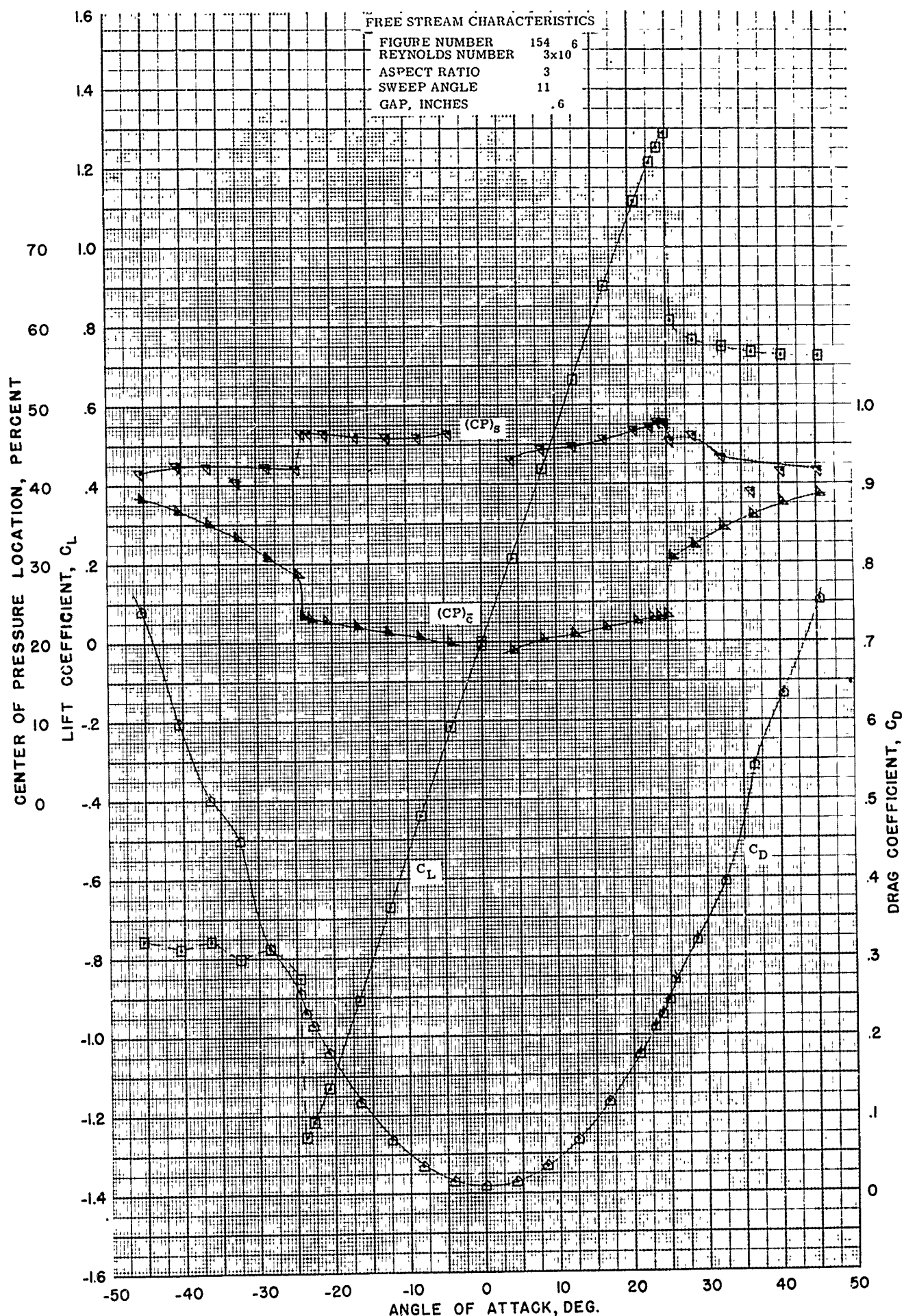


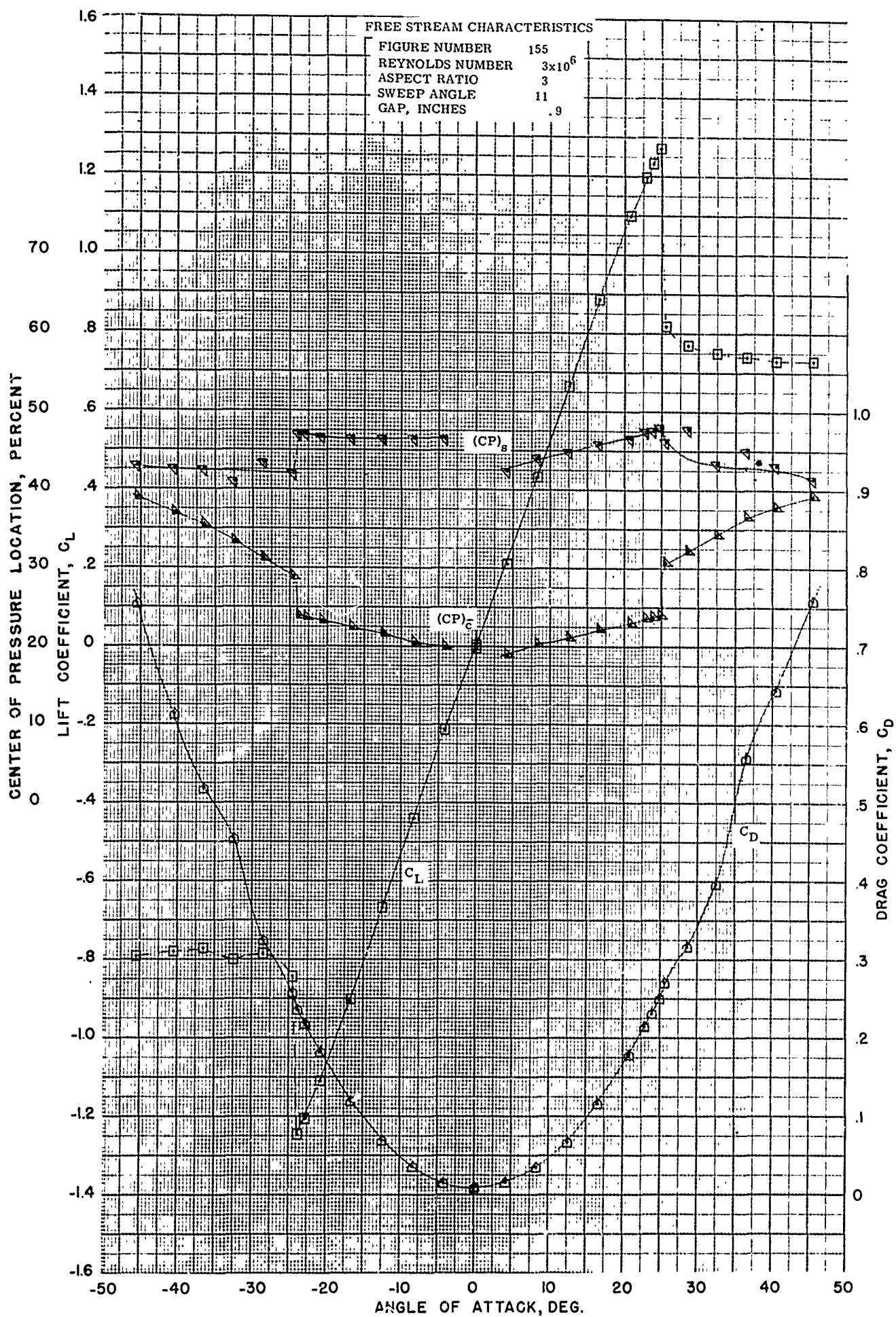


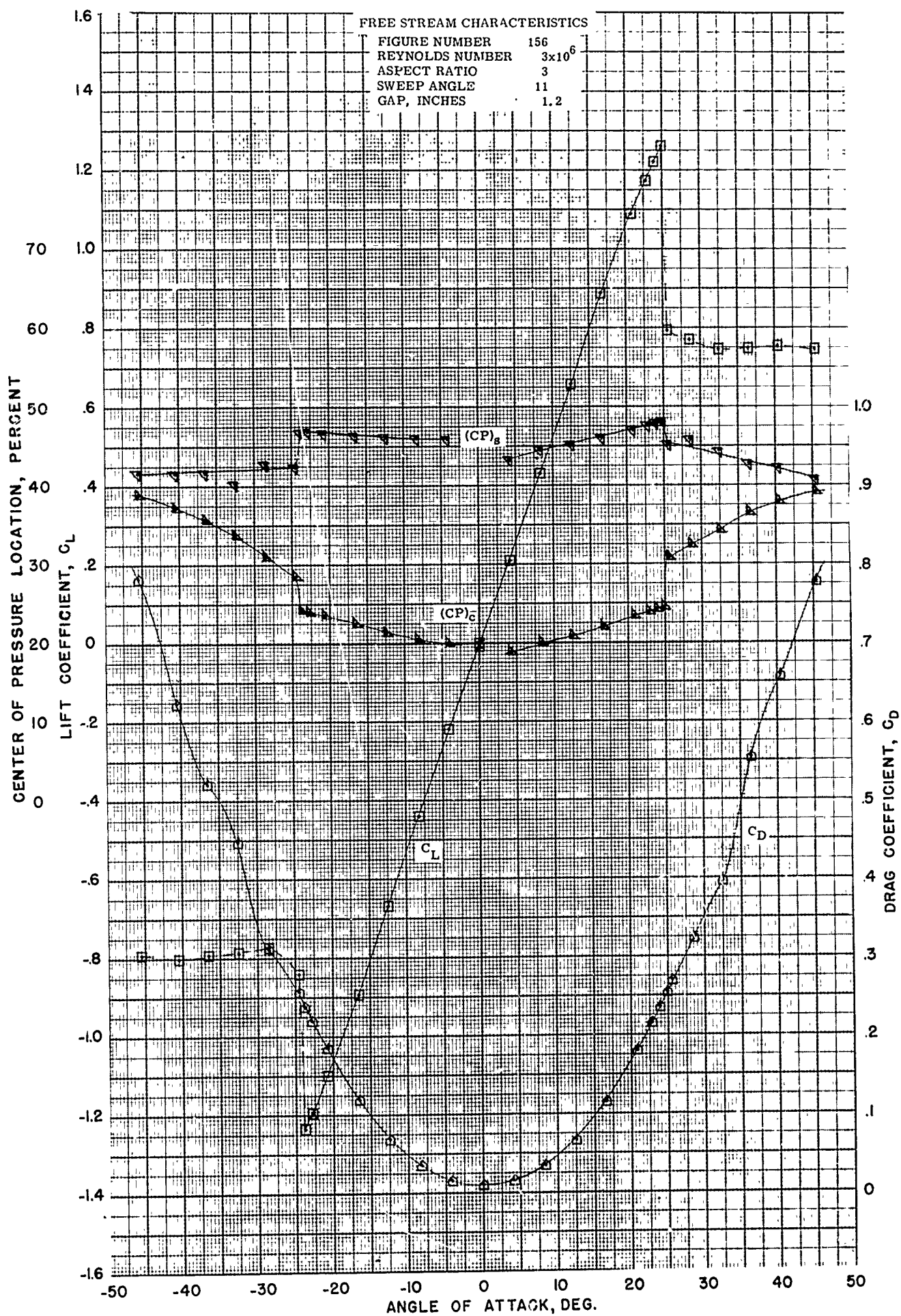


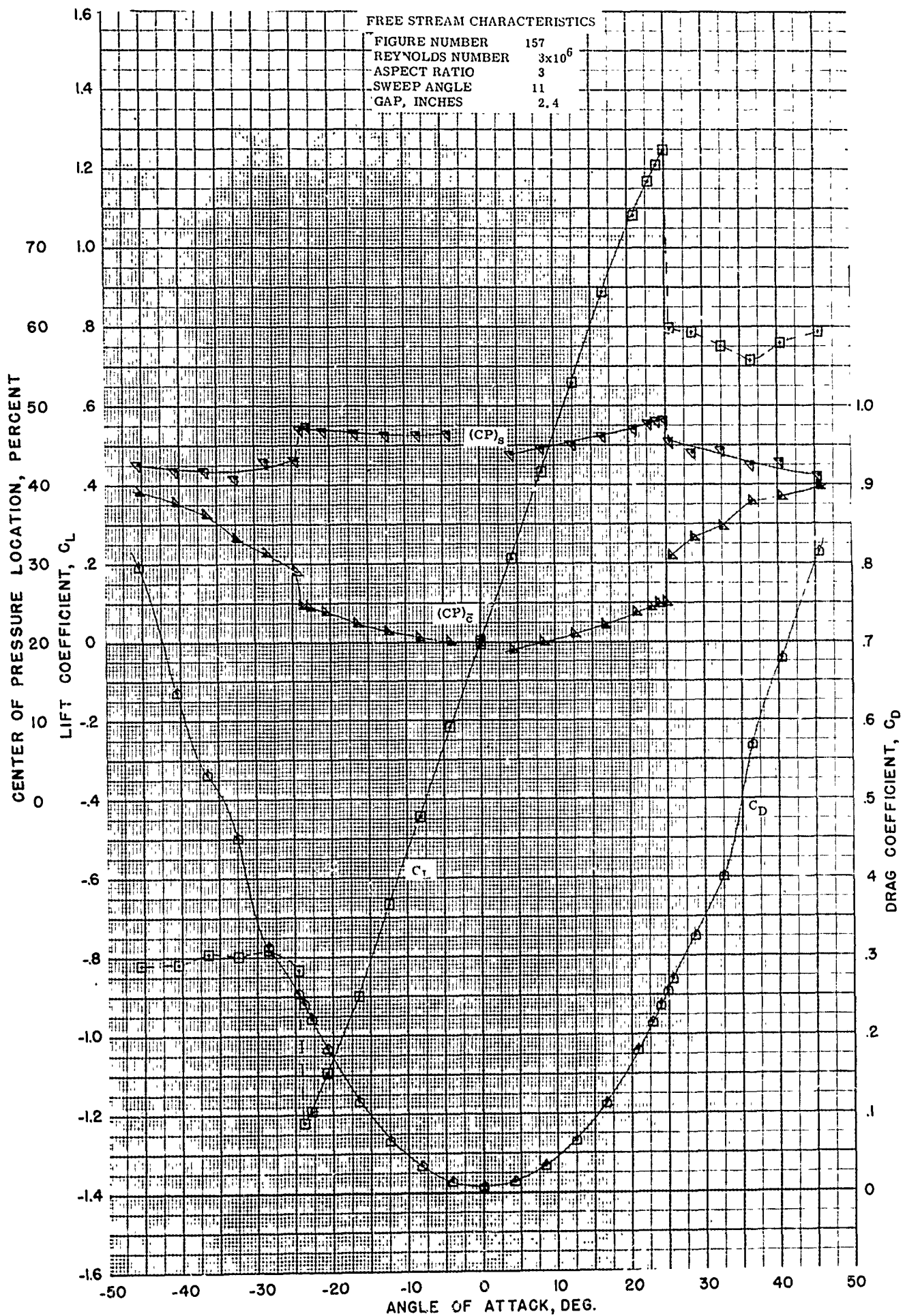


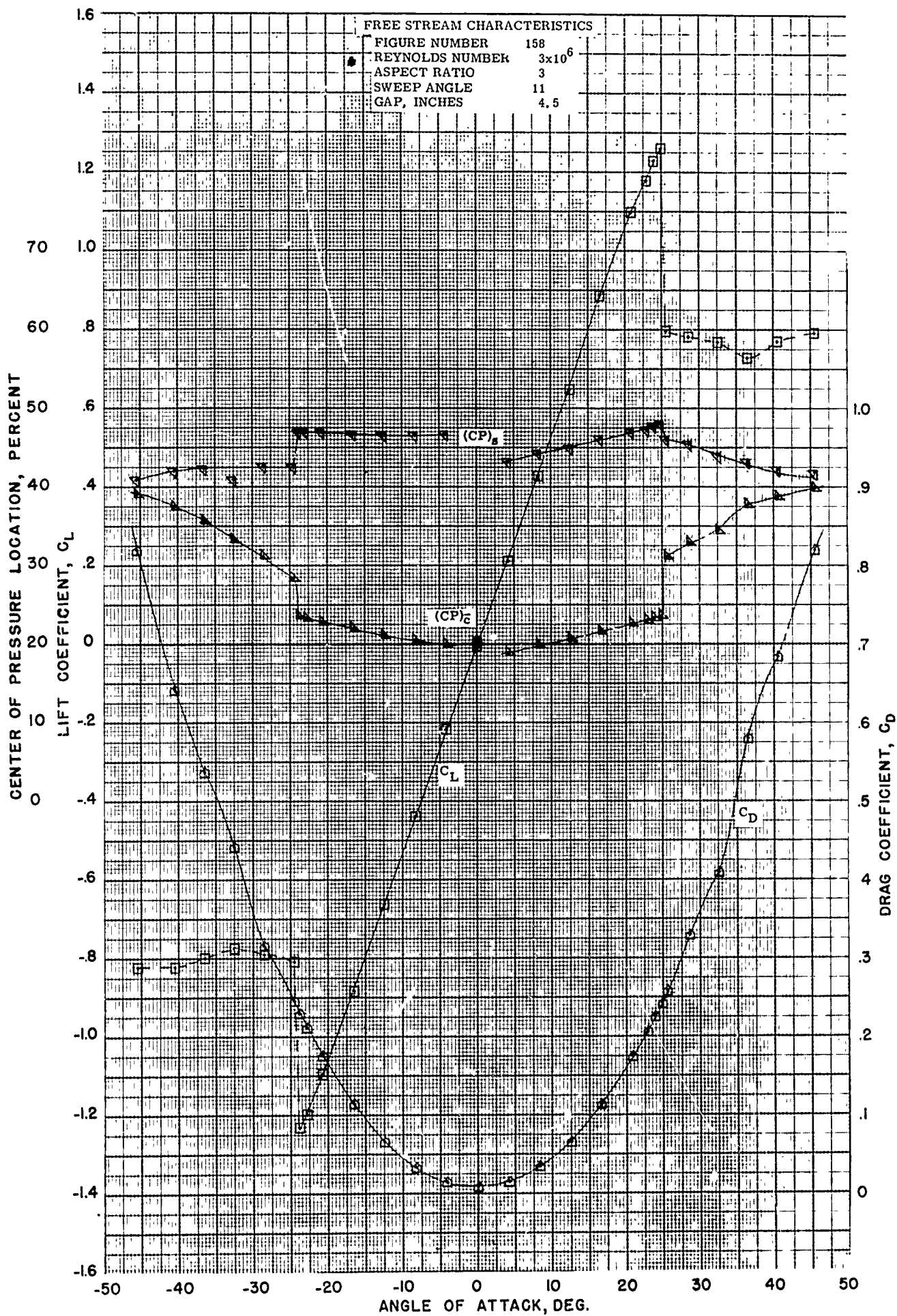


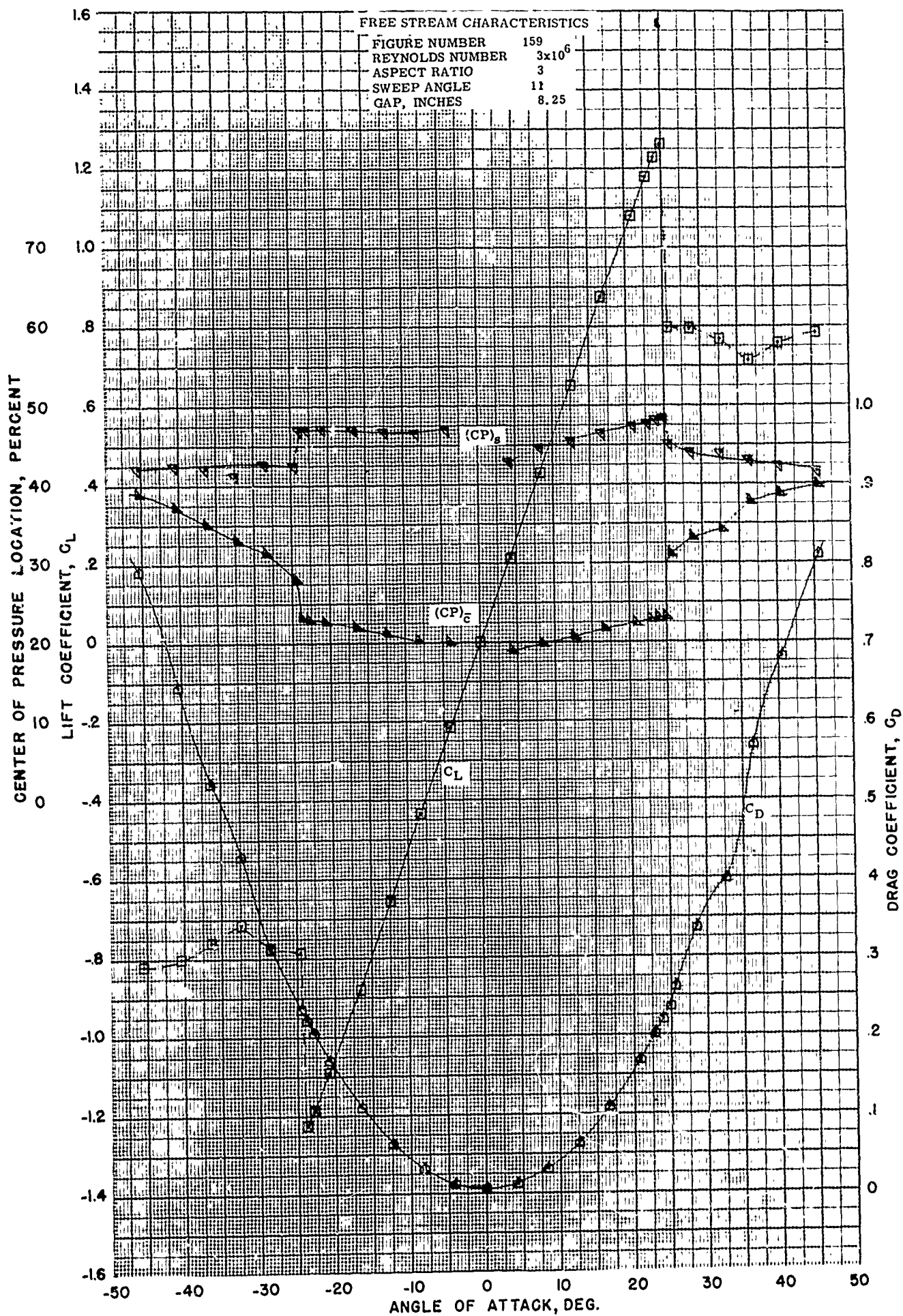


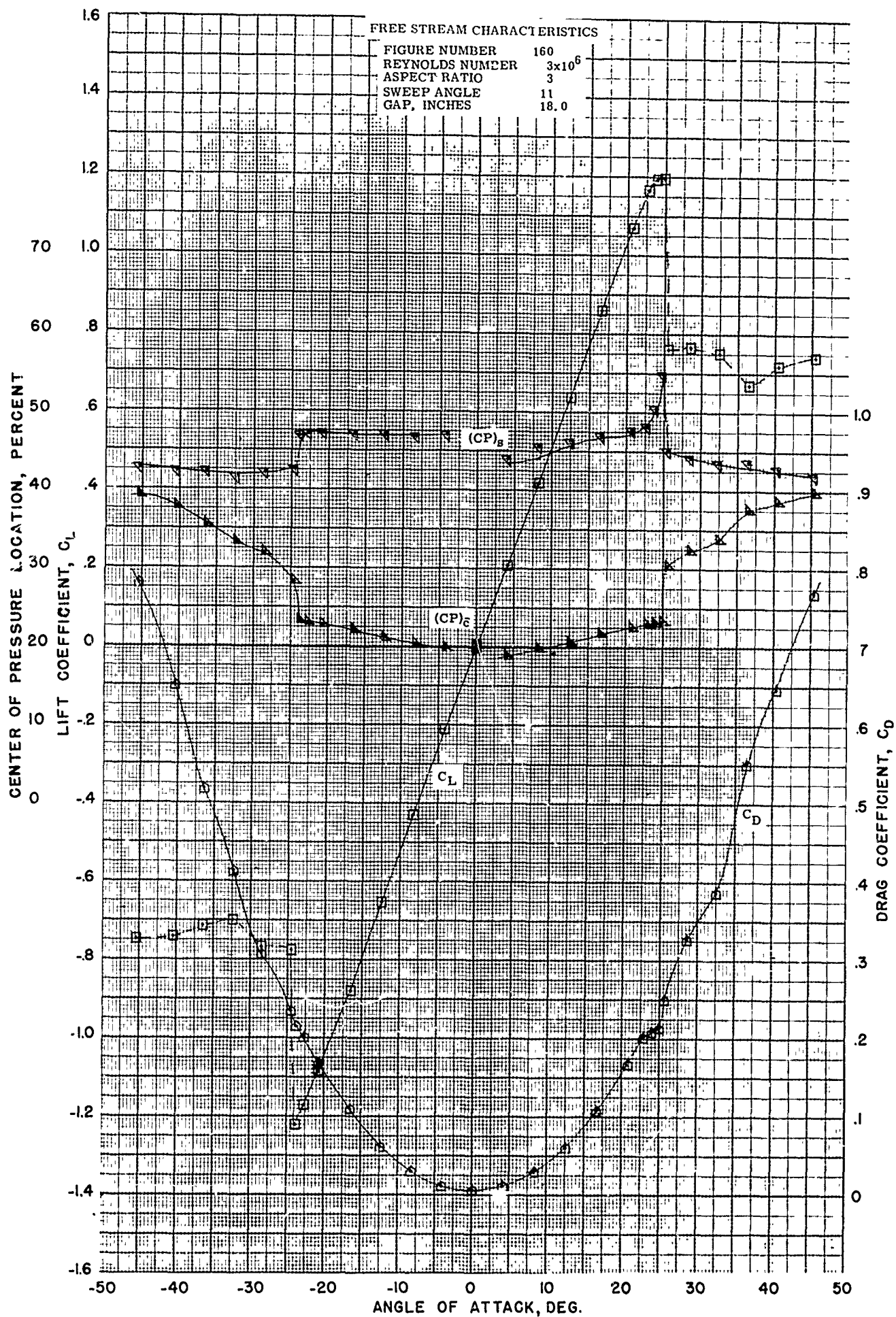


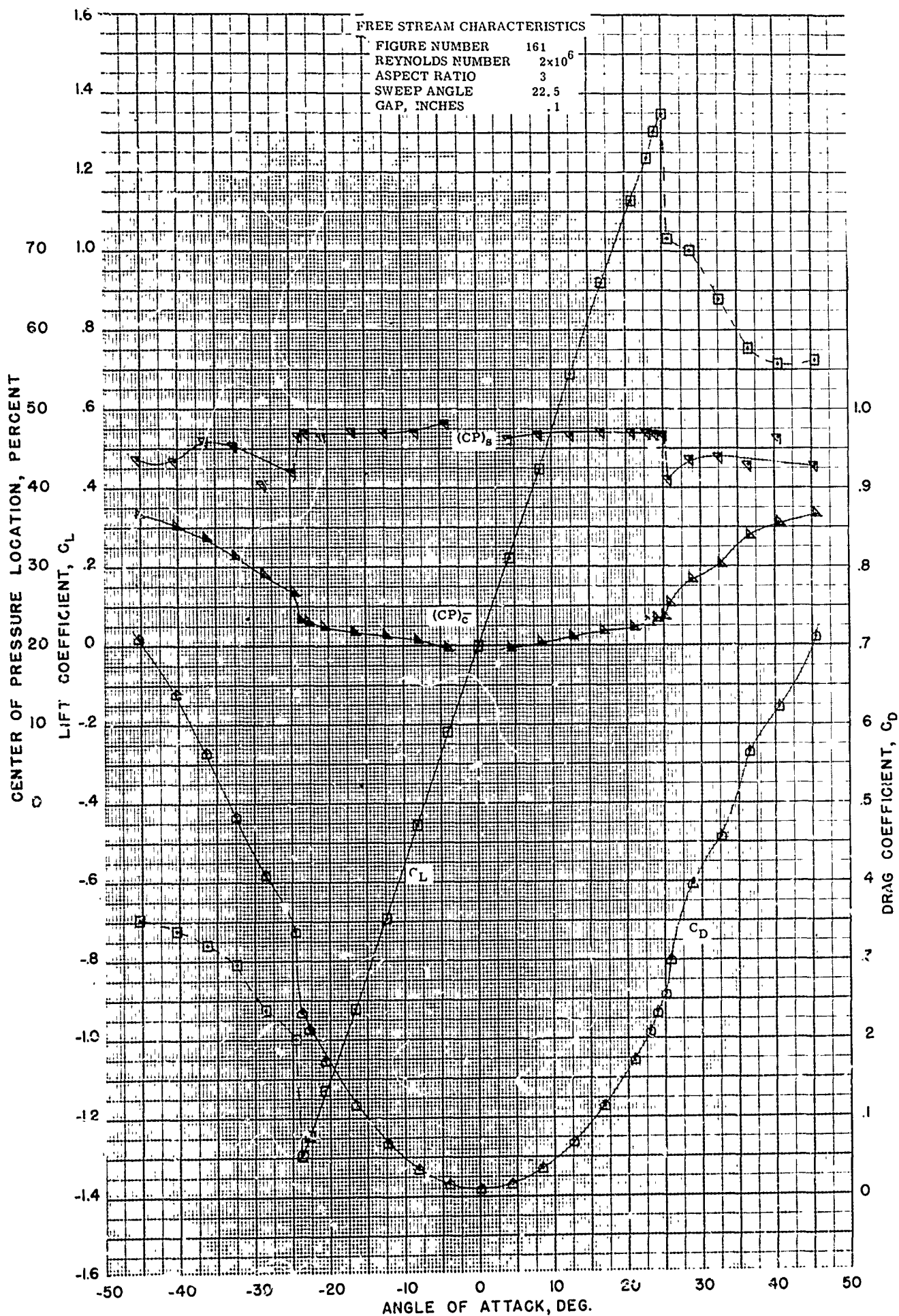


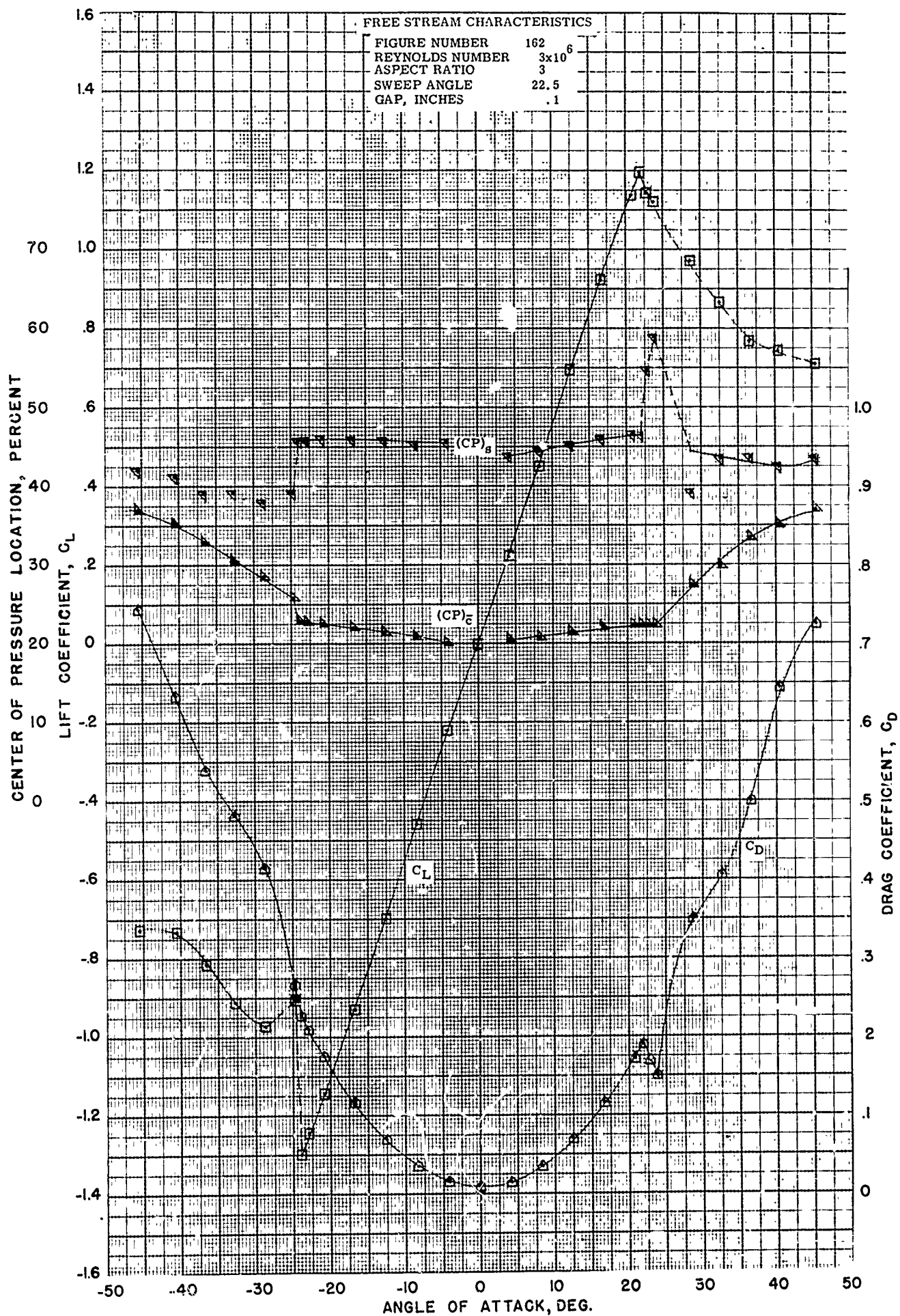


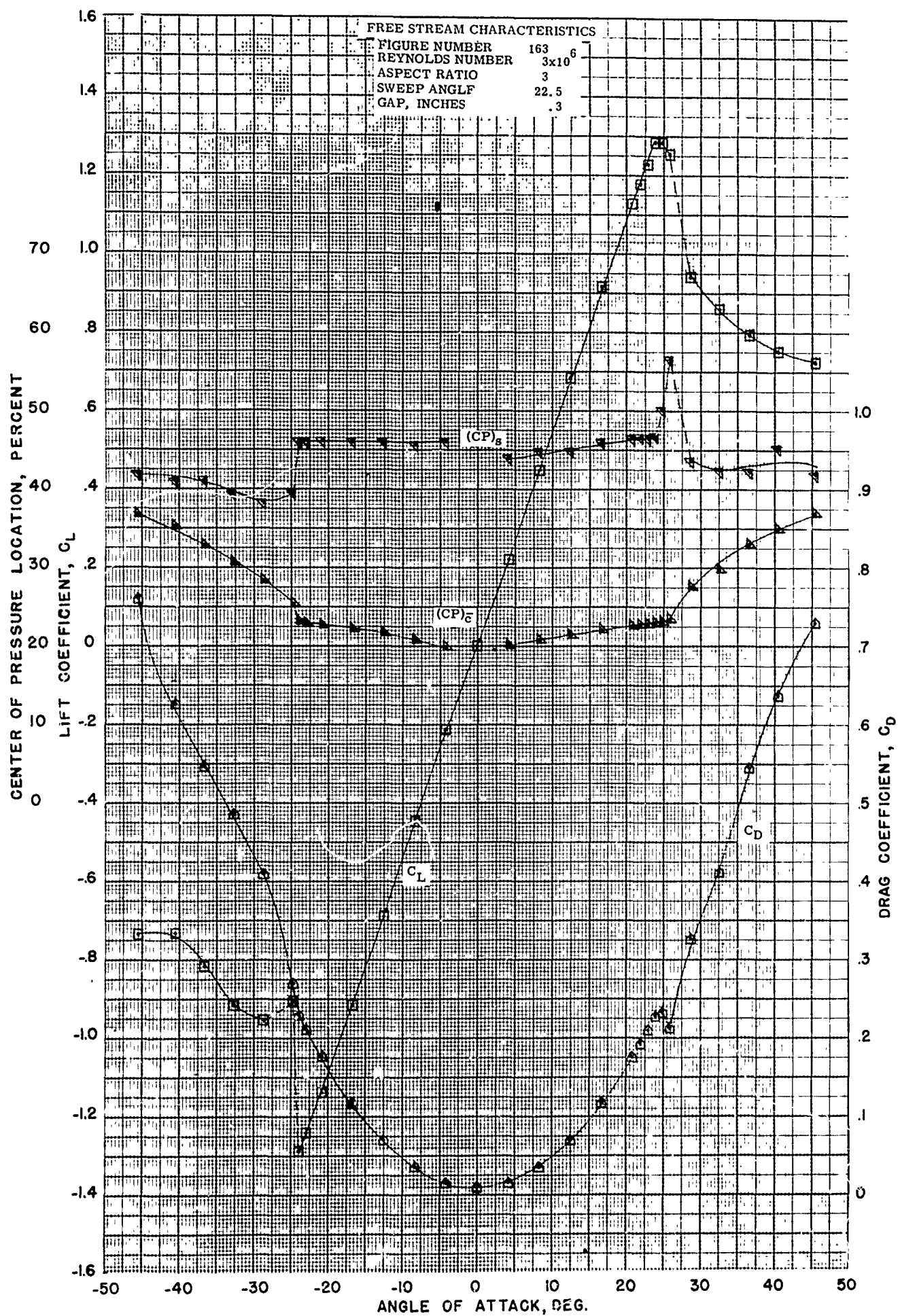


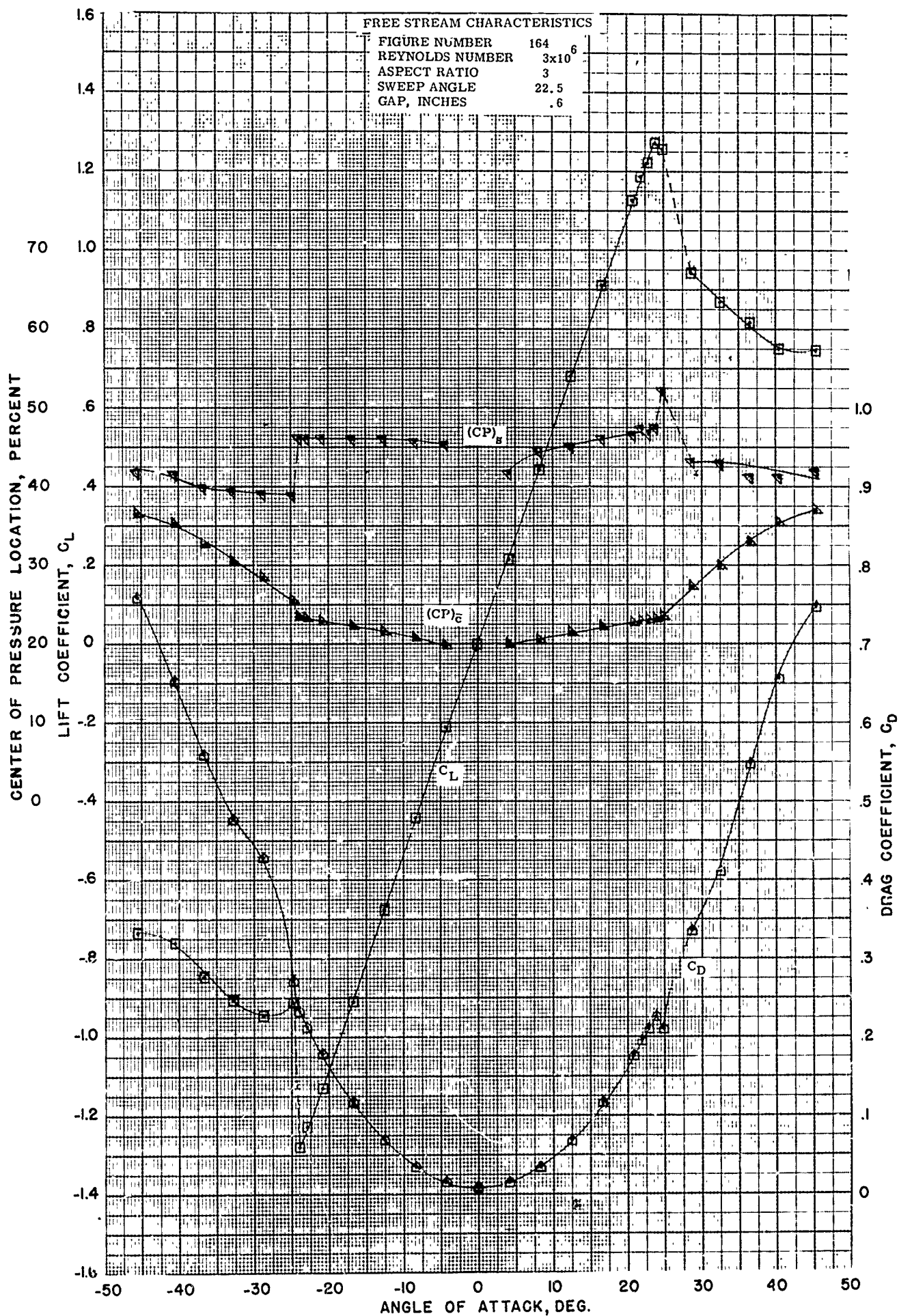


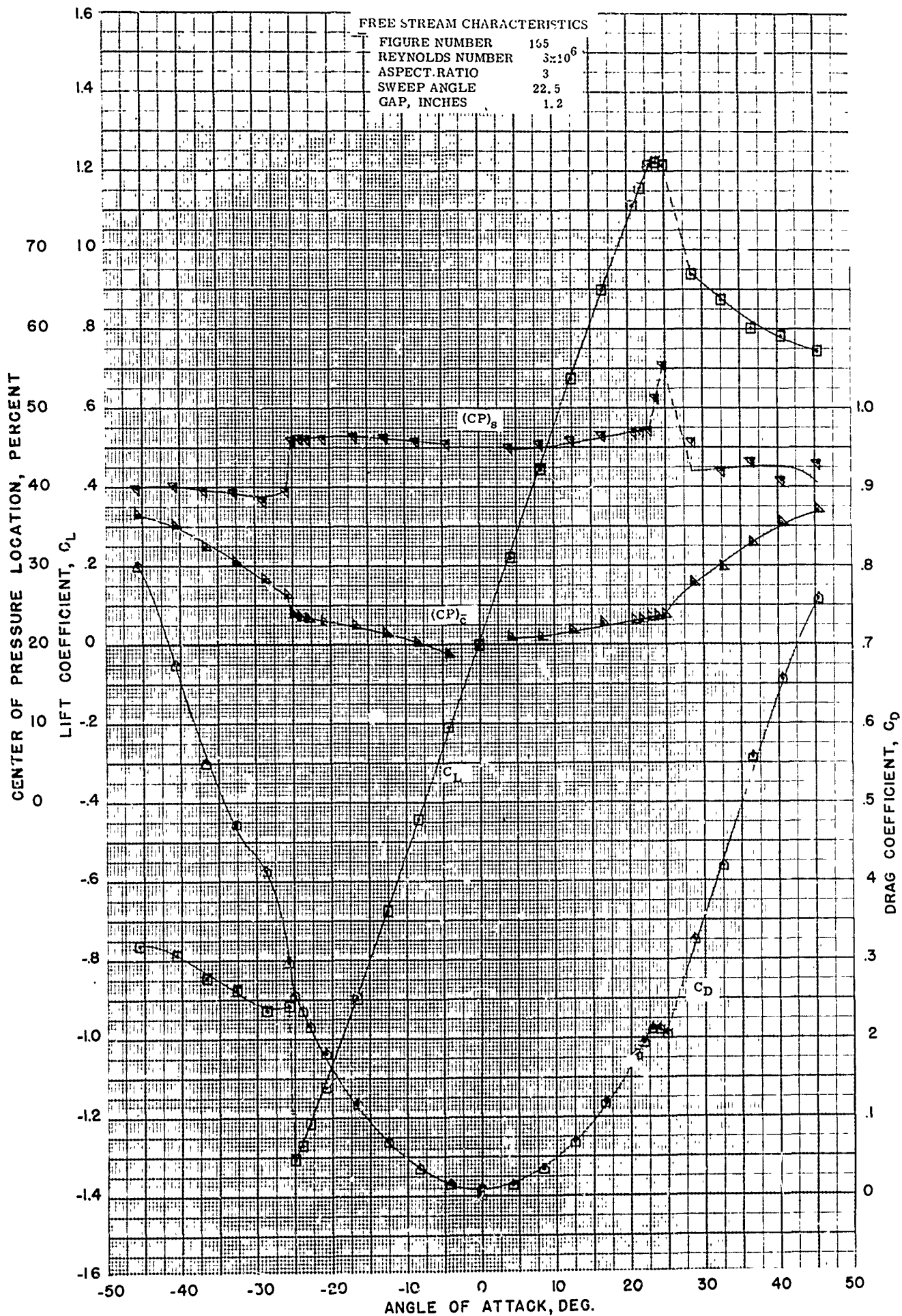


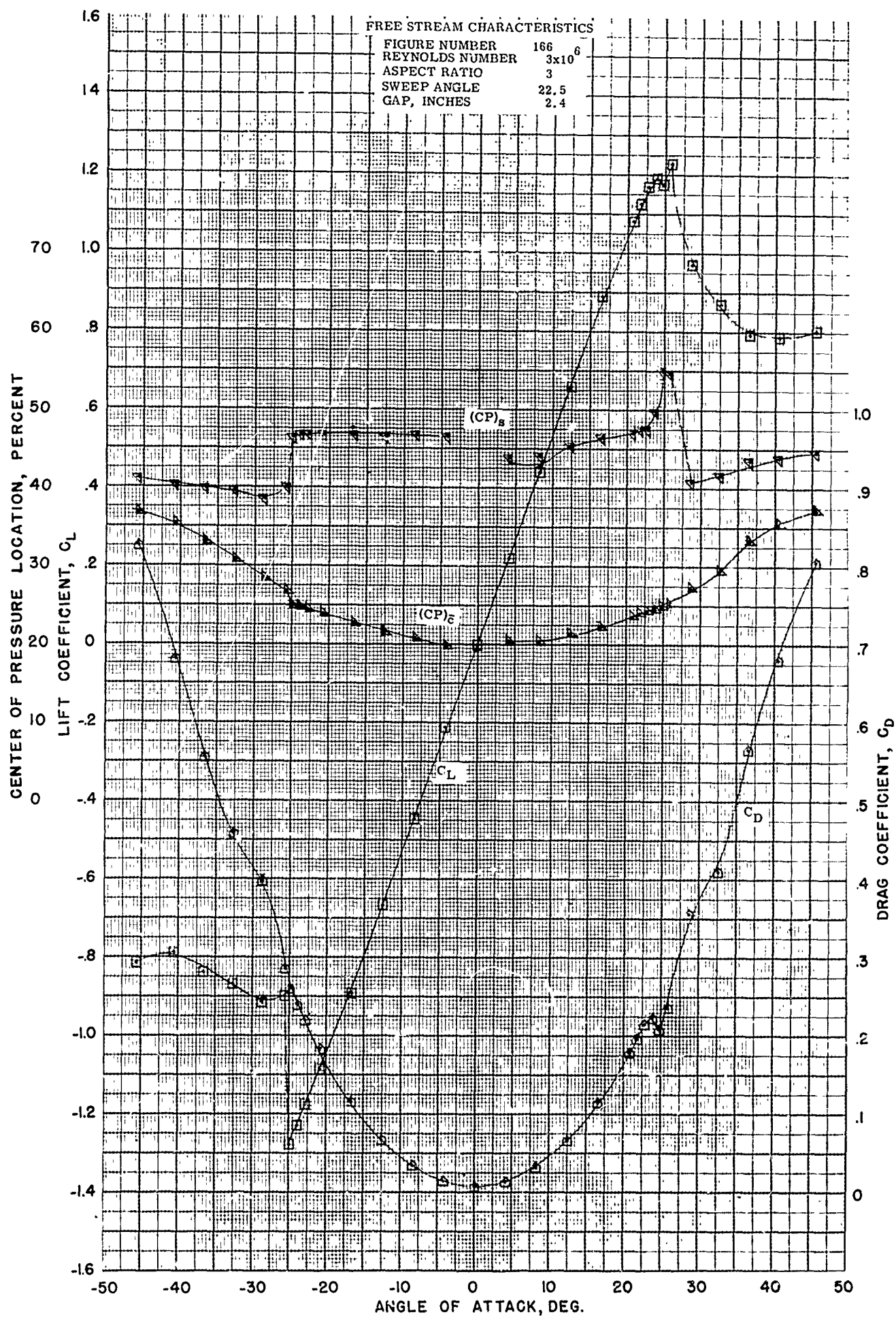


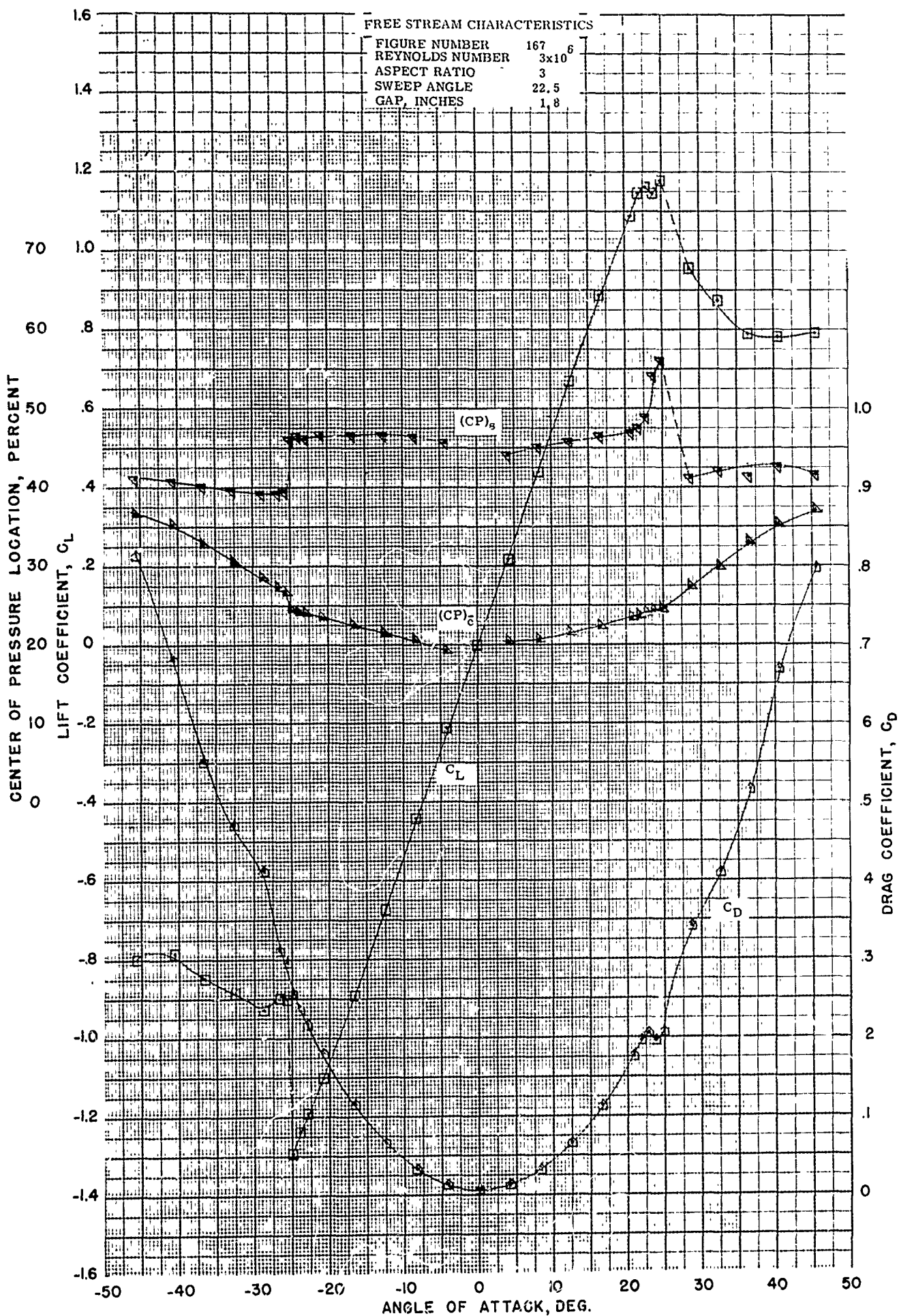


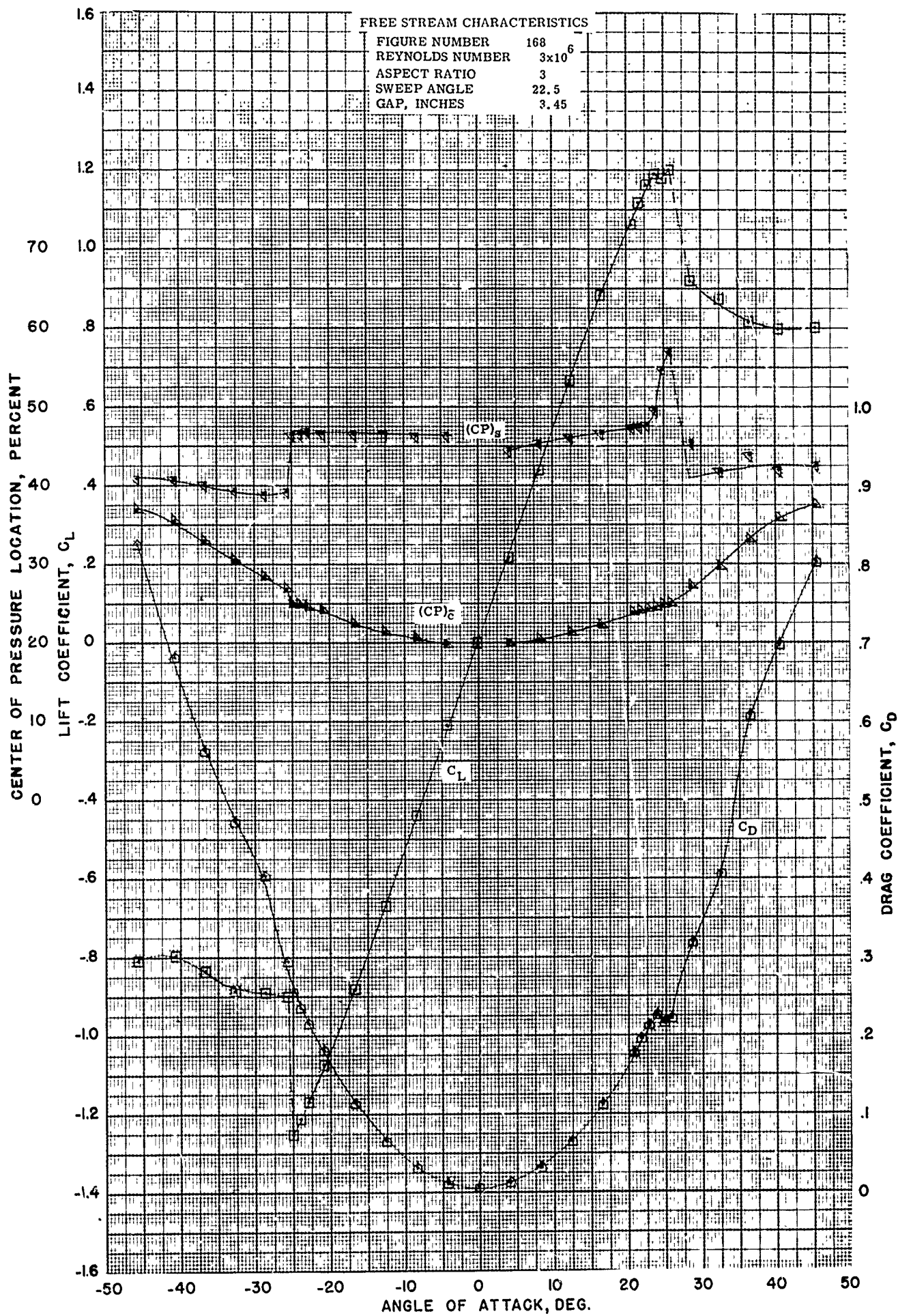


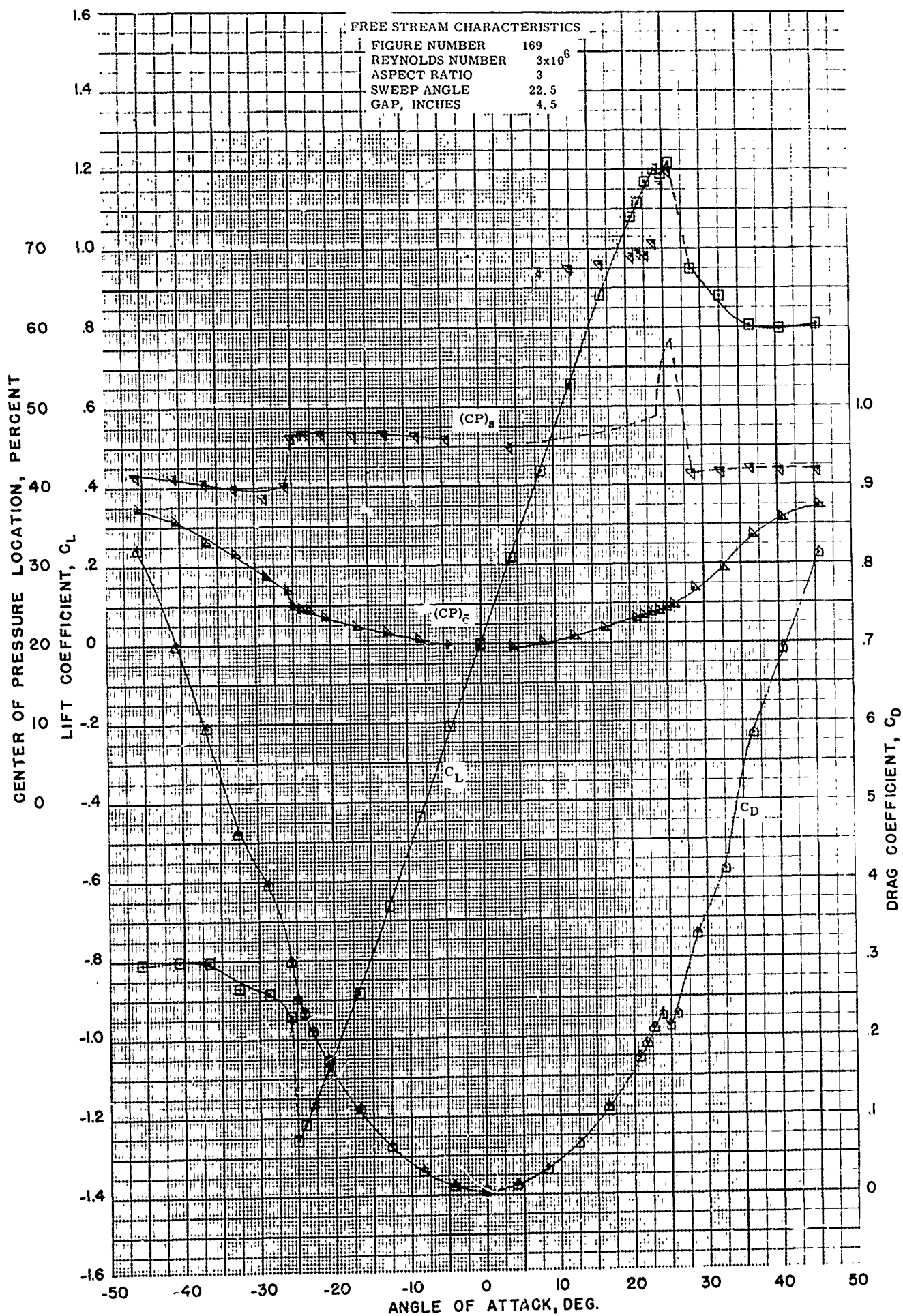


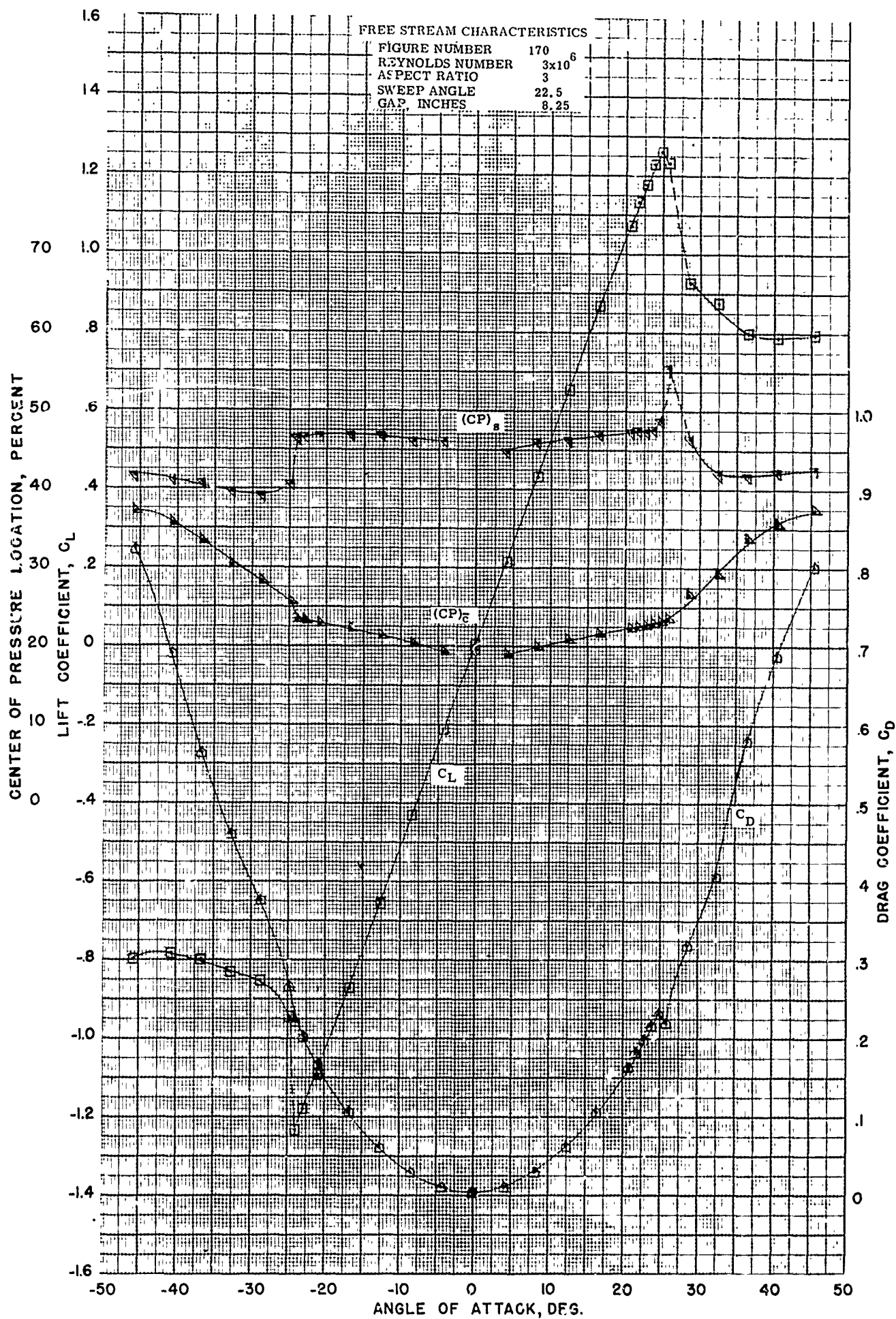


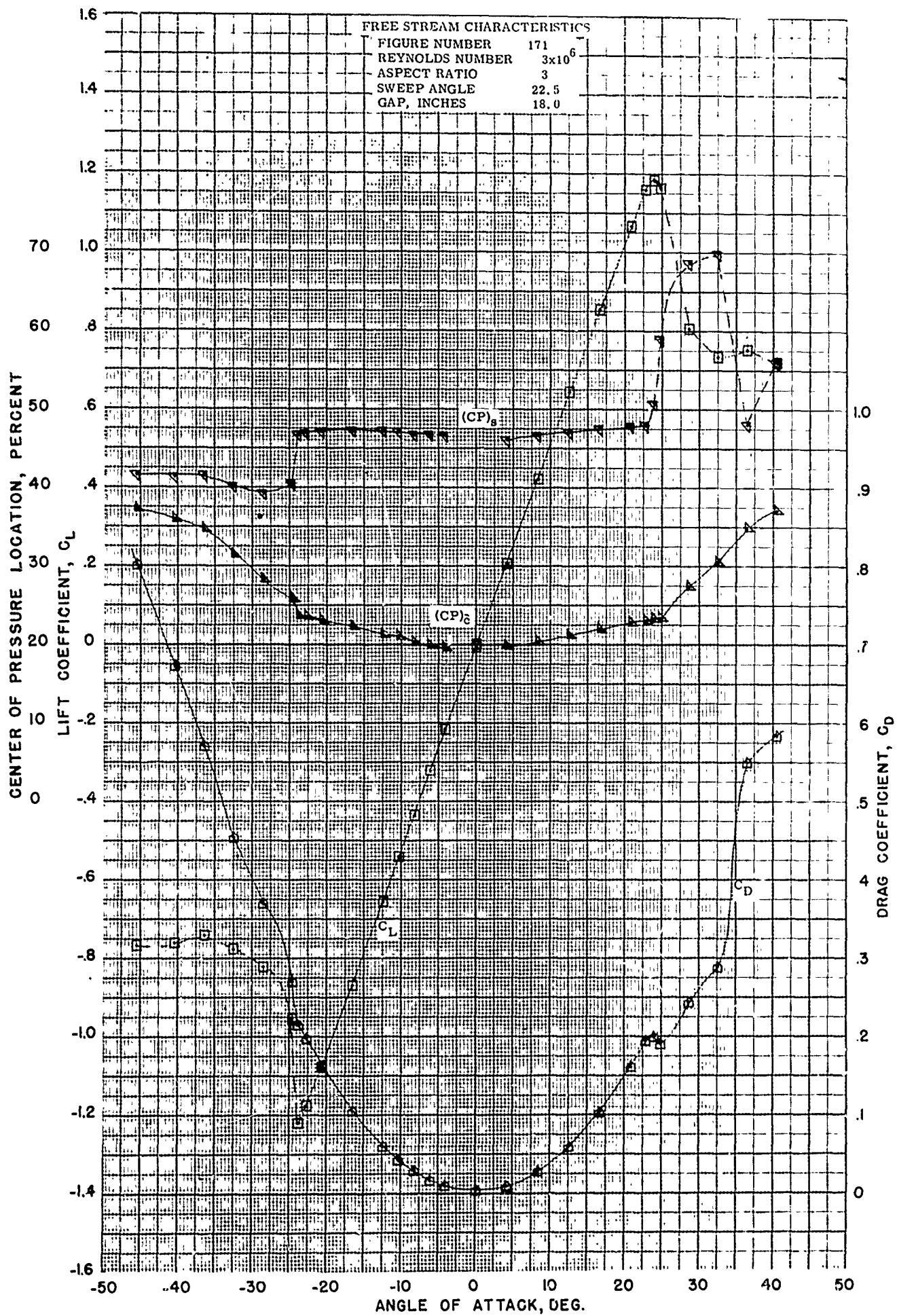






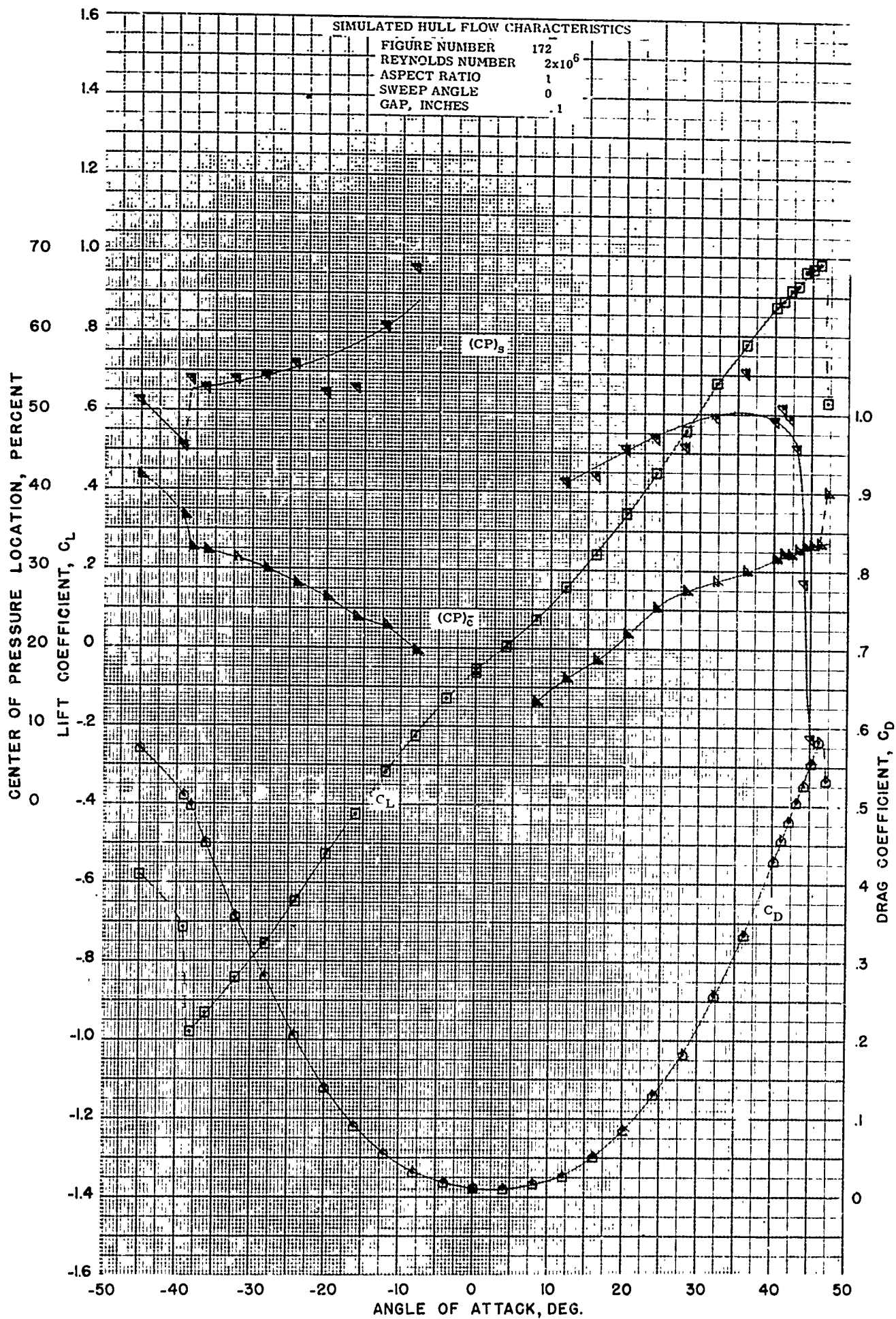


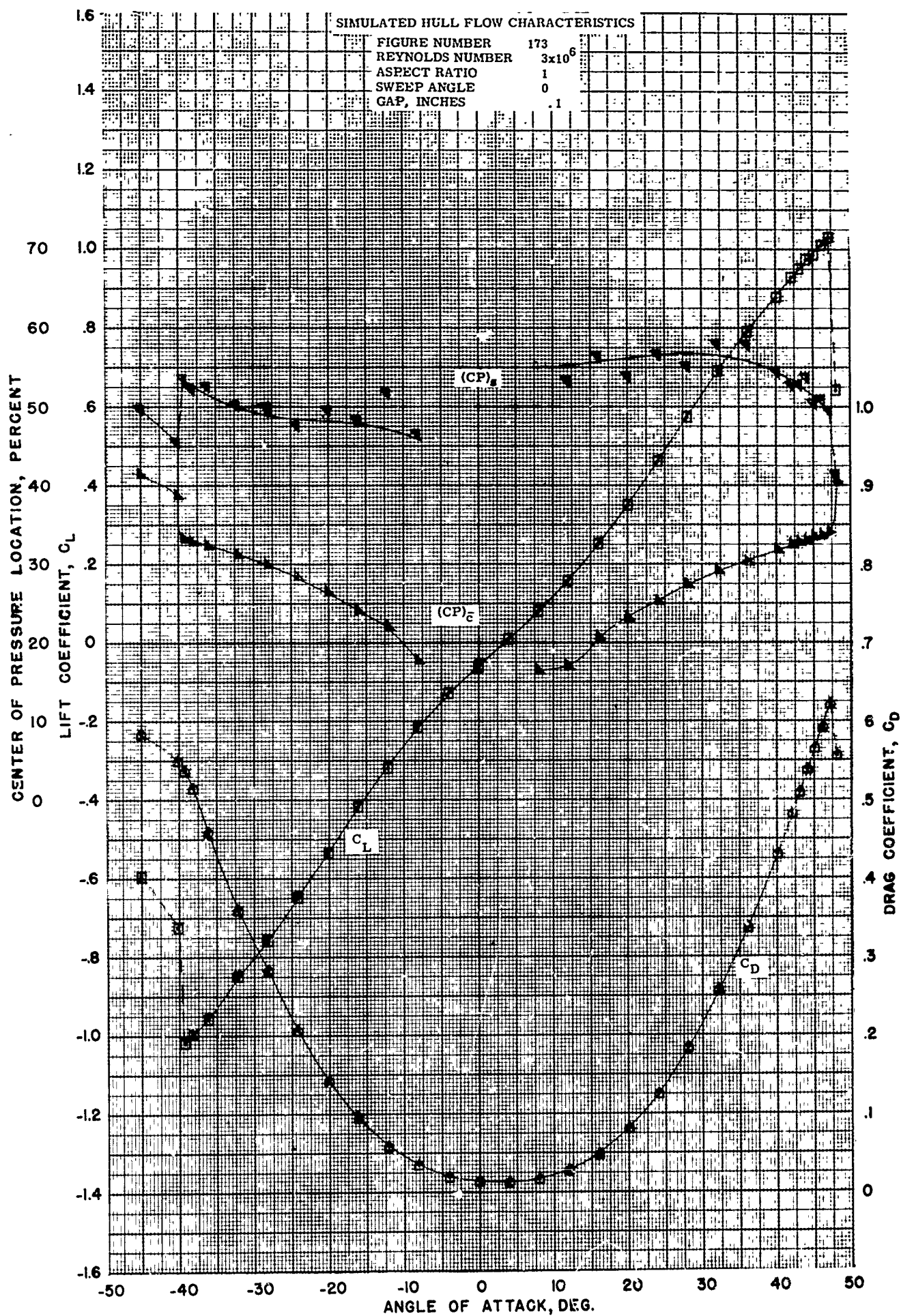


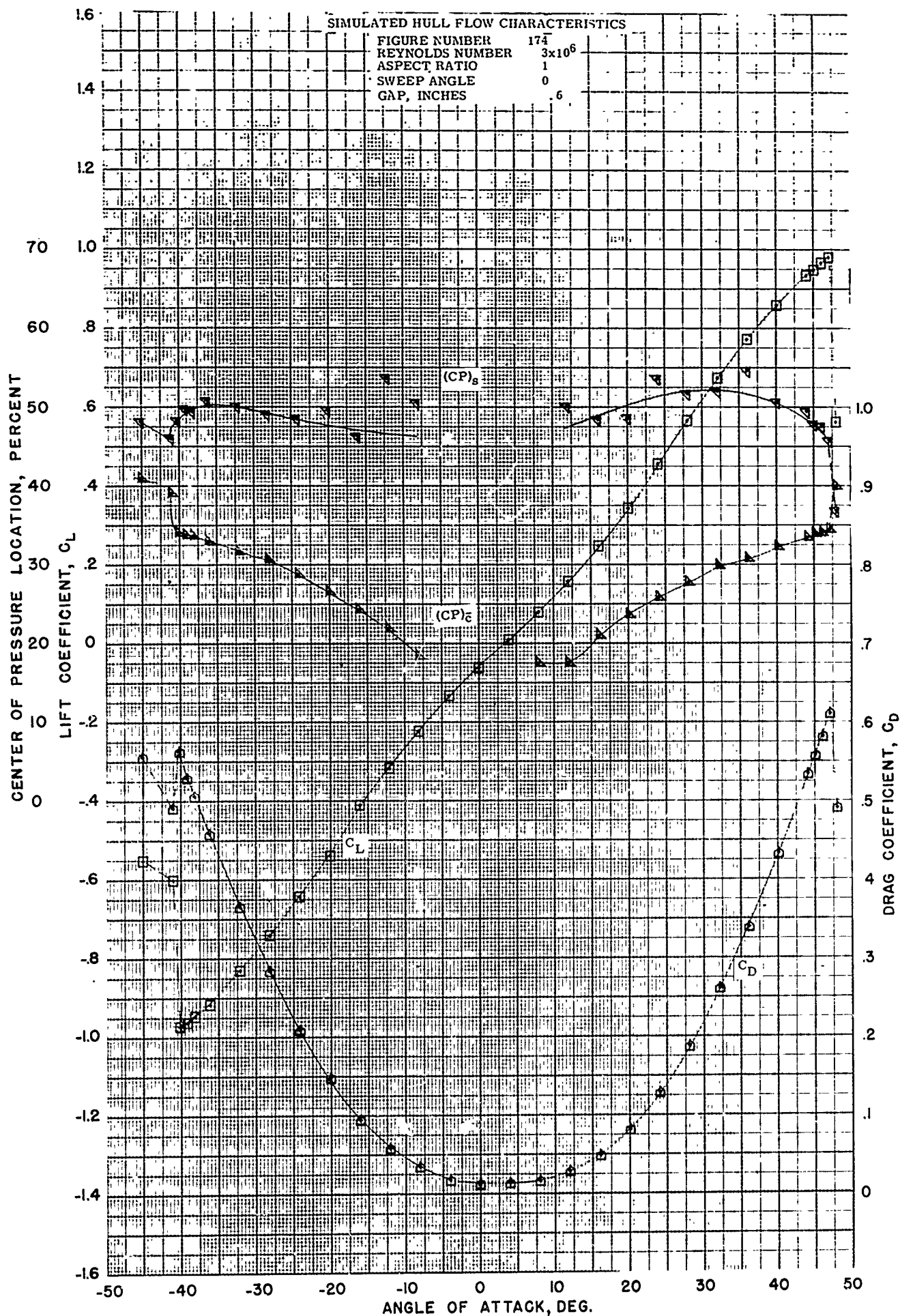


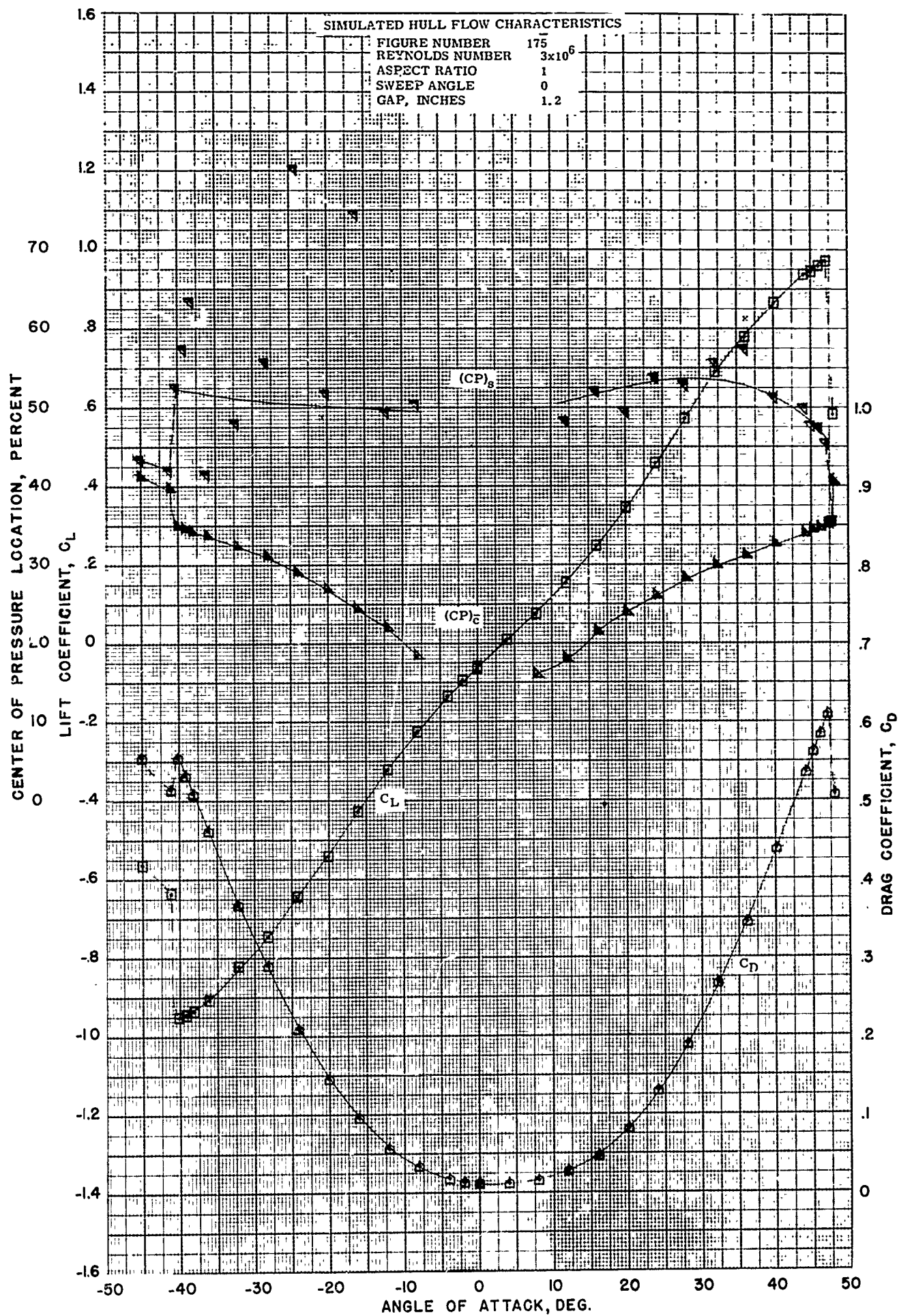
APPENDIX B

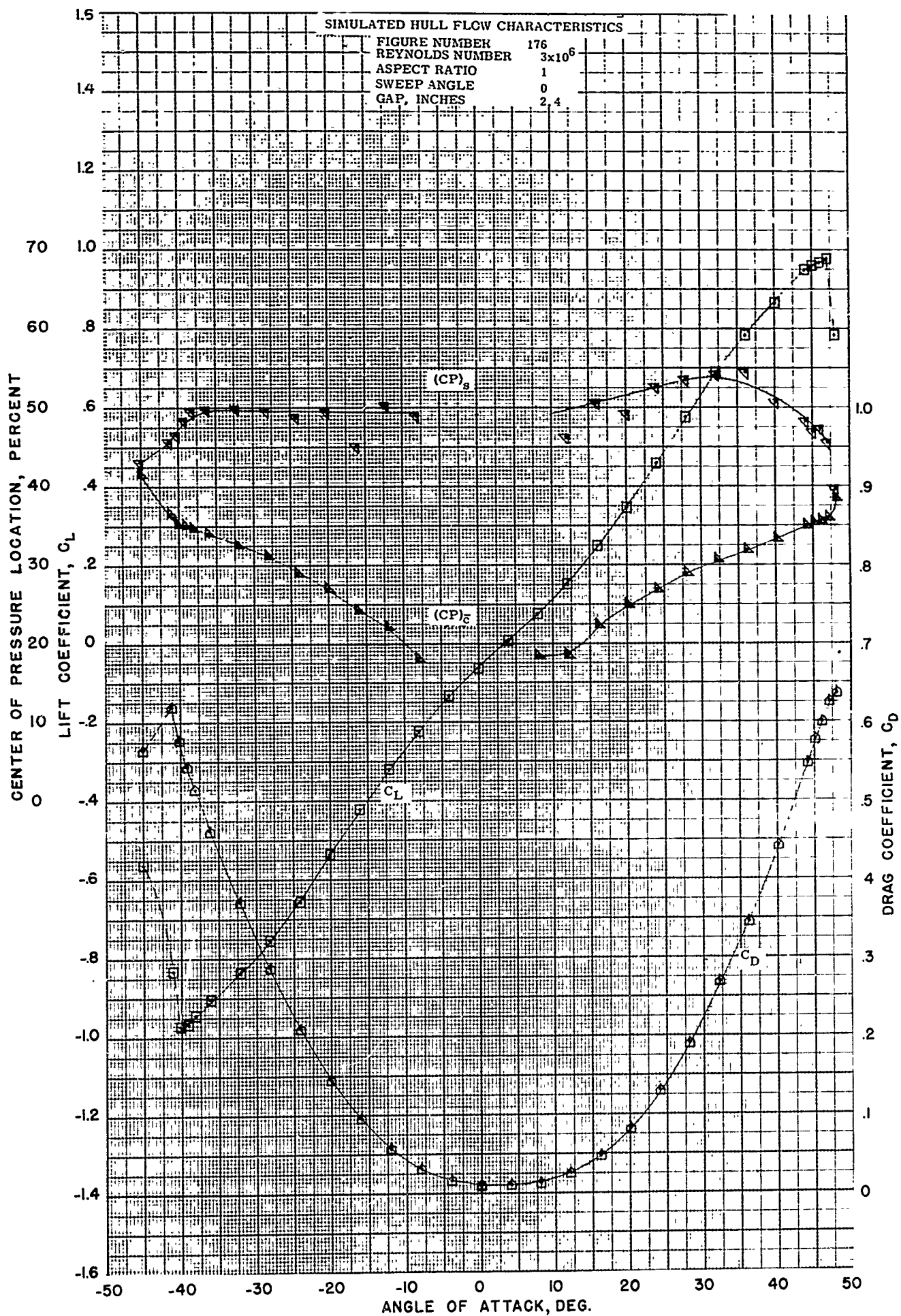
Simulated Hull Flow Characteristics
For Various Gap Sizes

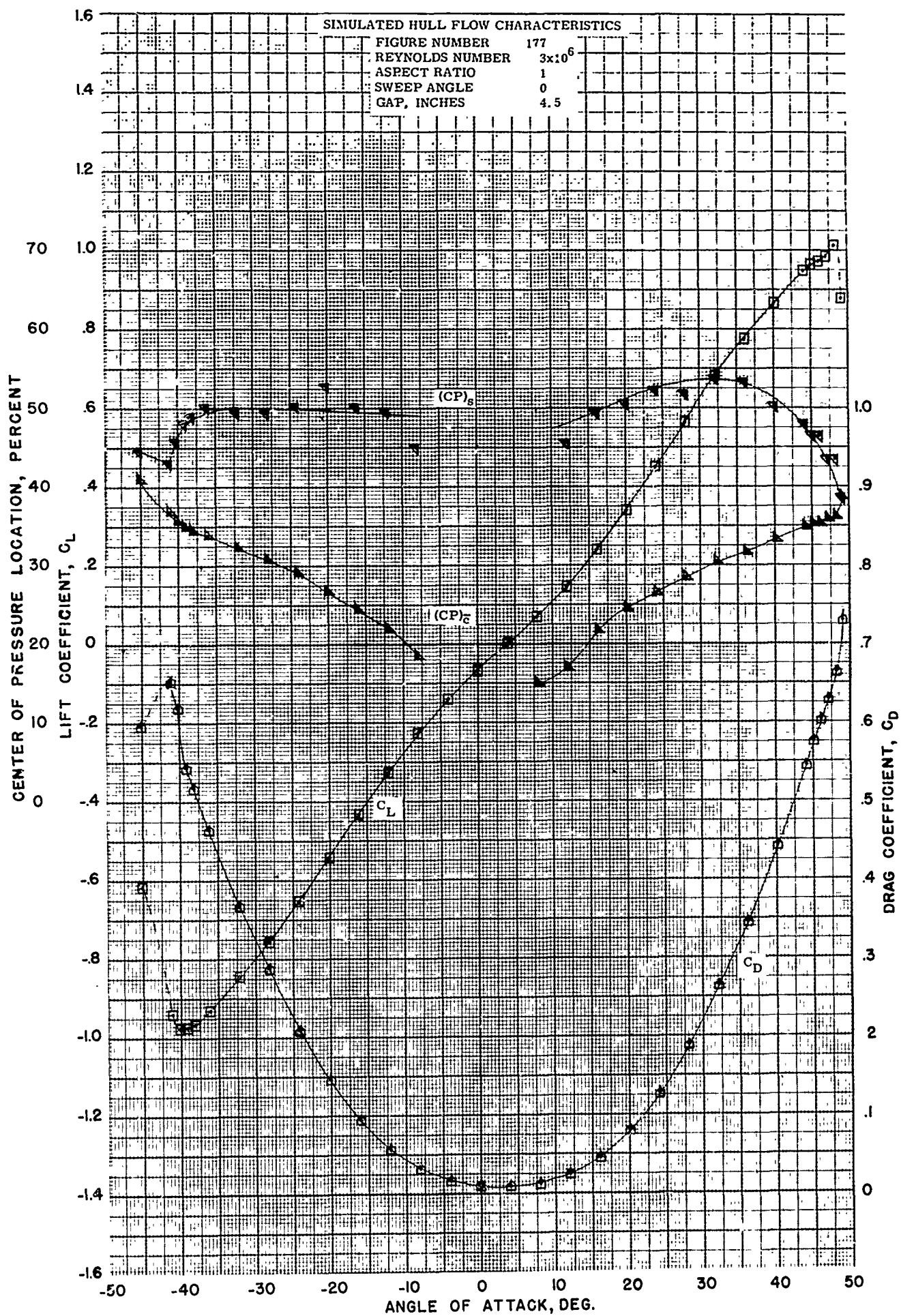


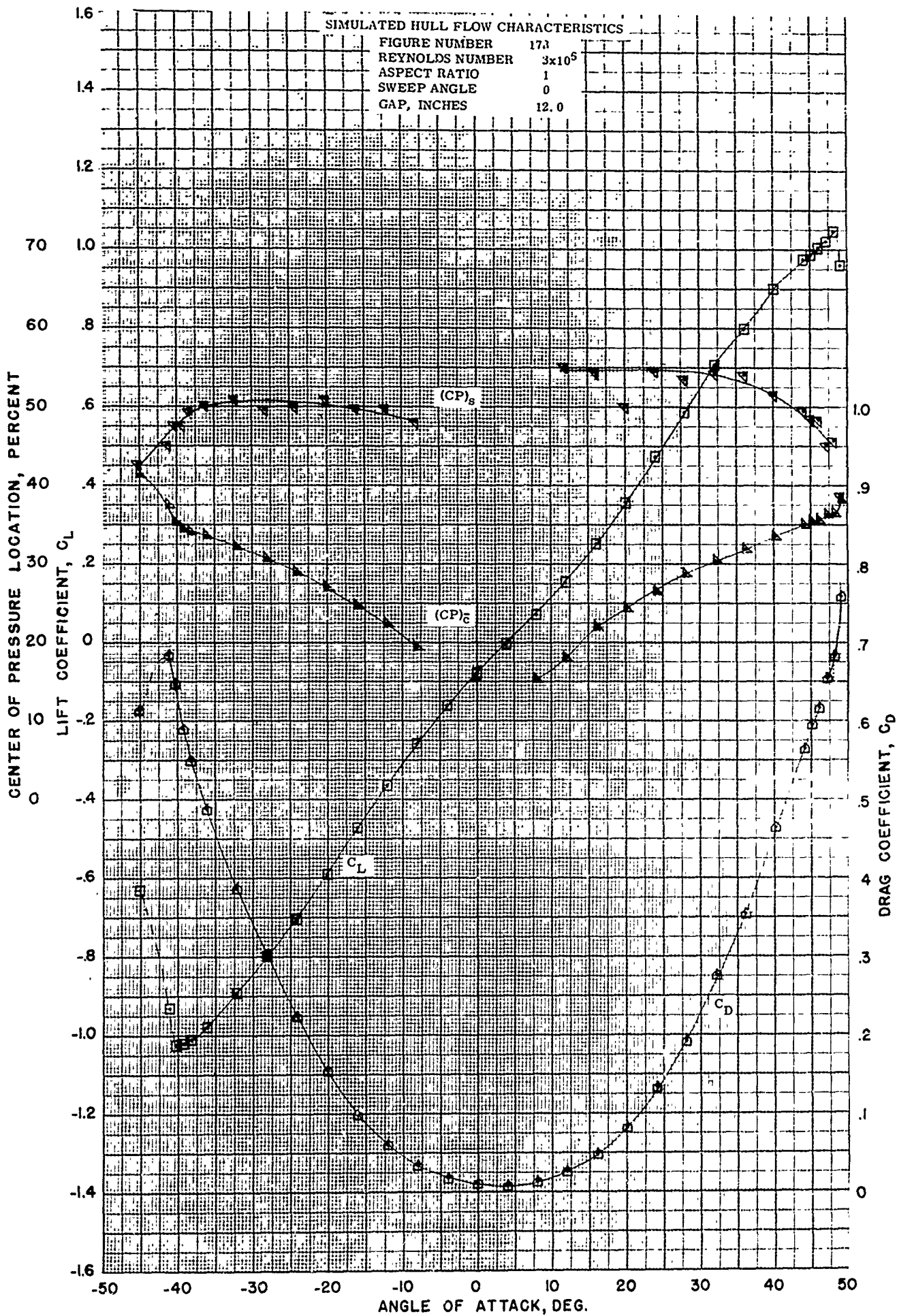


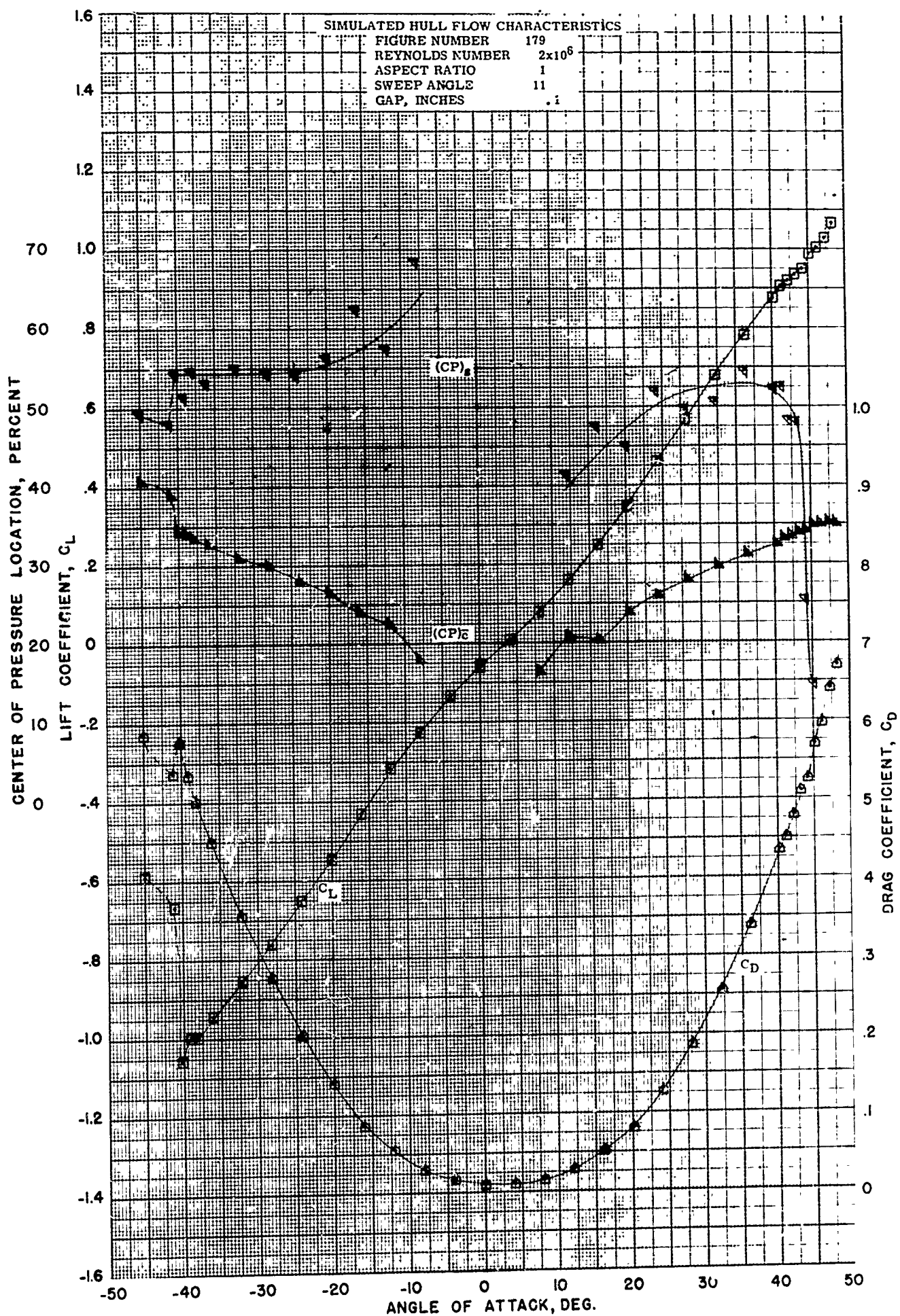


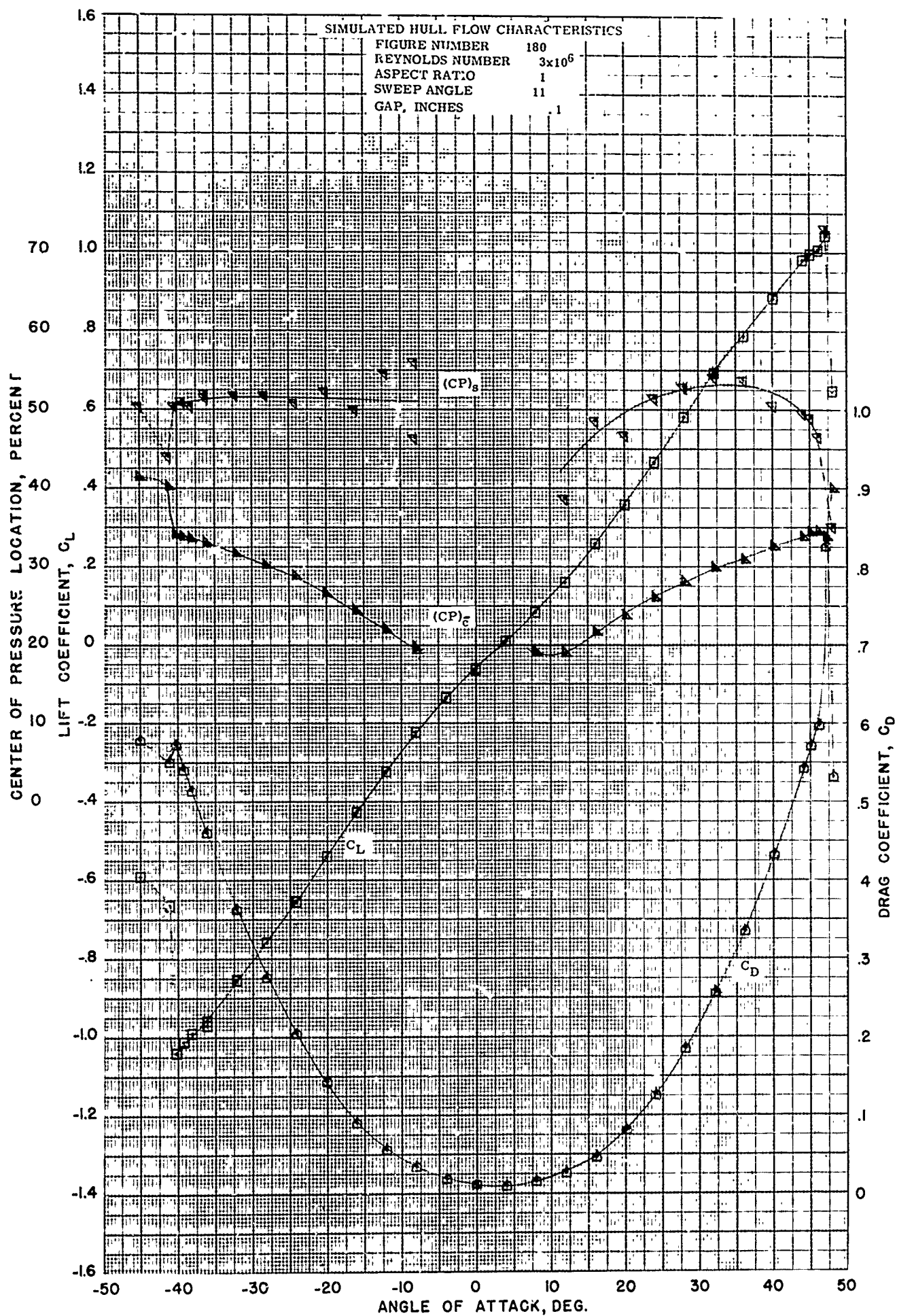


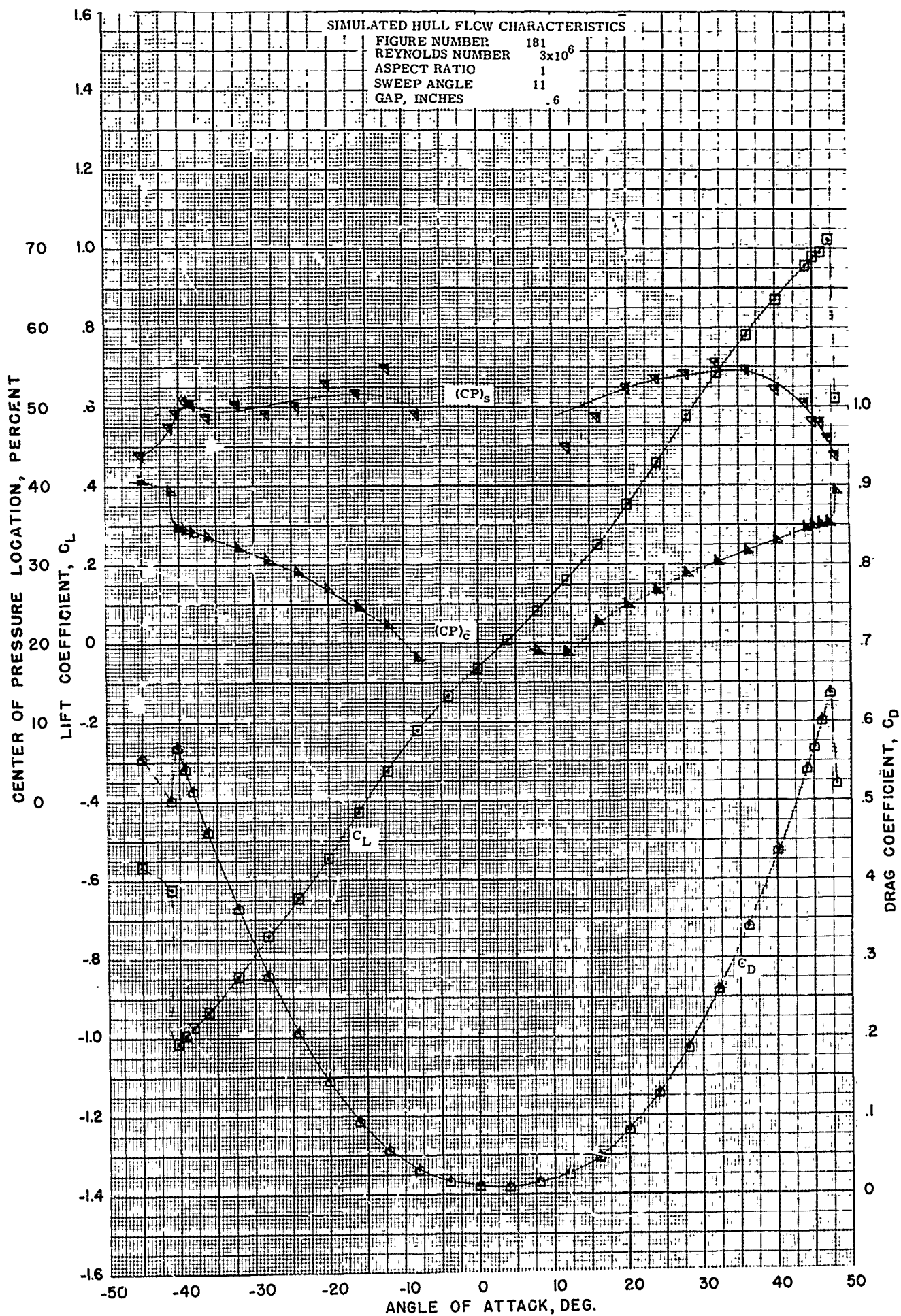


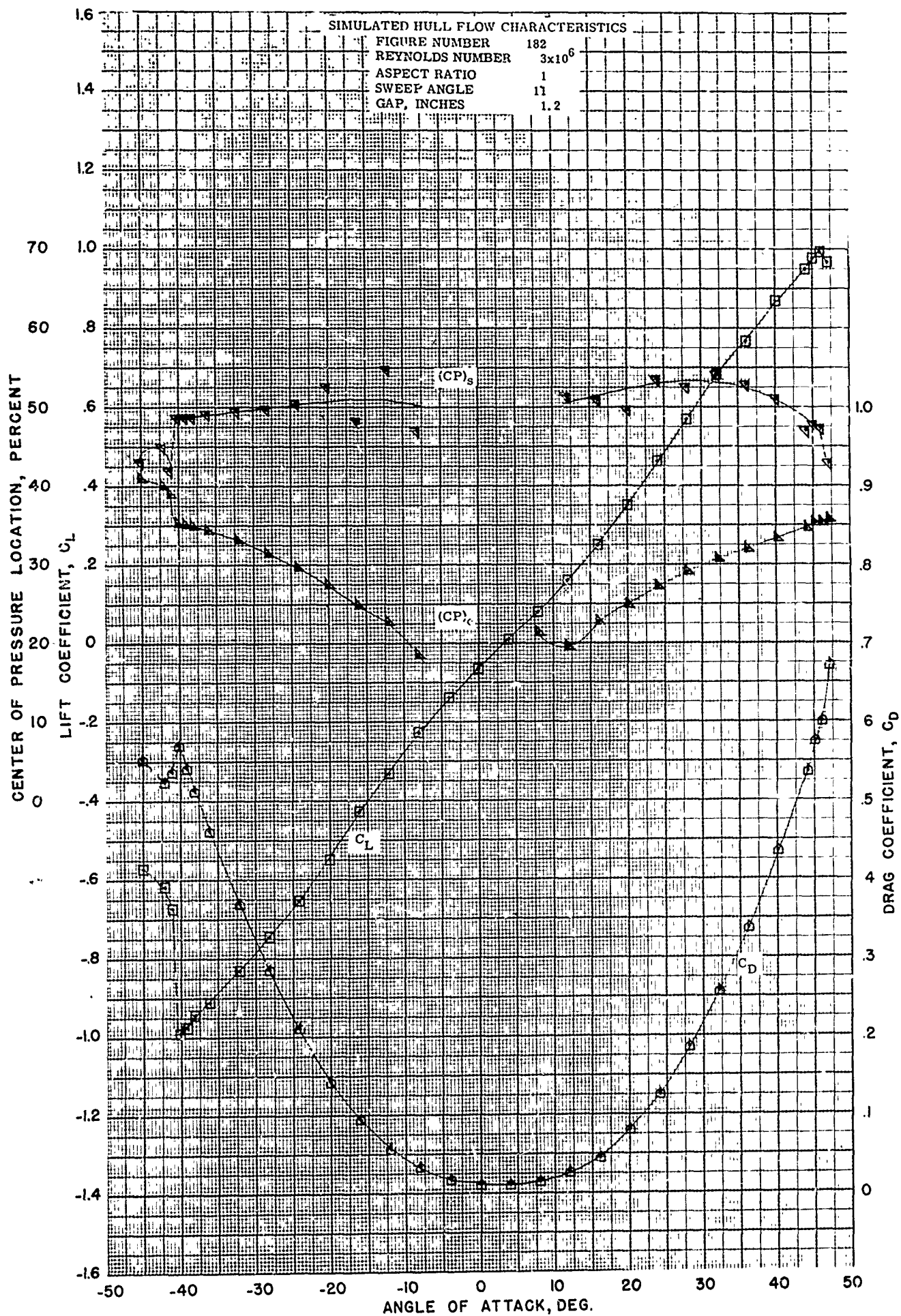


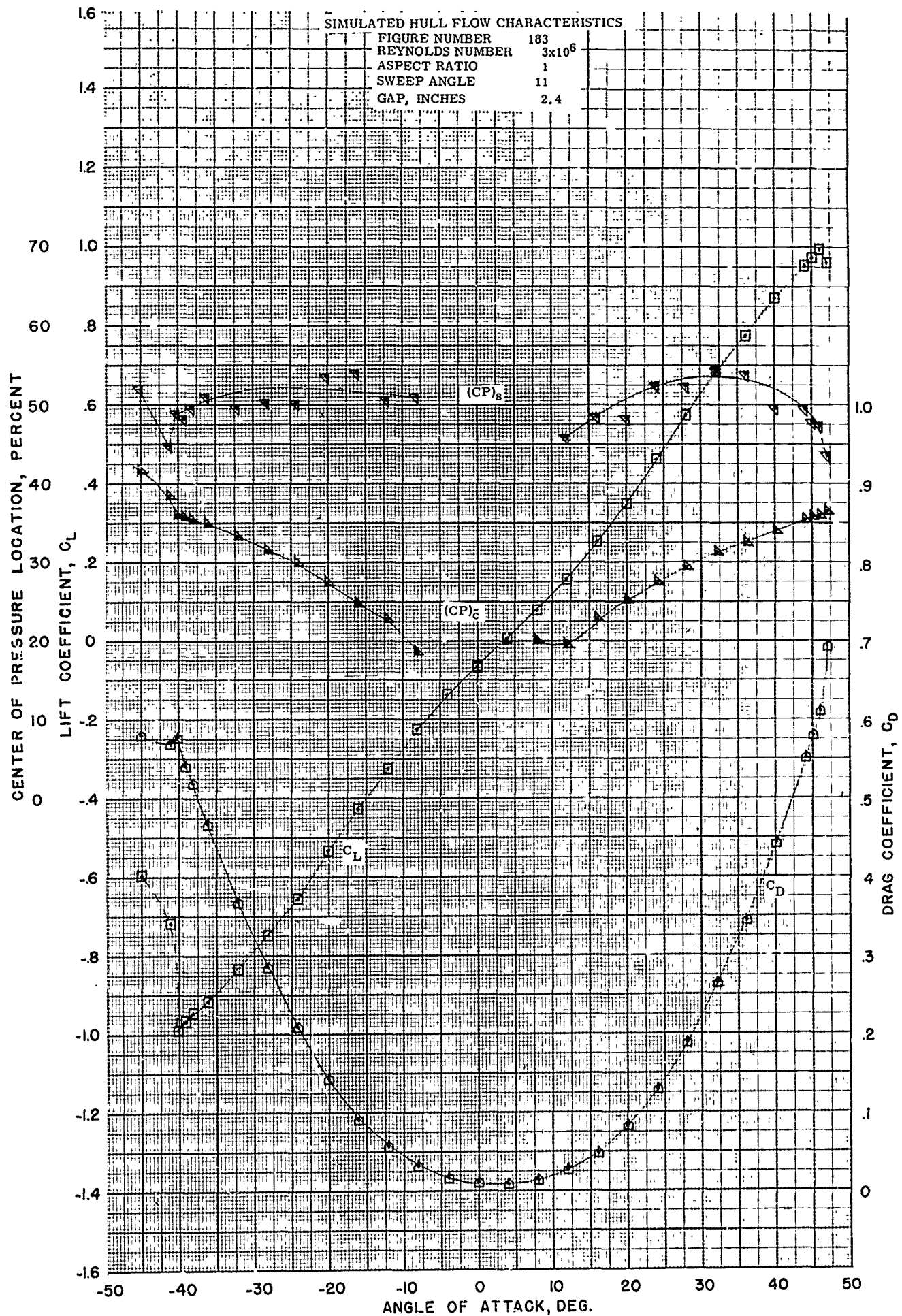


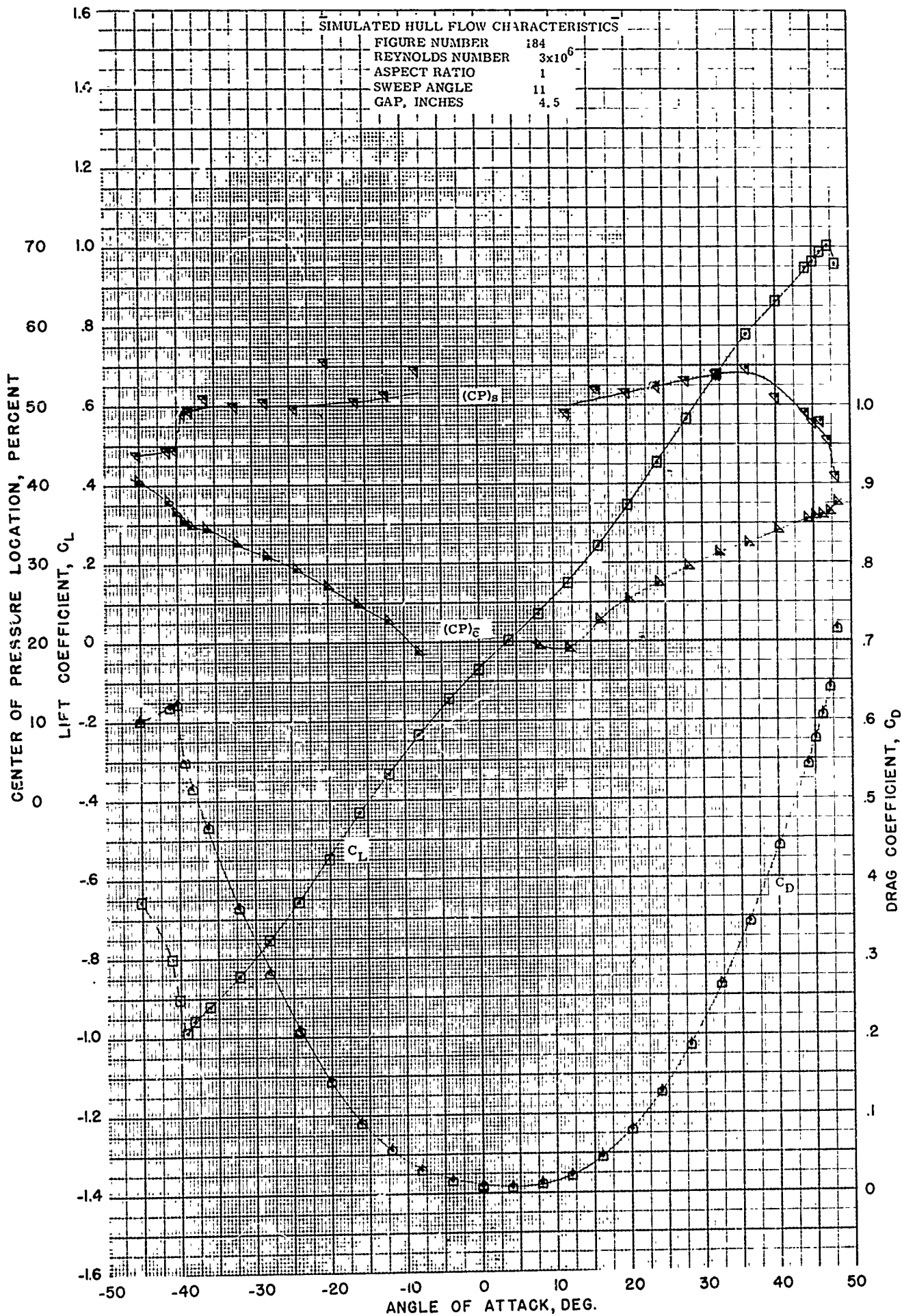


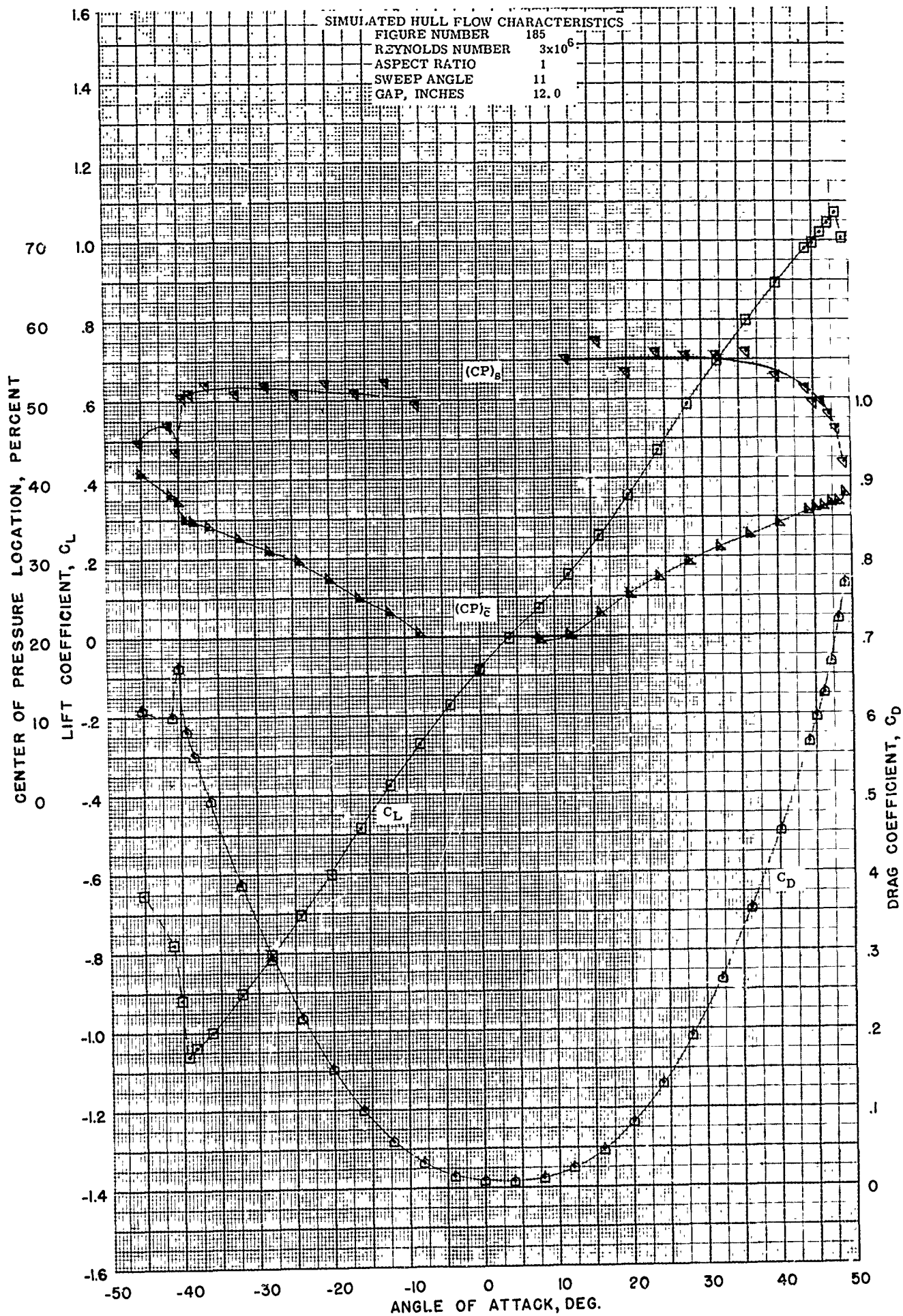


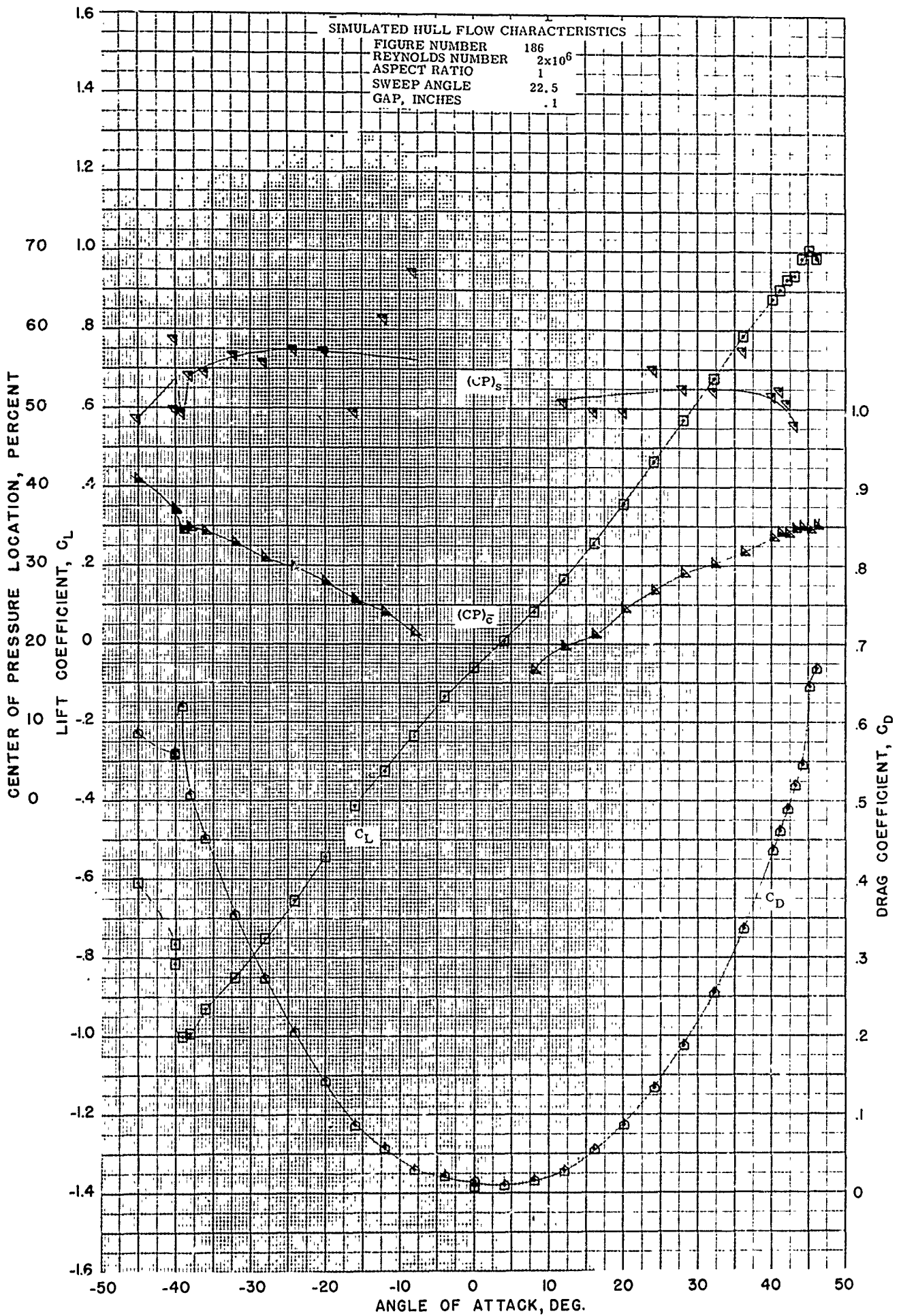


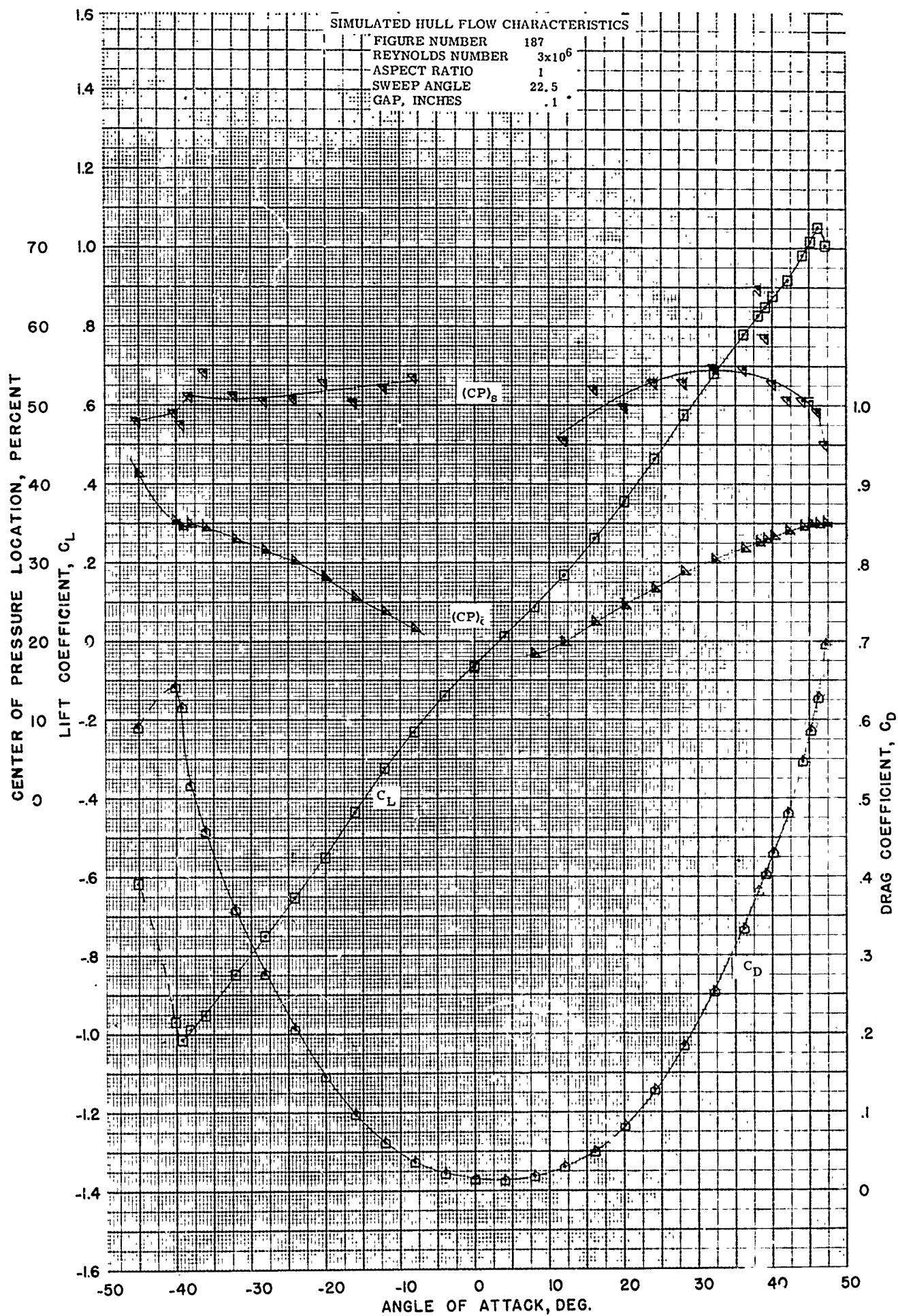


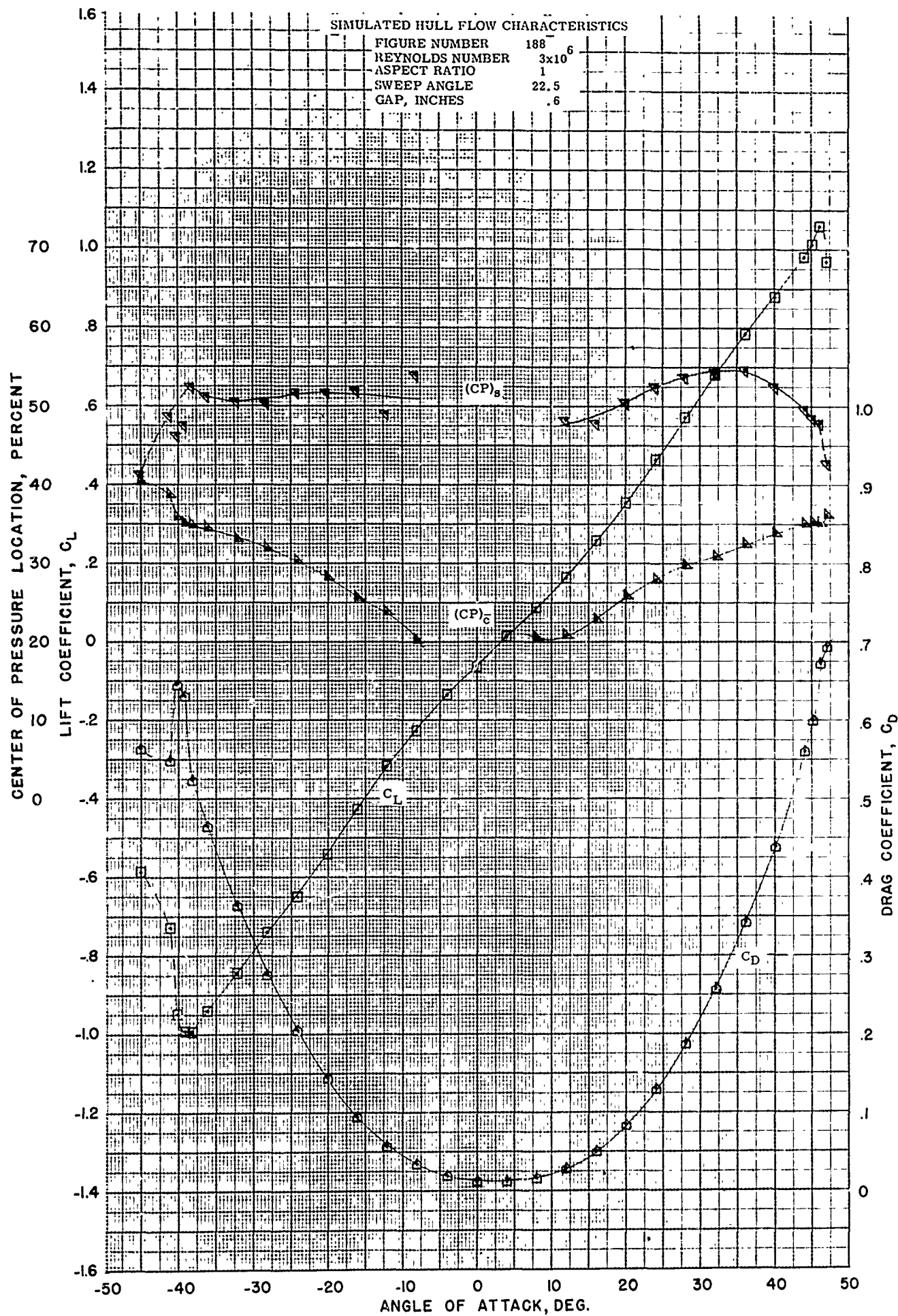


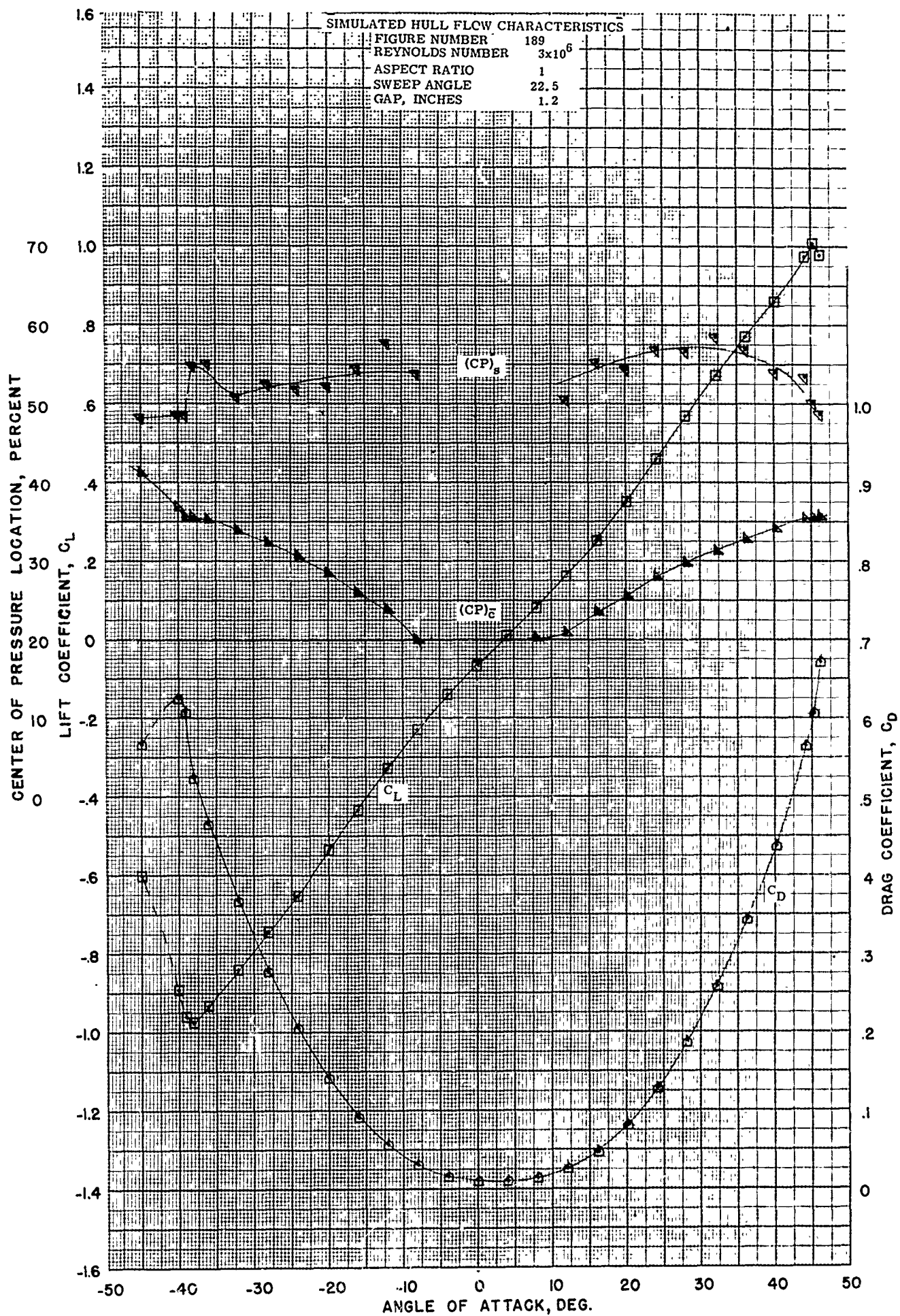


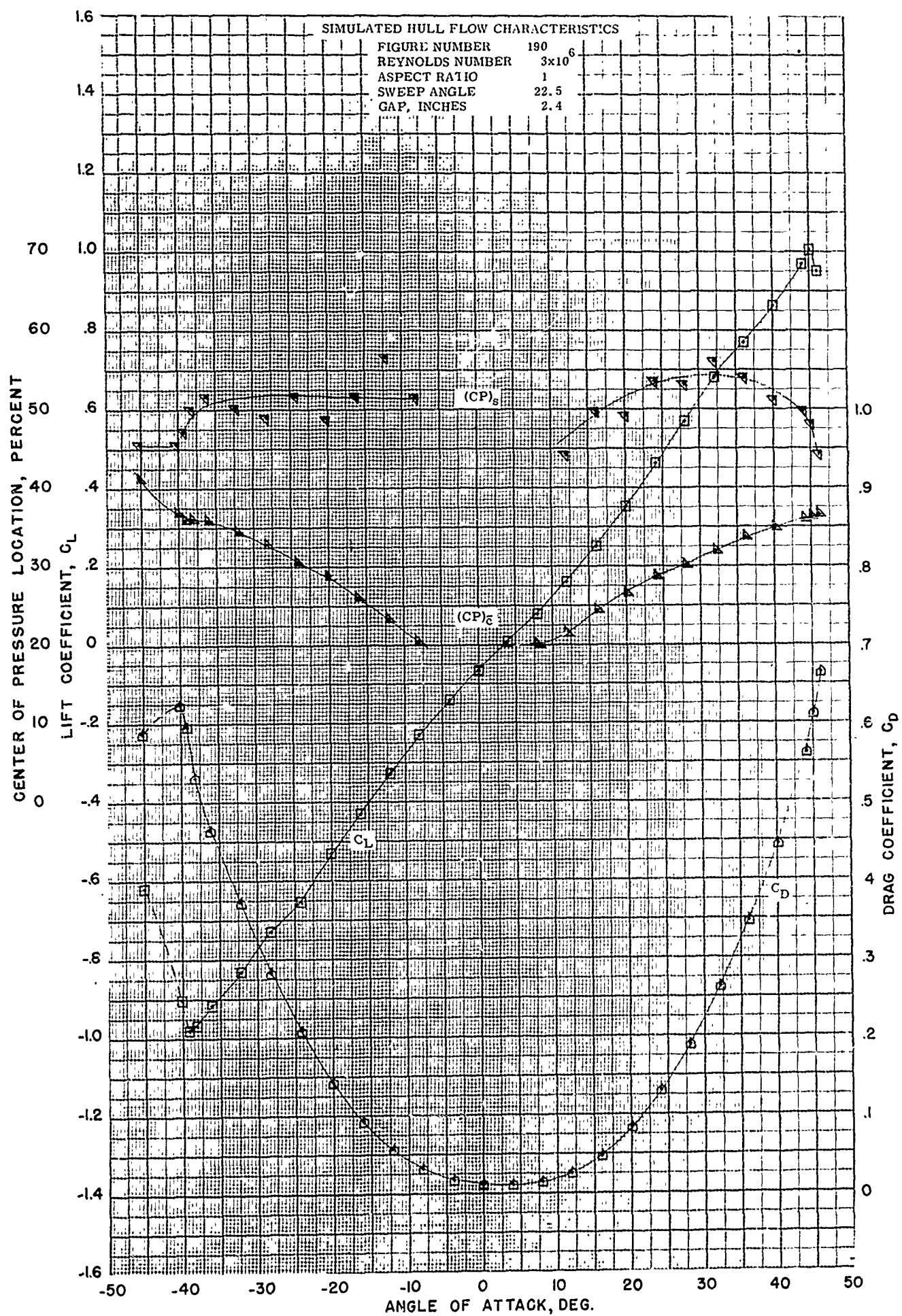


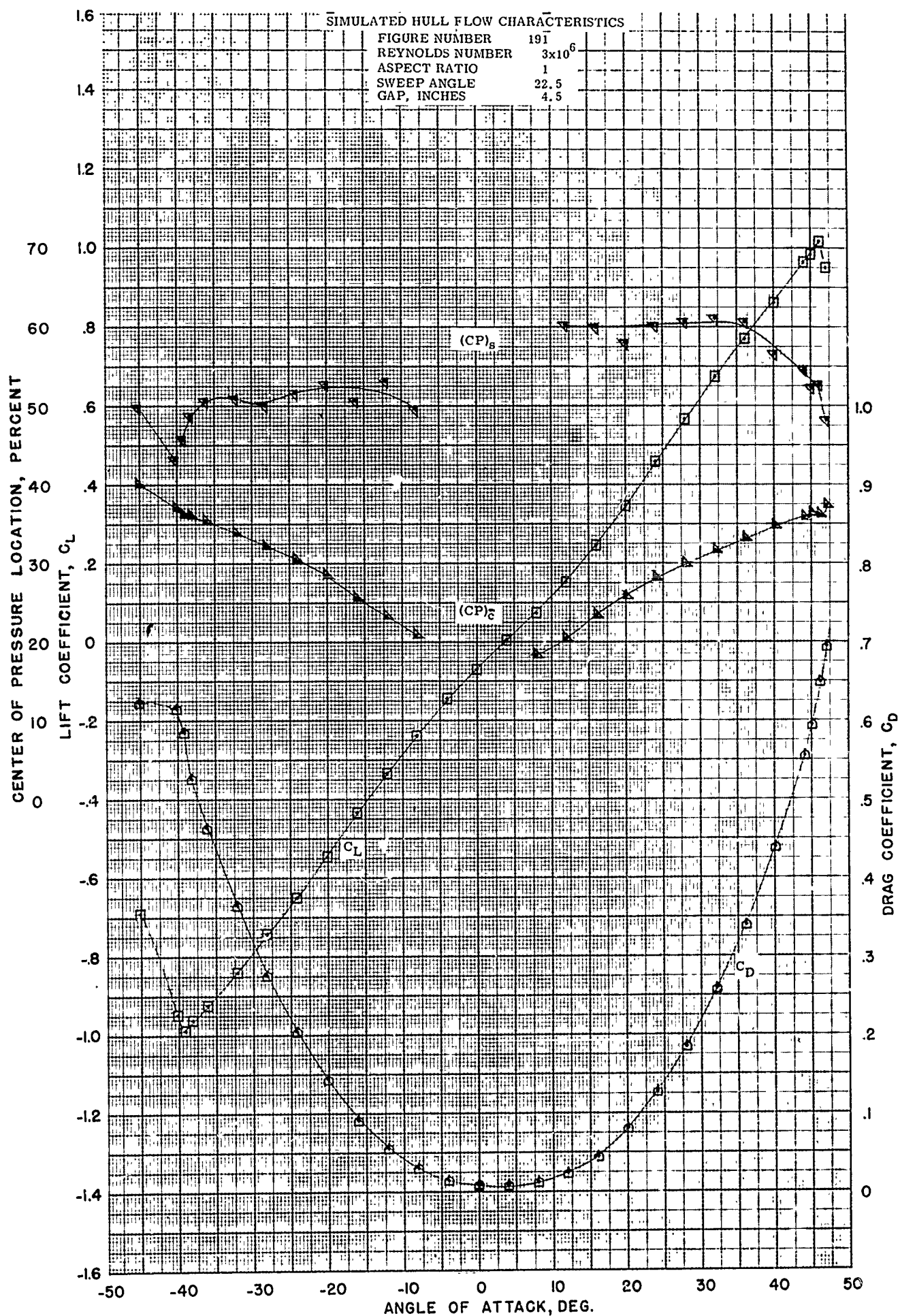


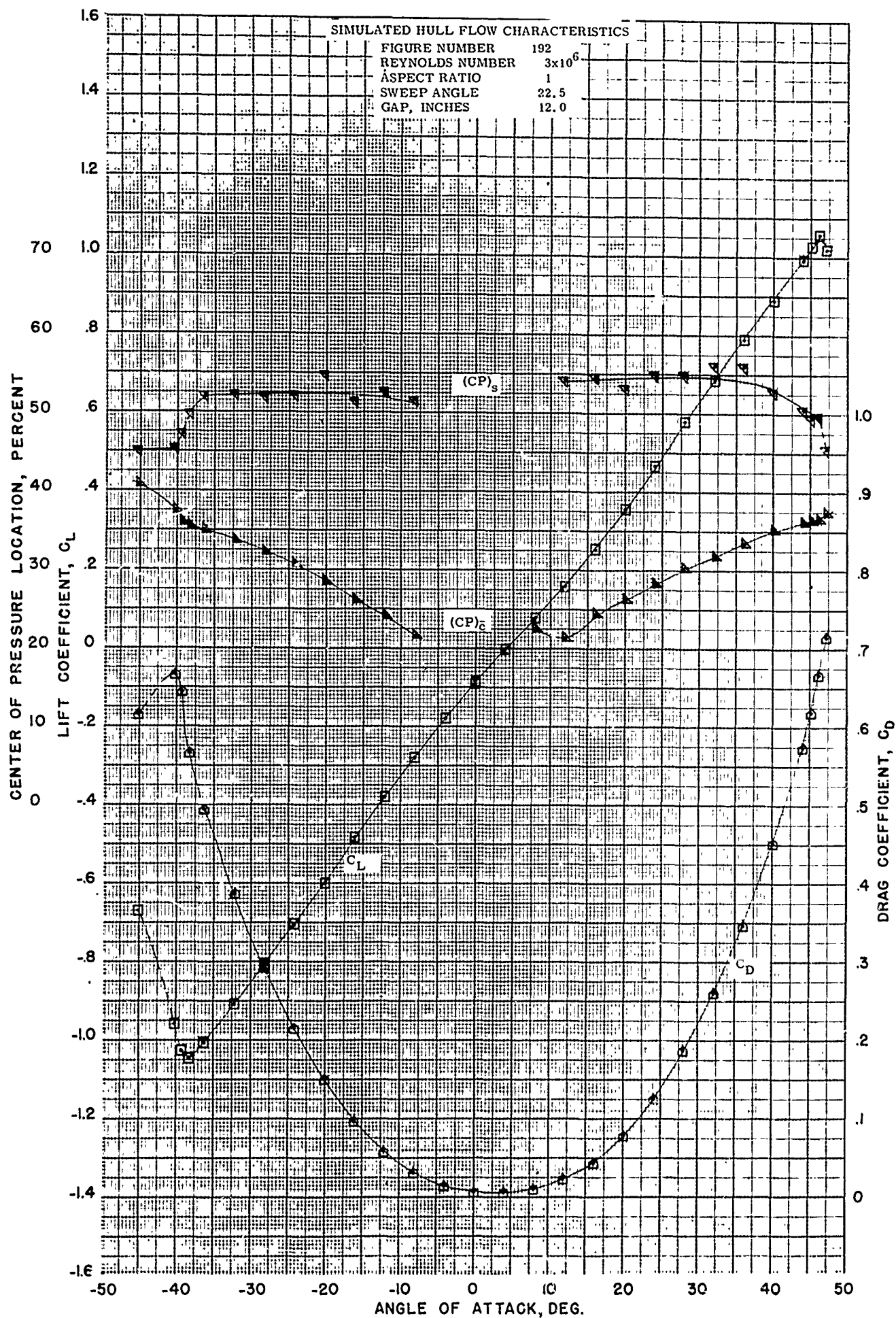


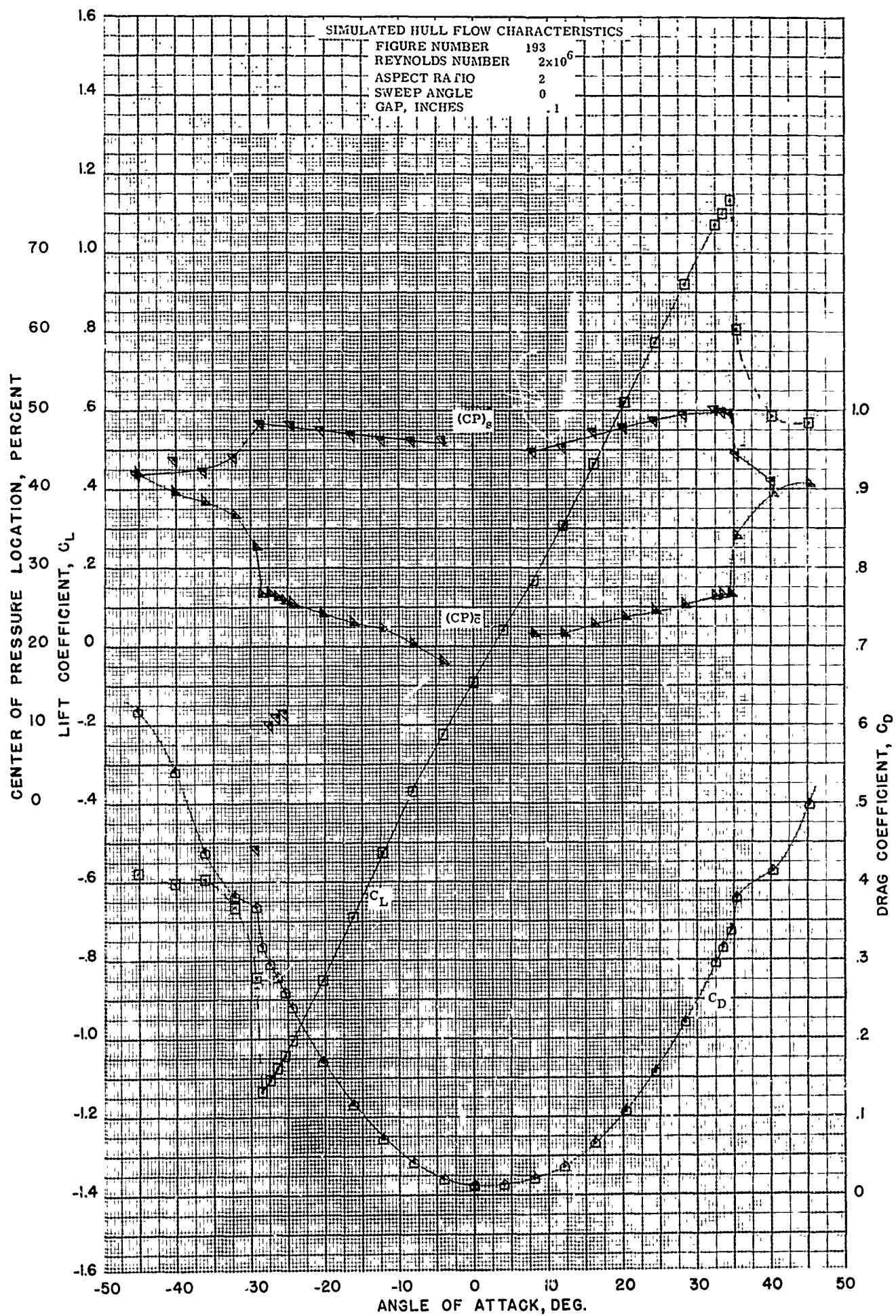


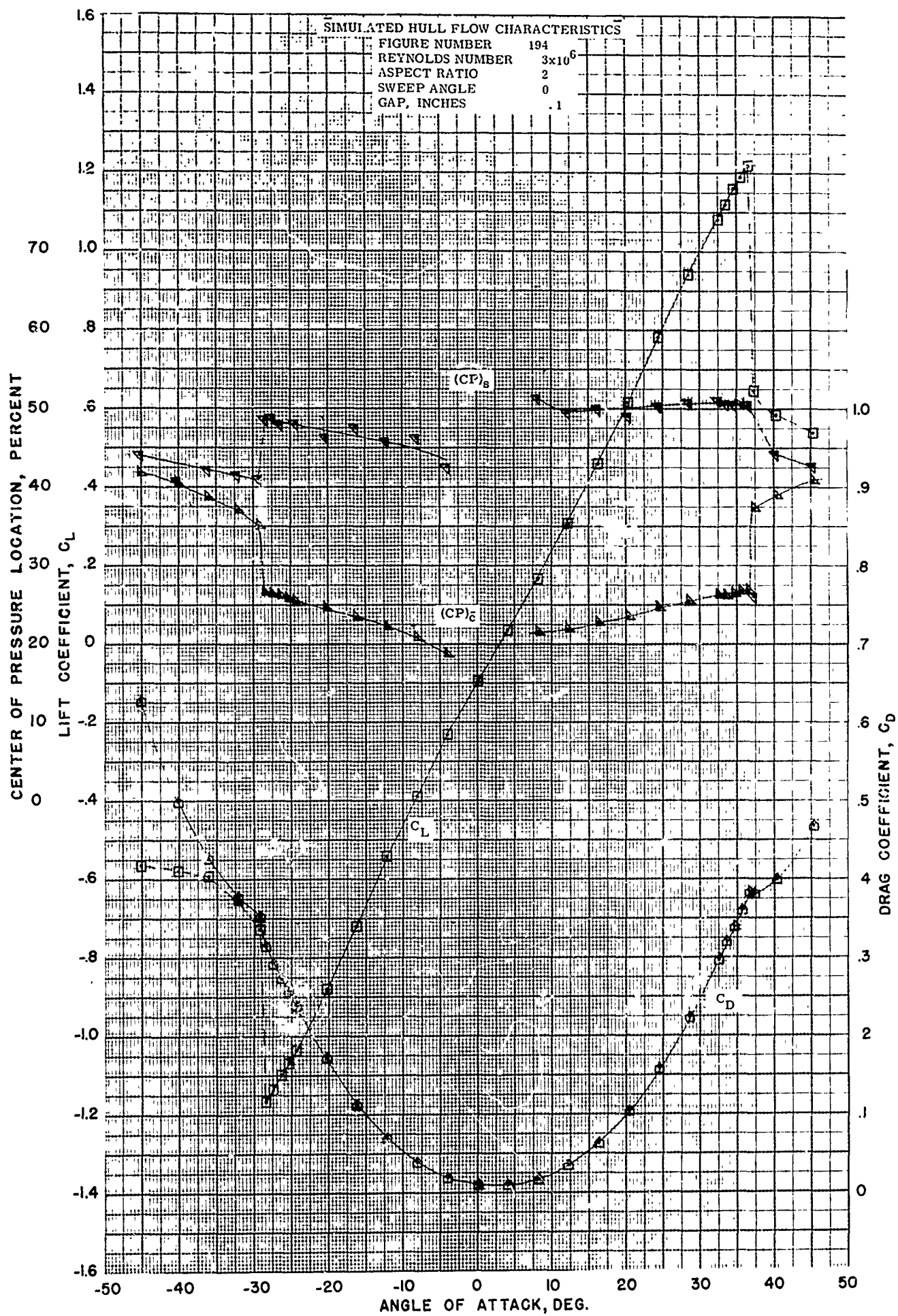


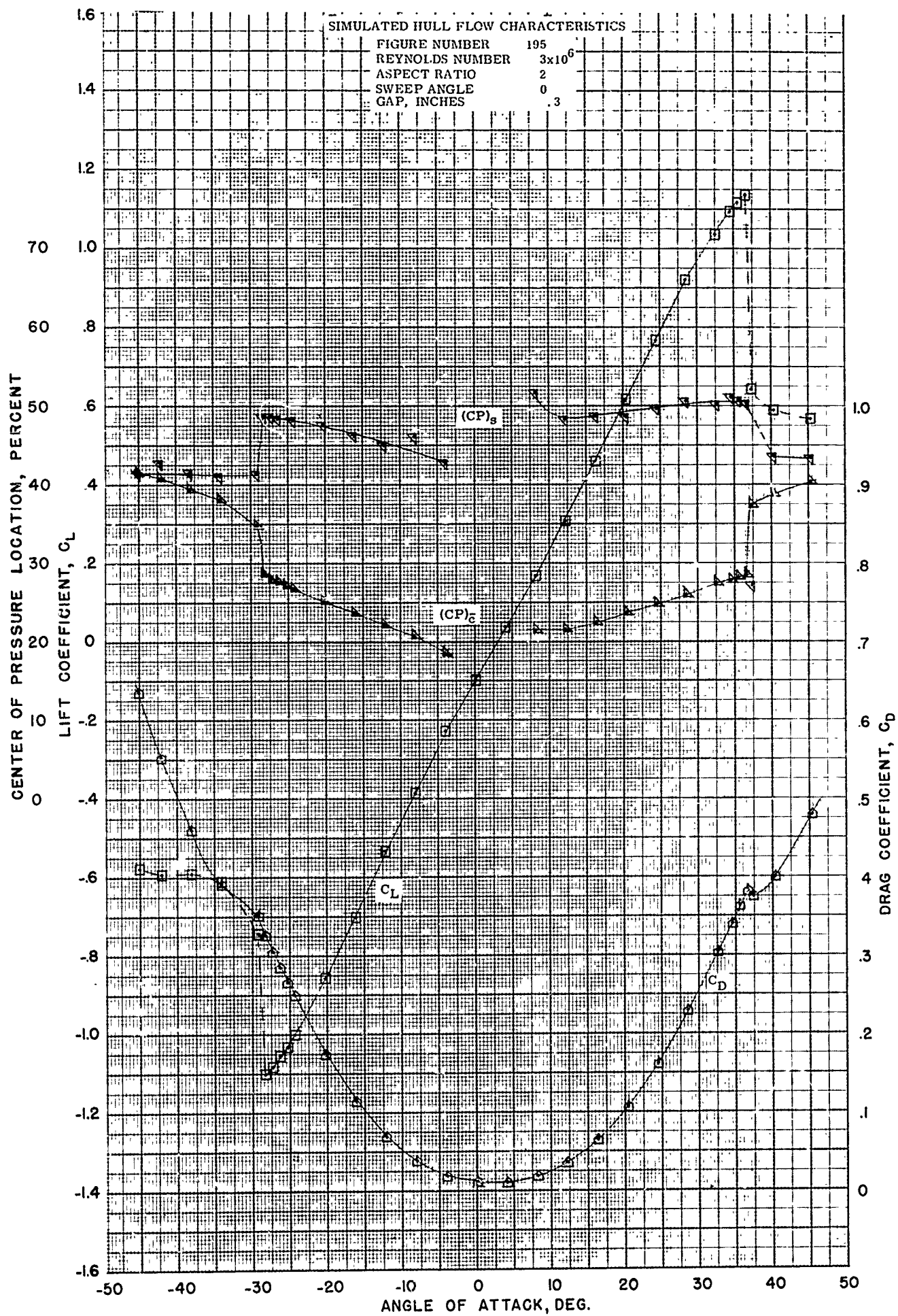


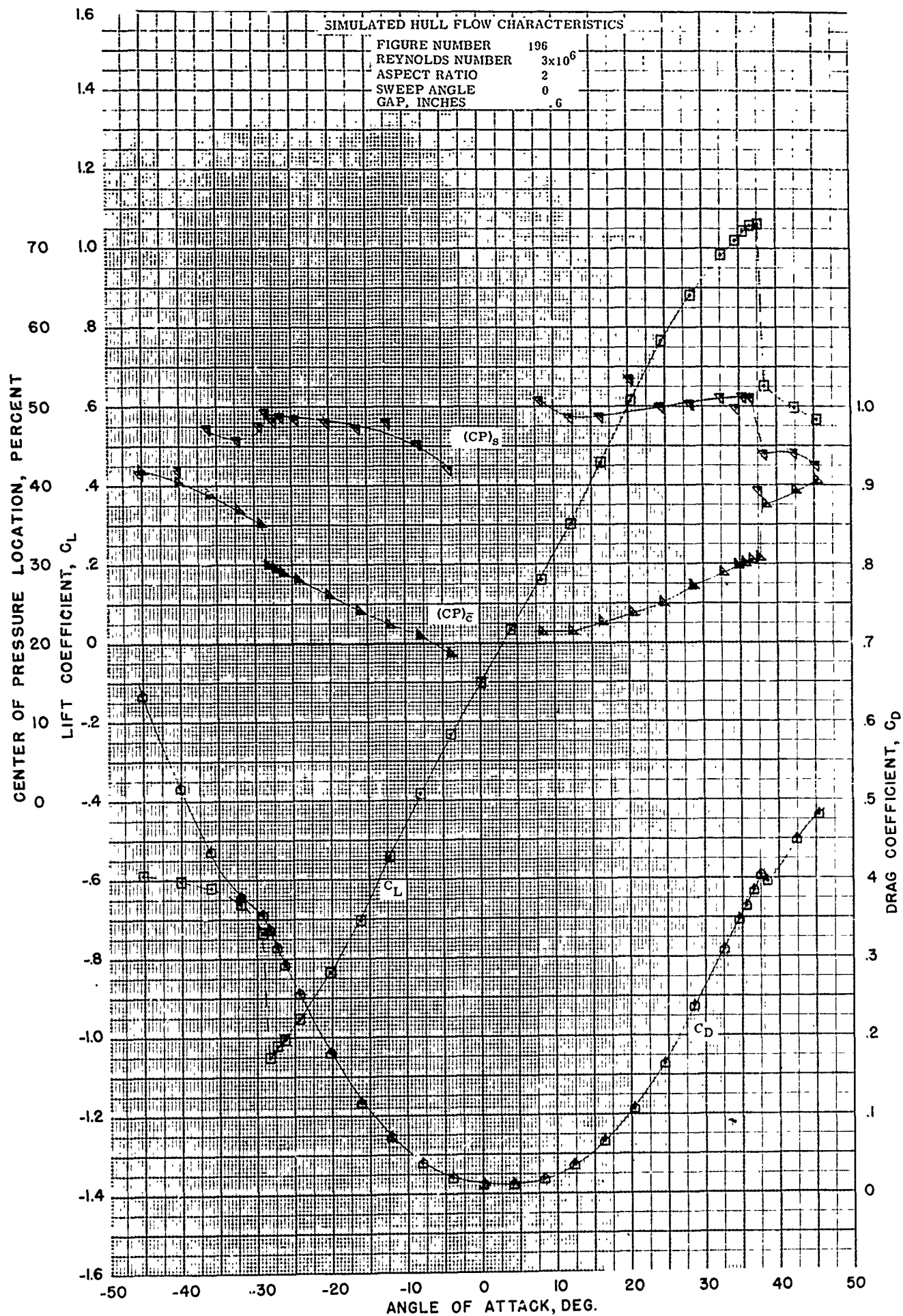


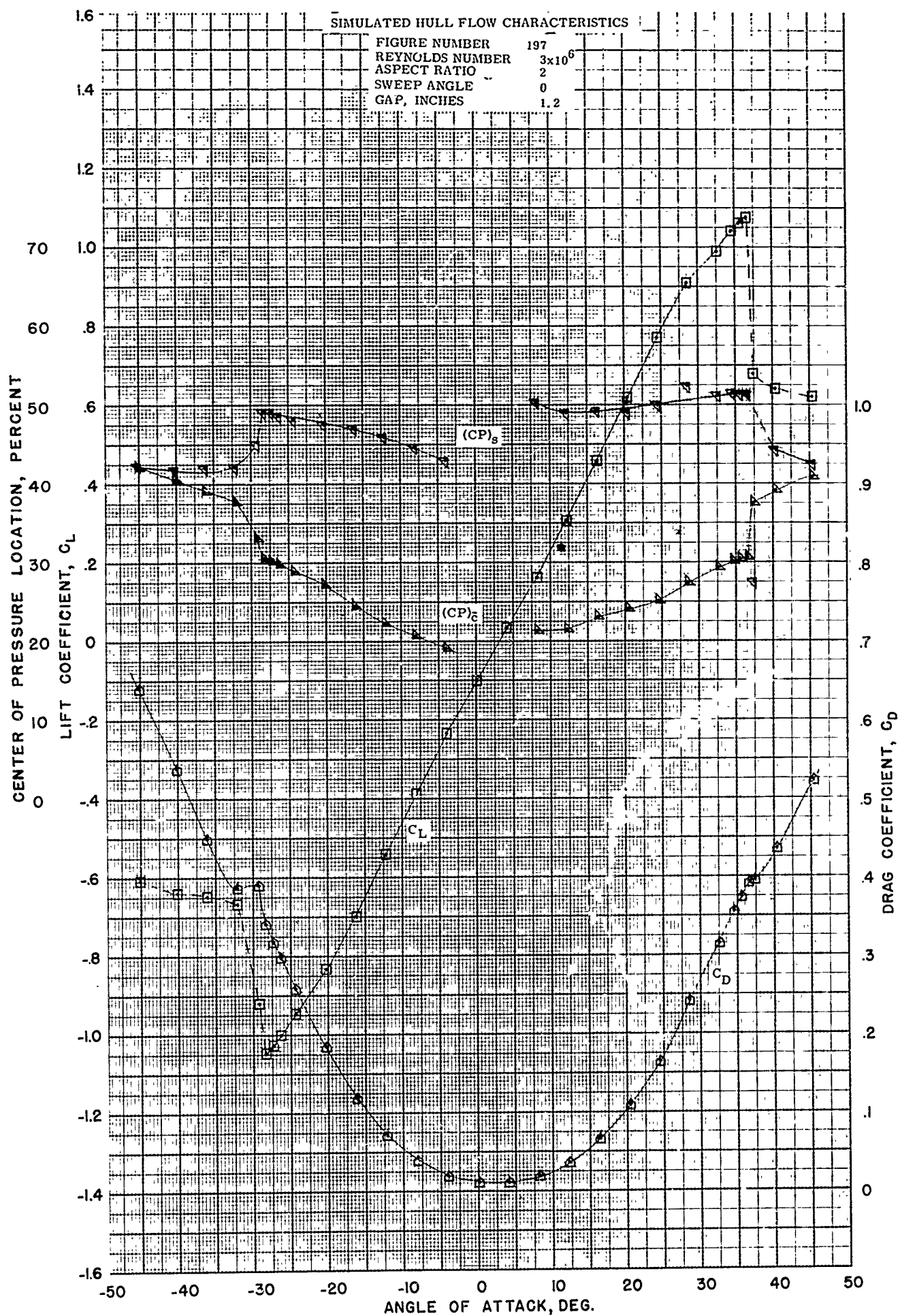


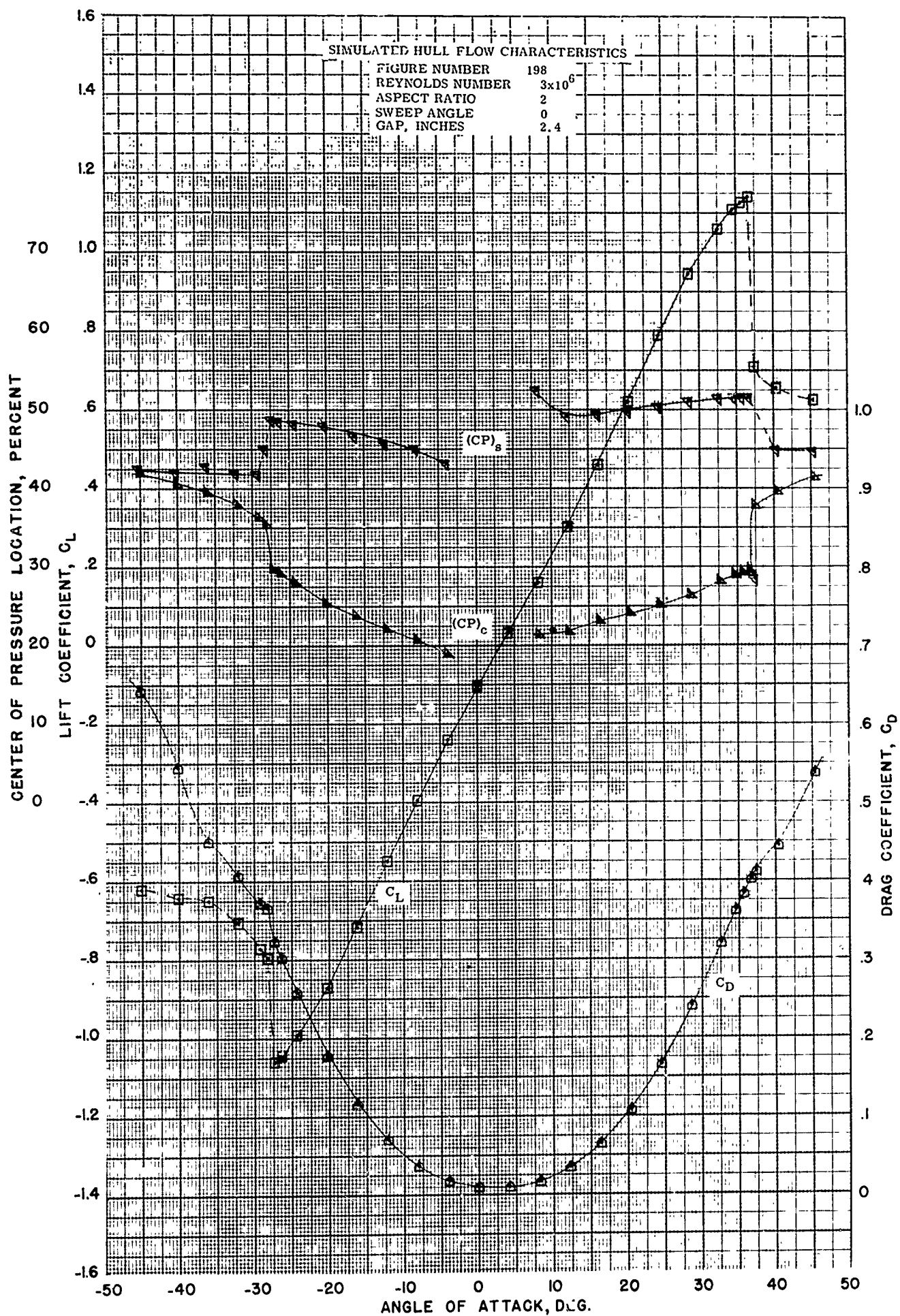


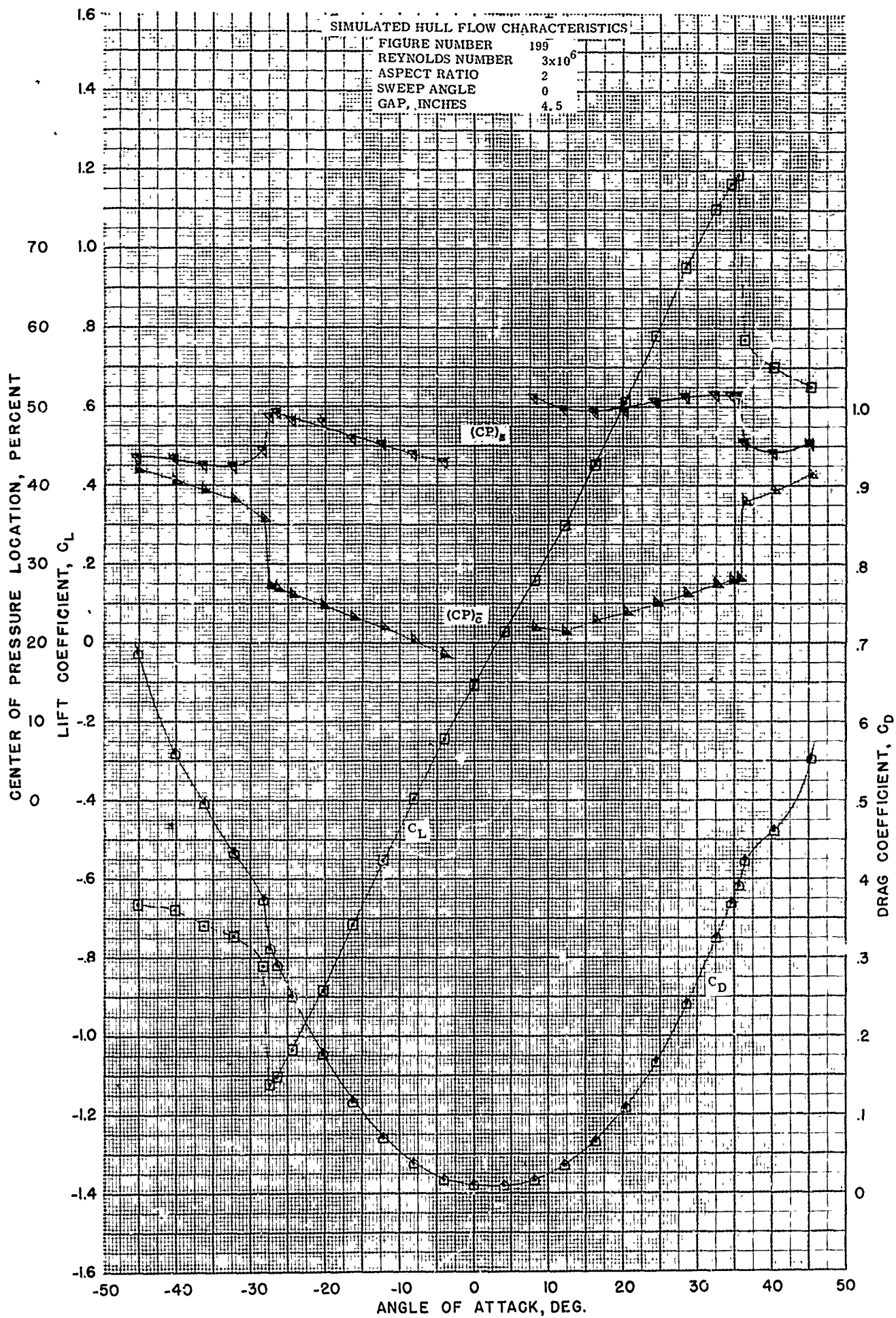


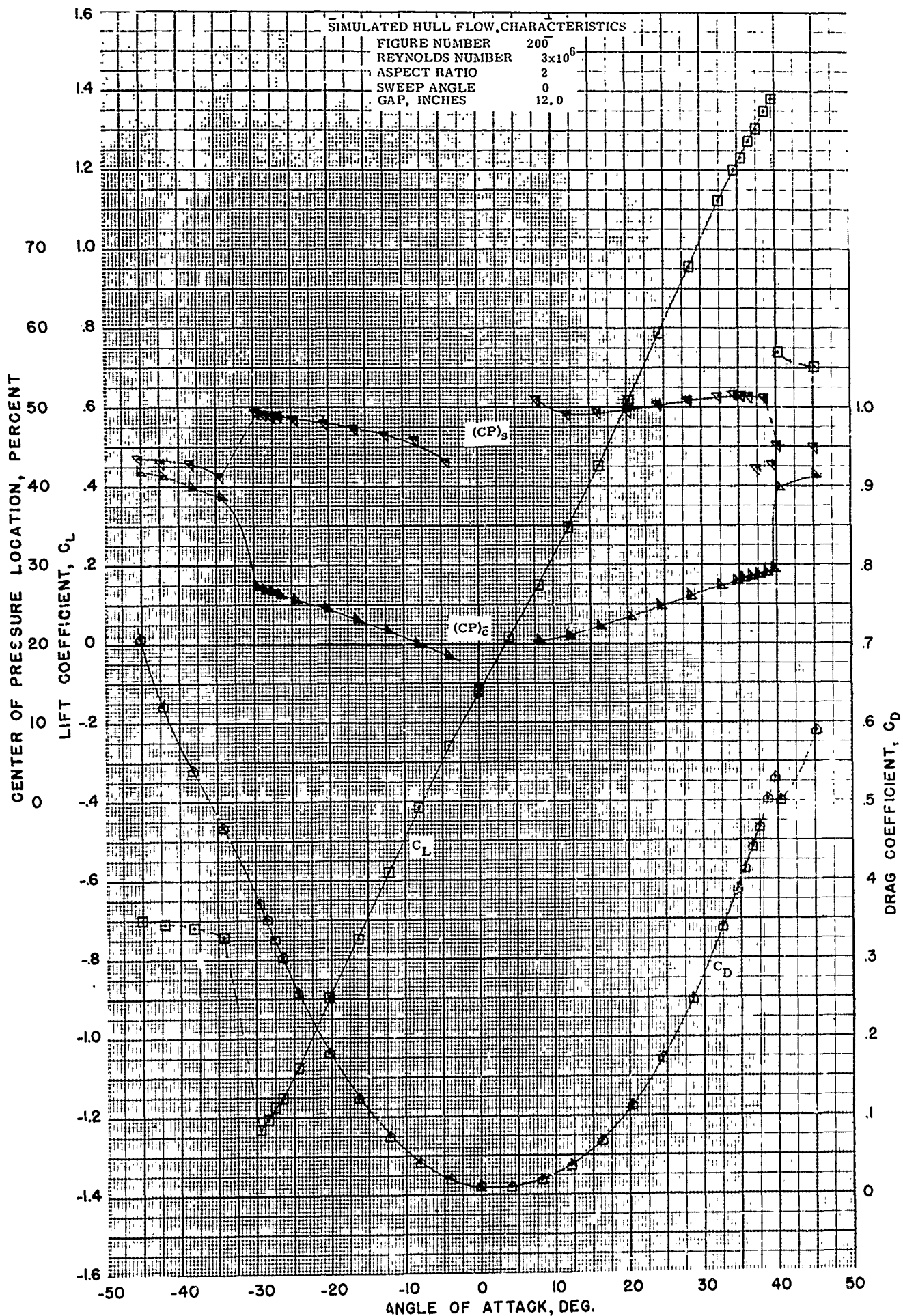


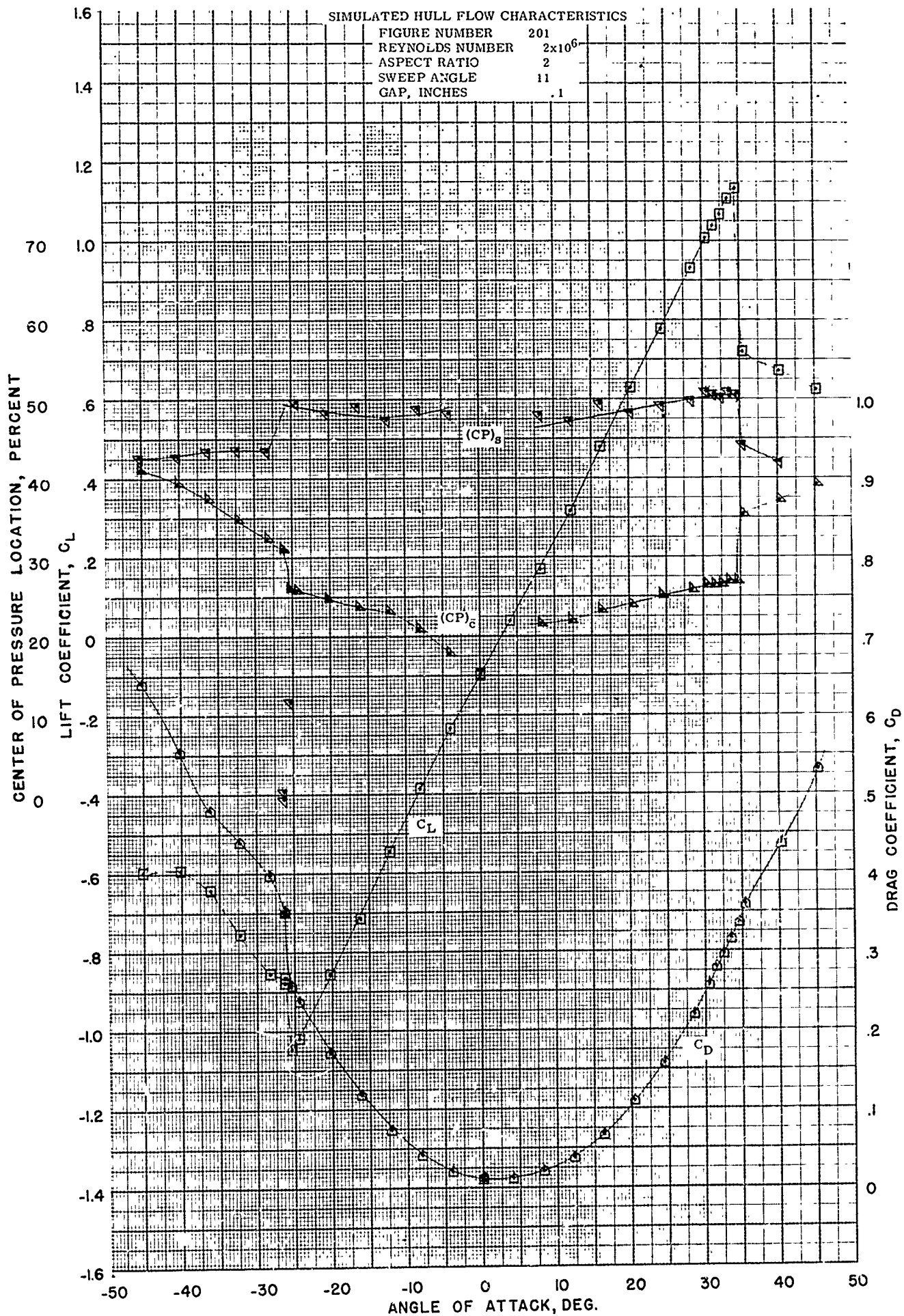


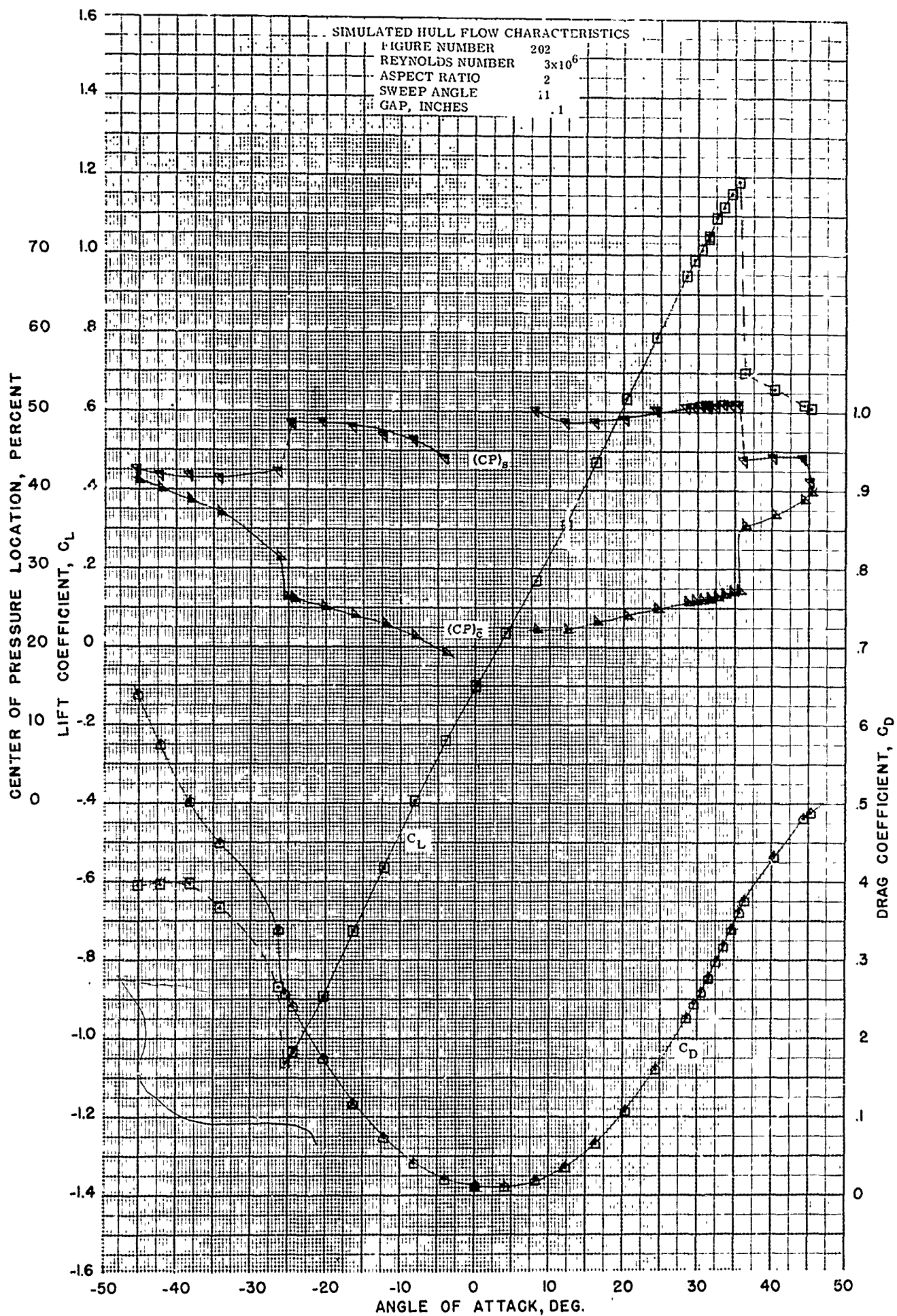


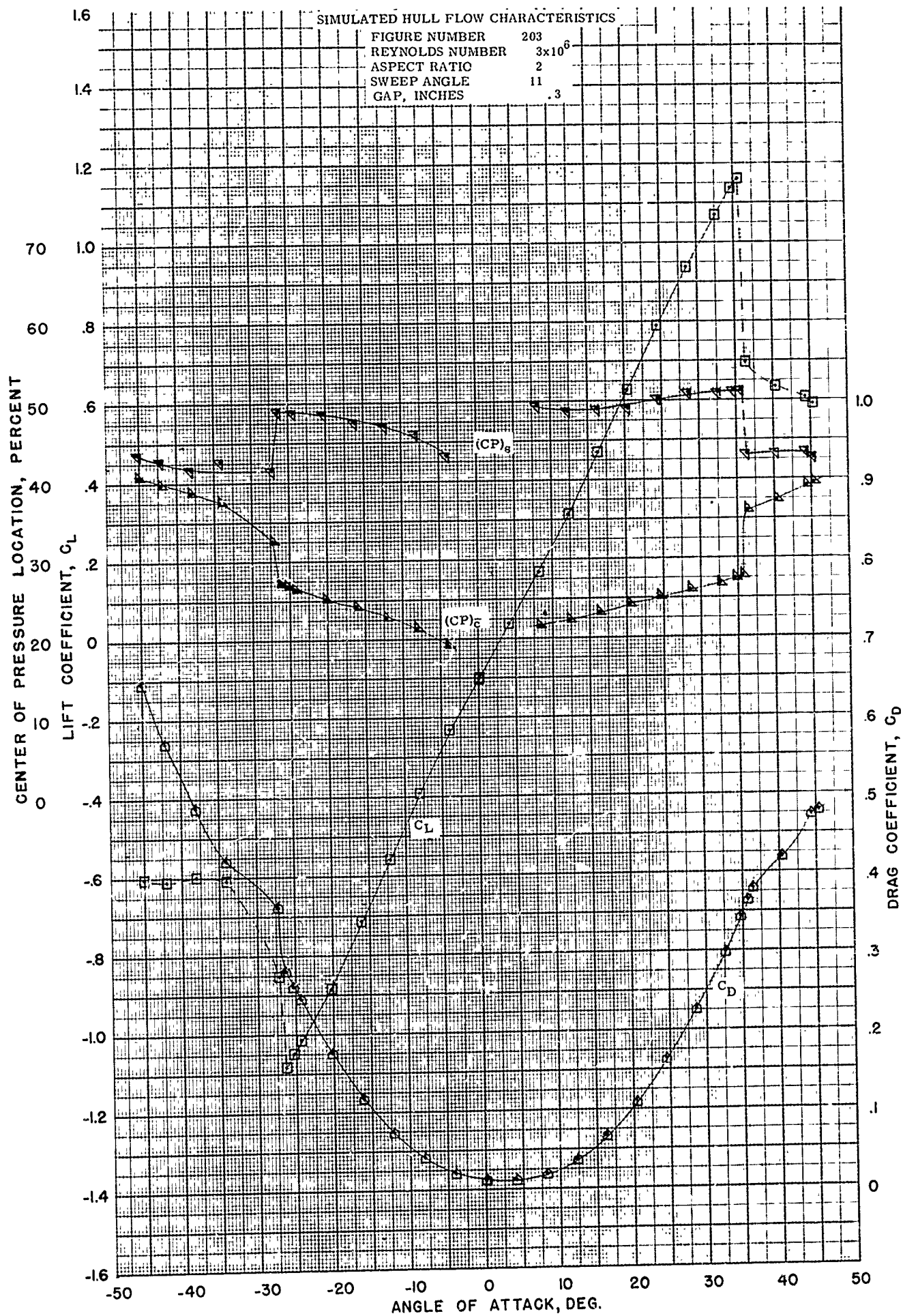


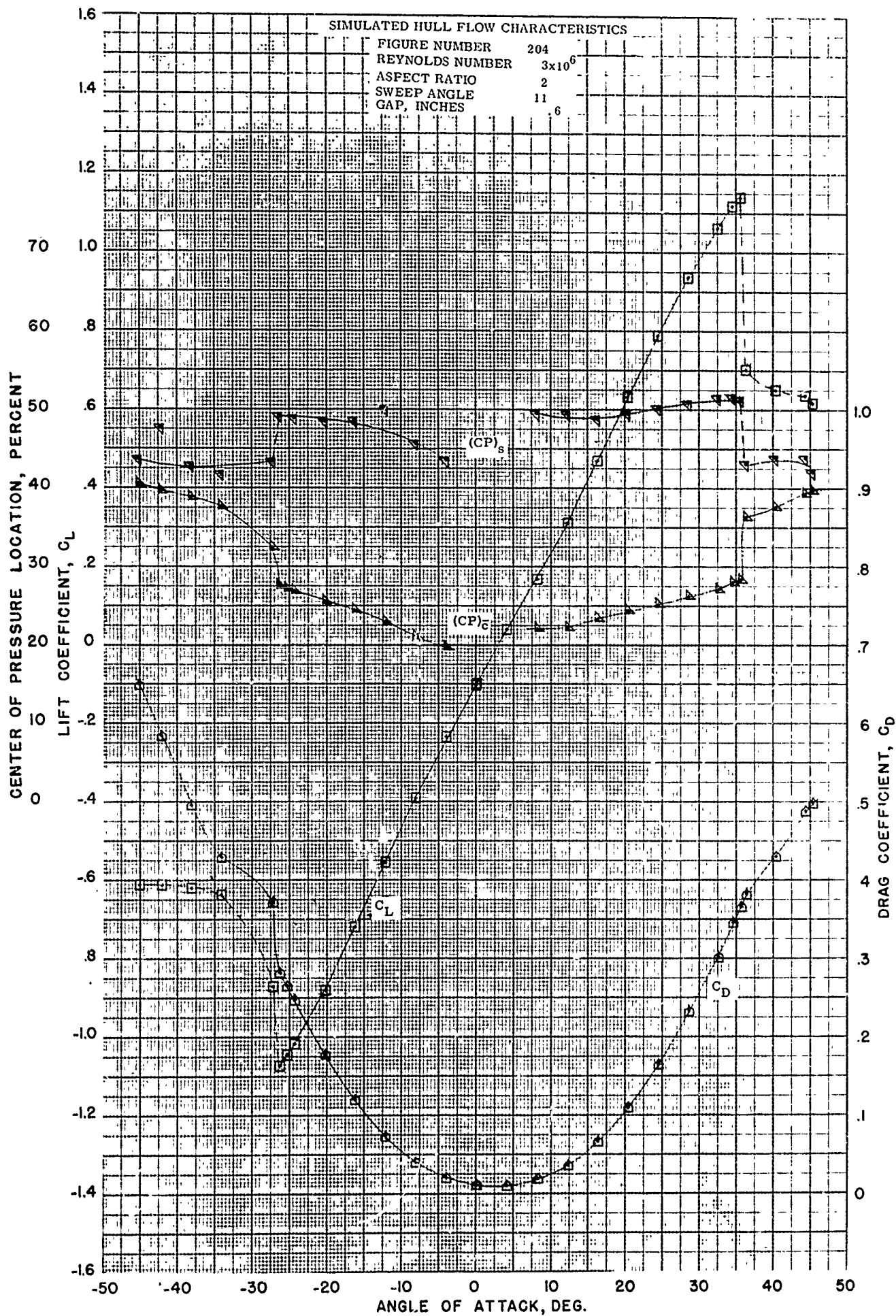


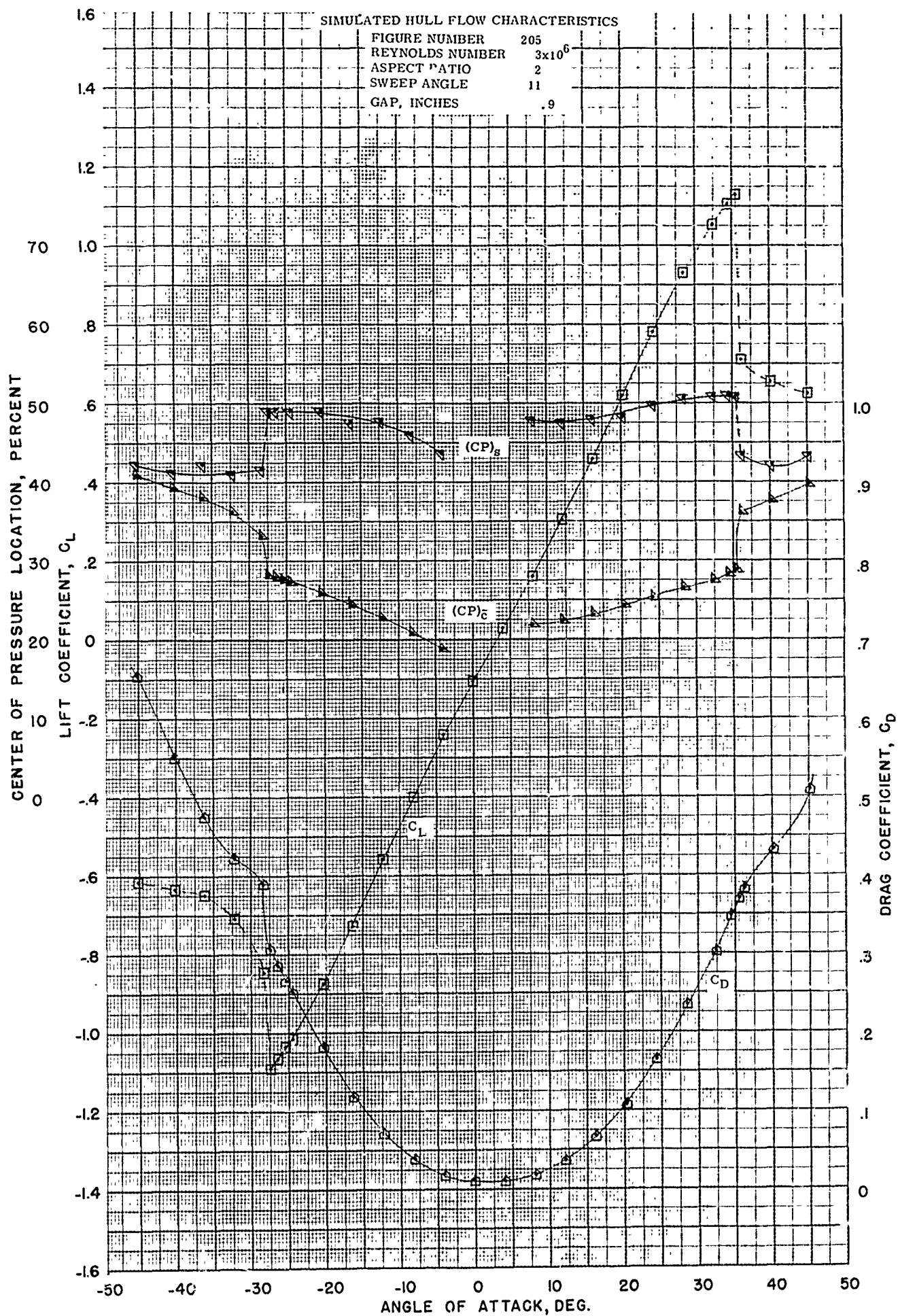


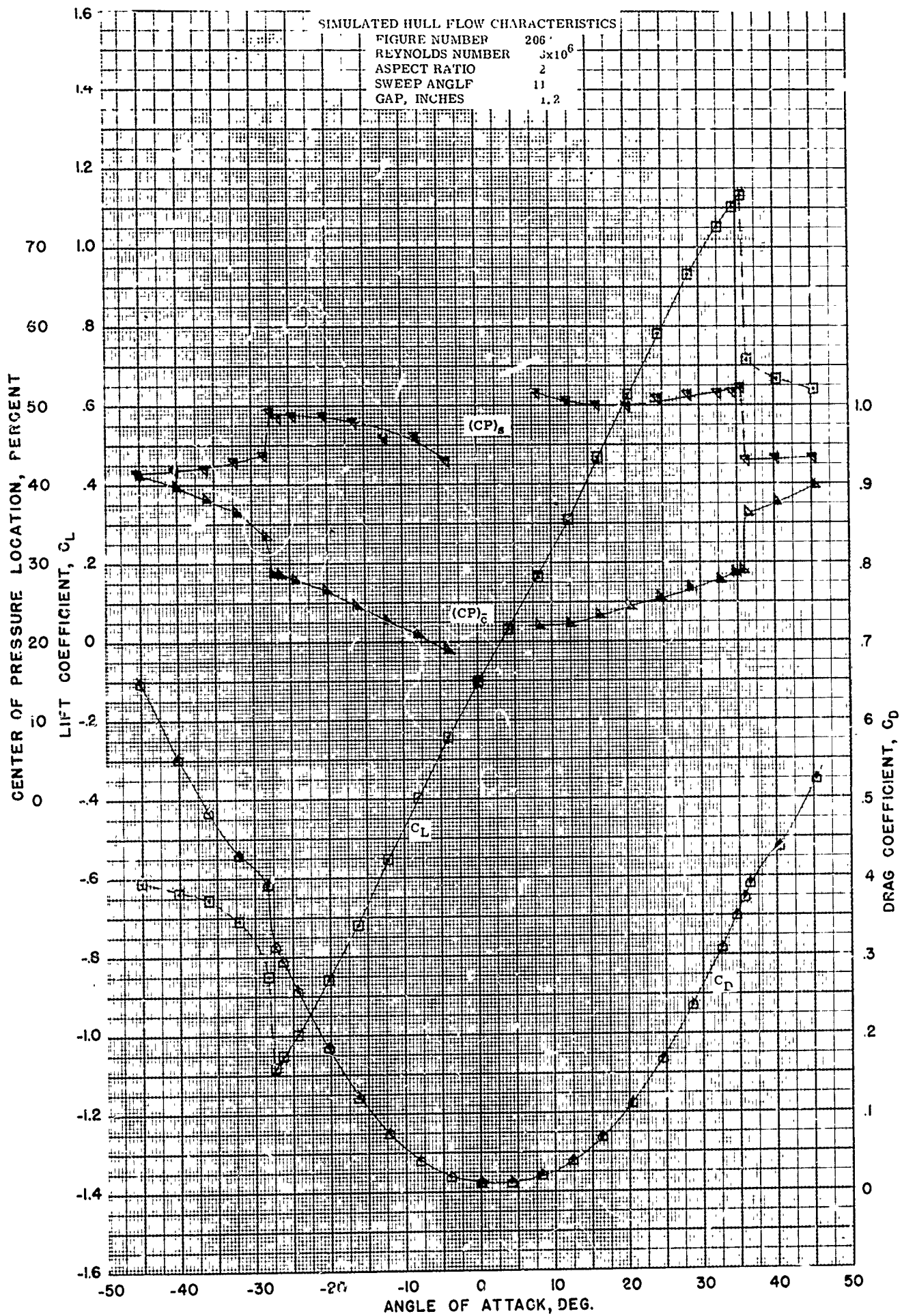


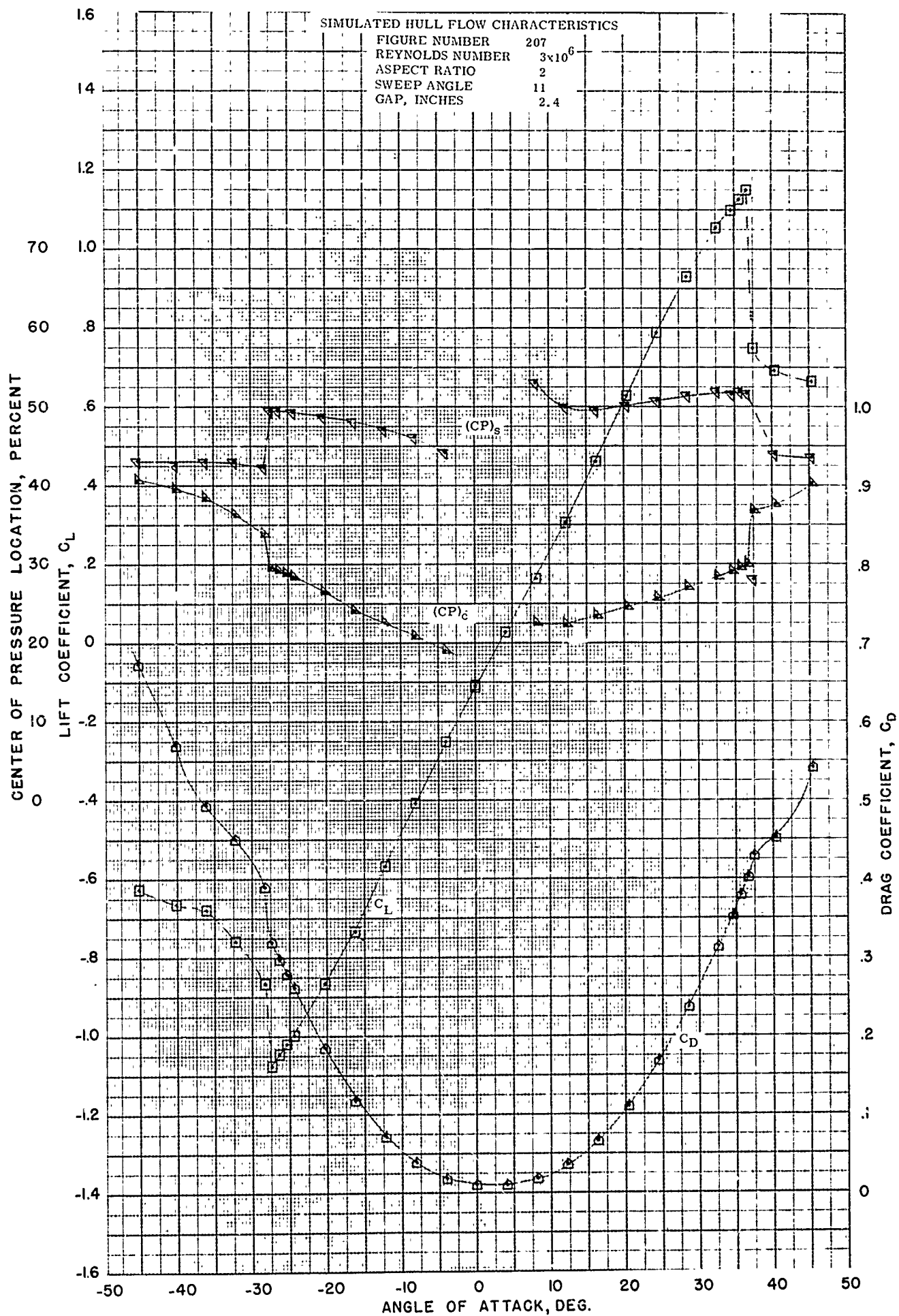


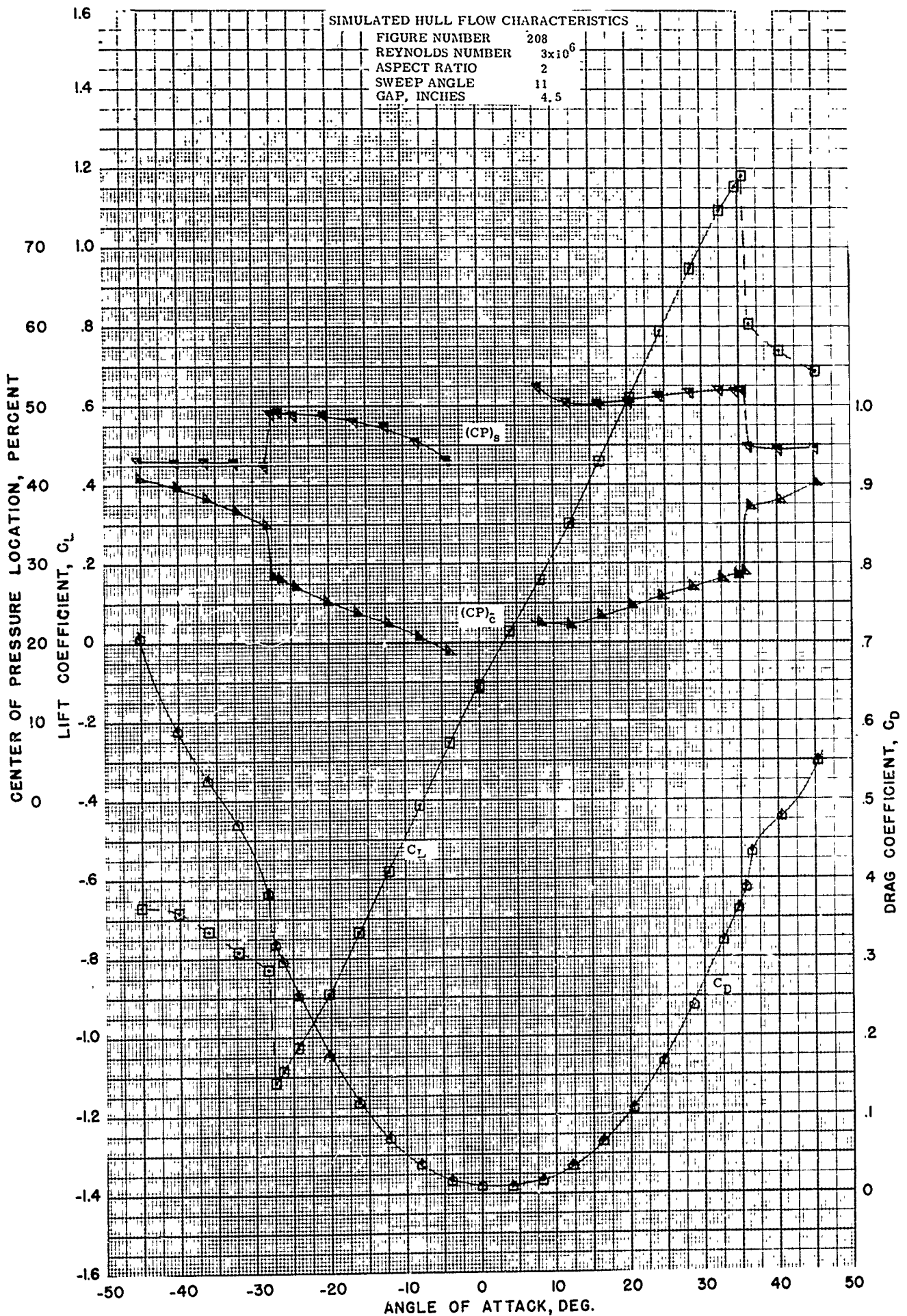


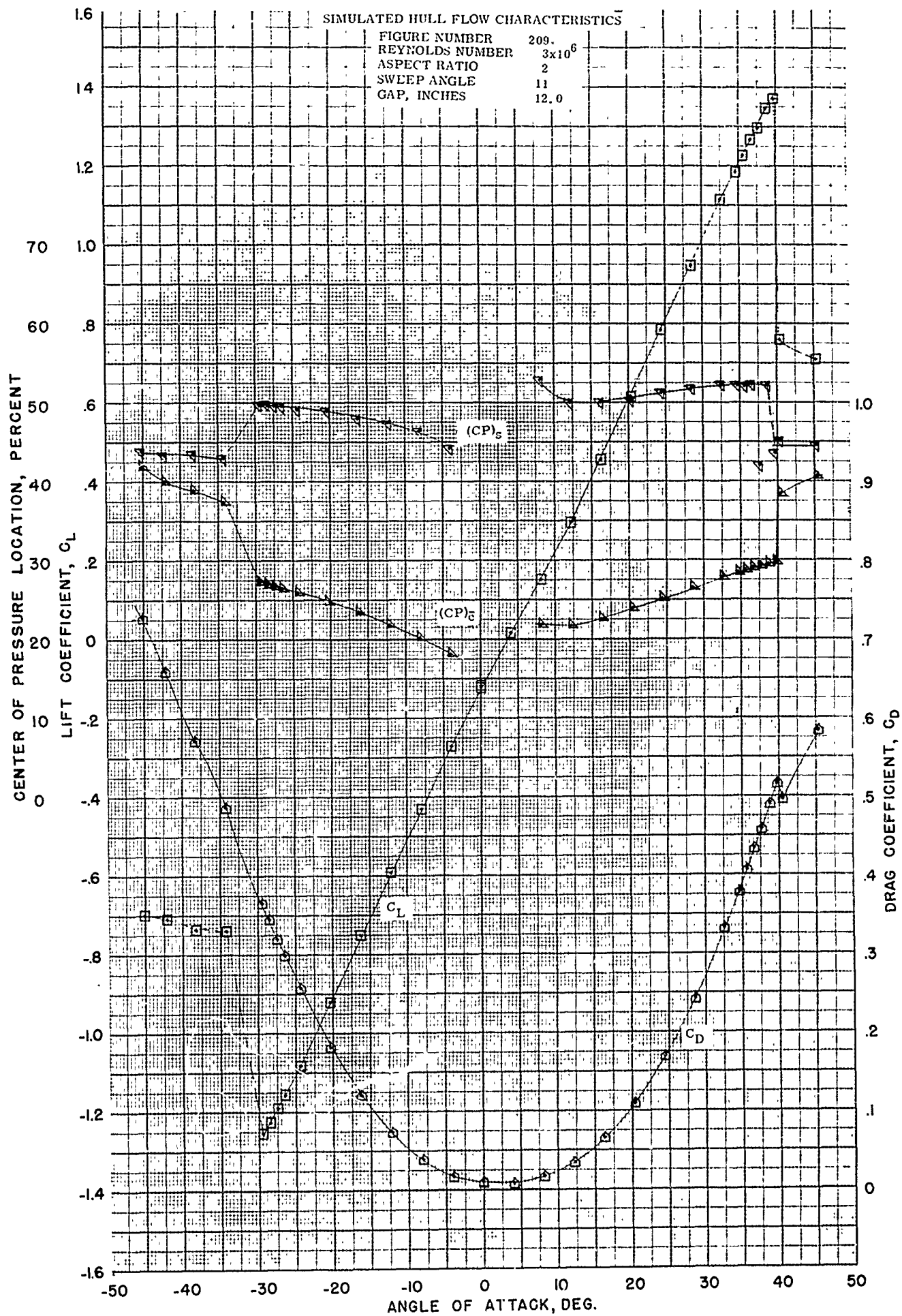


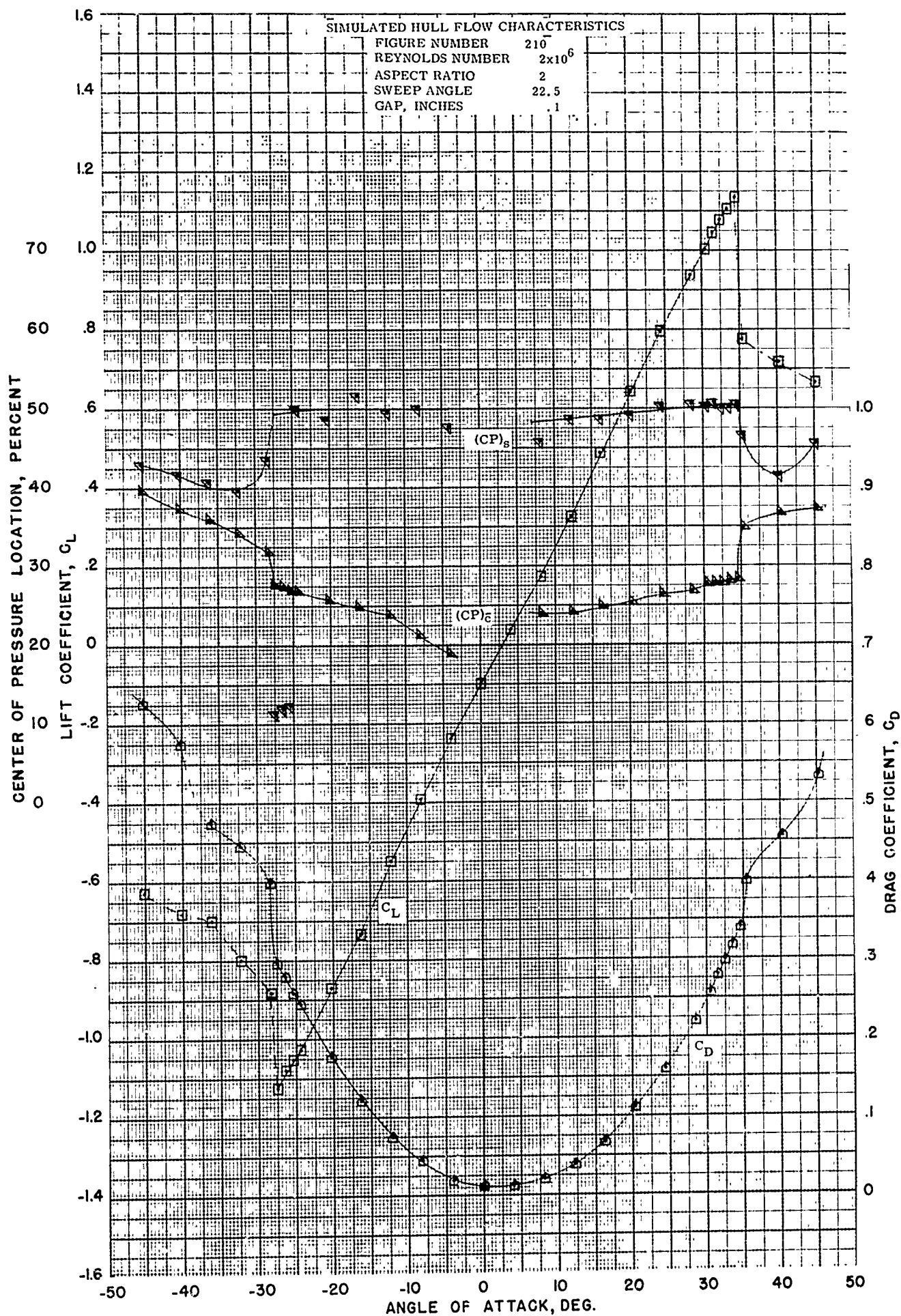


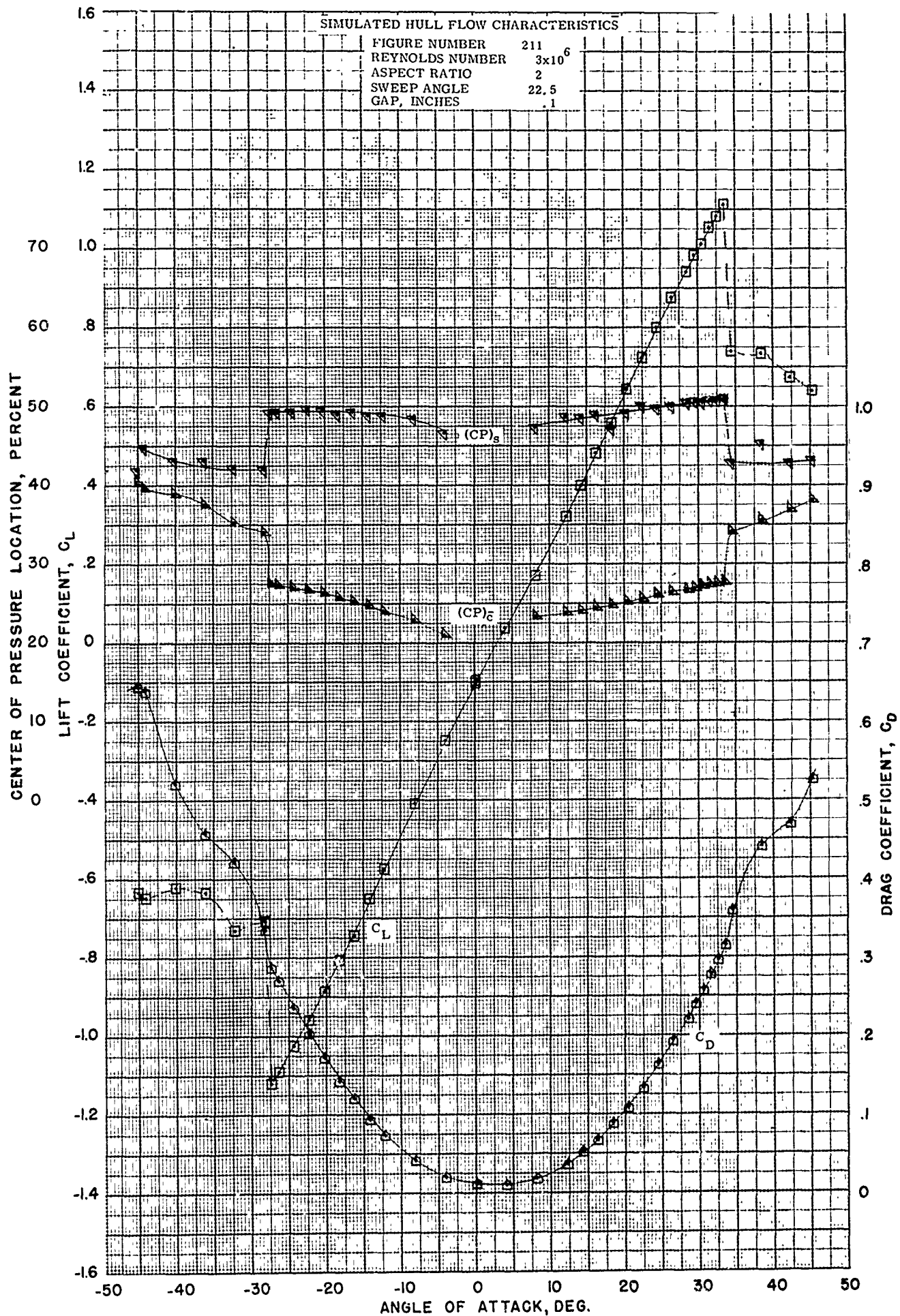


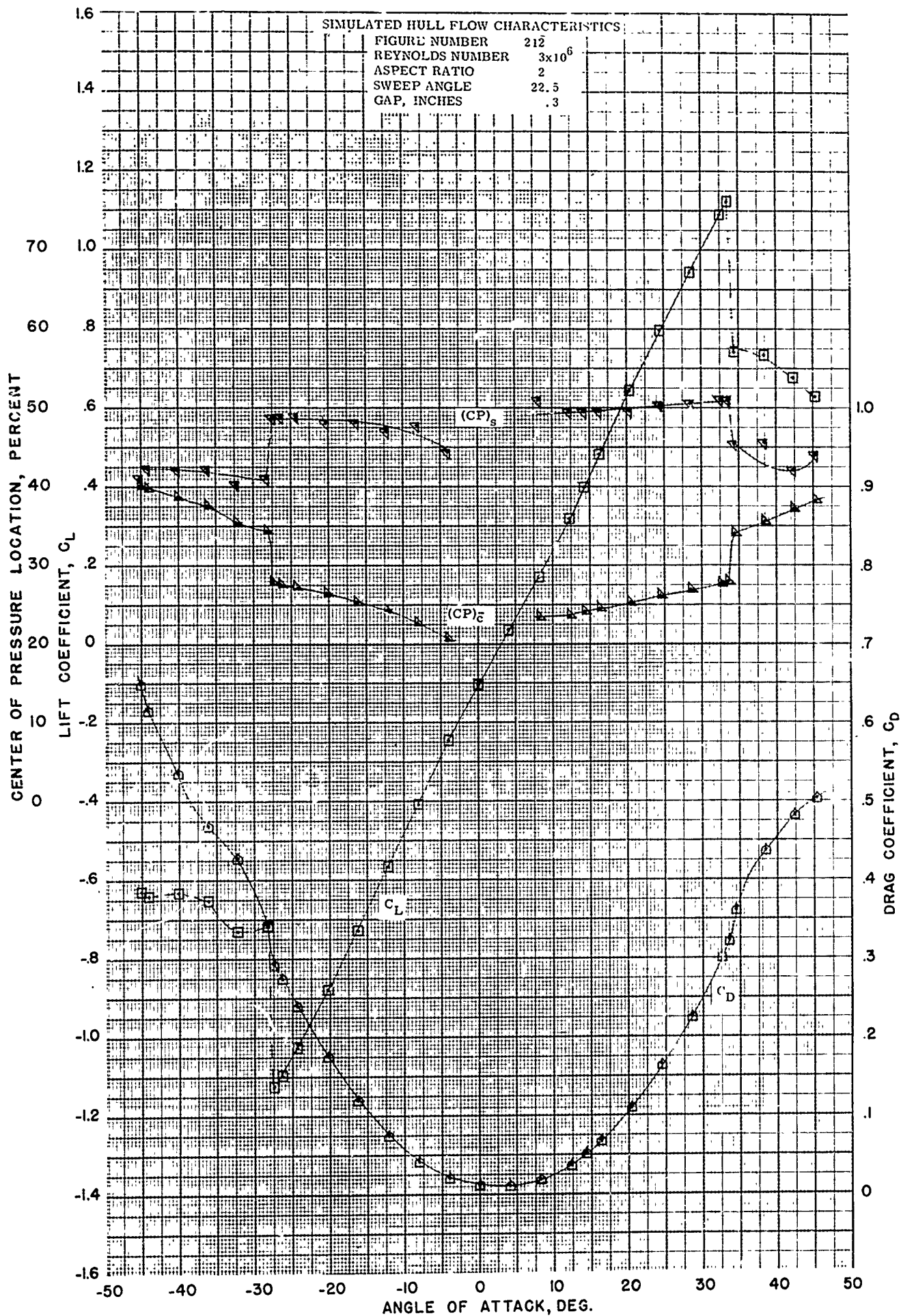


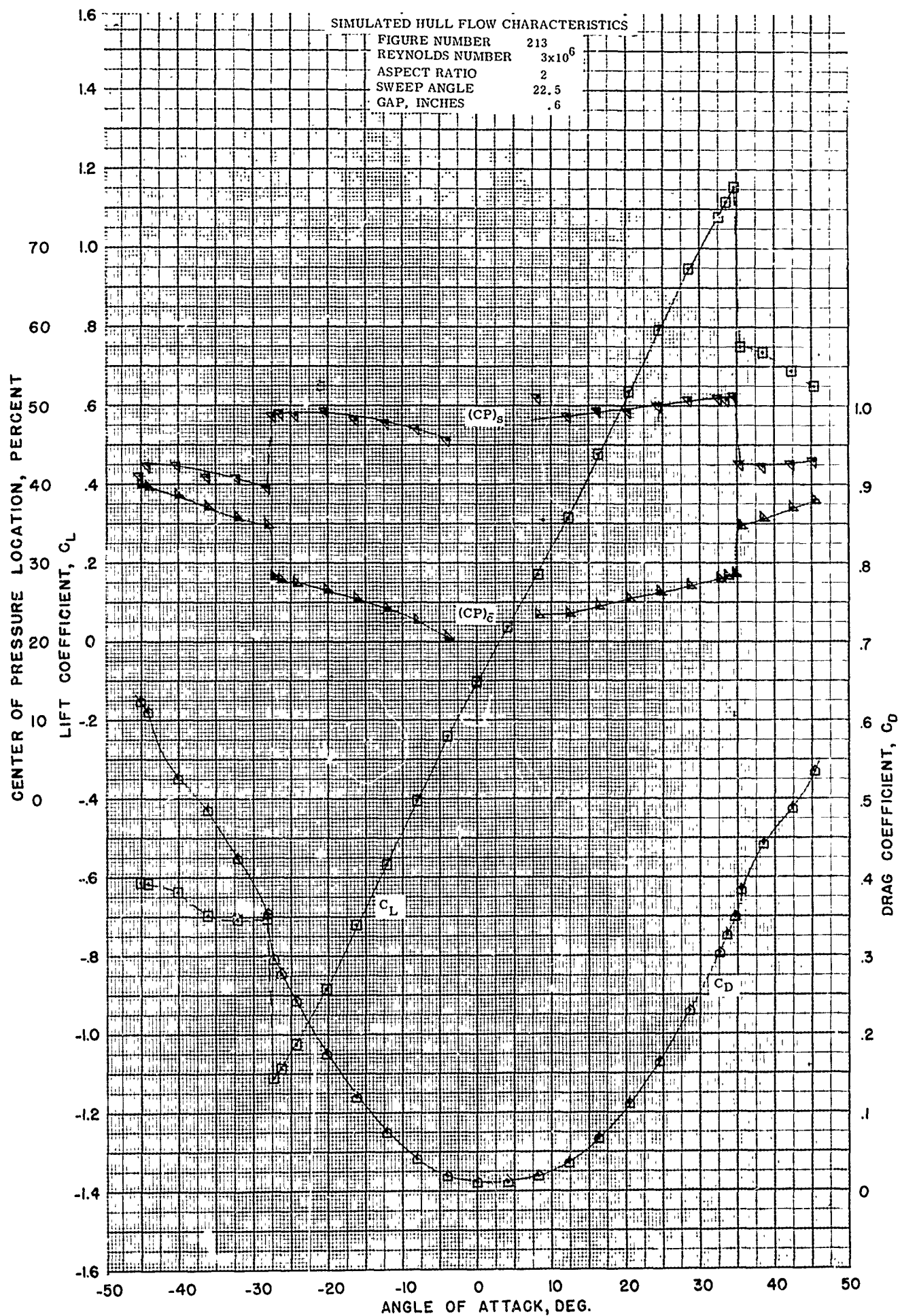


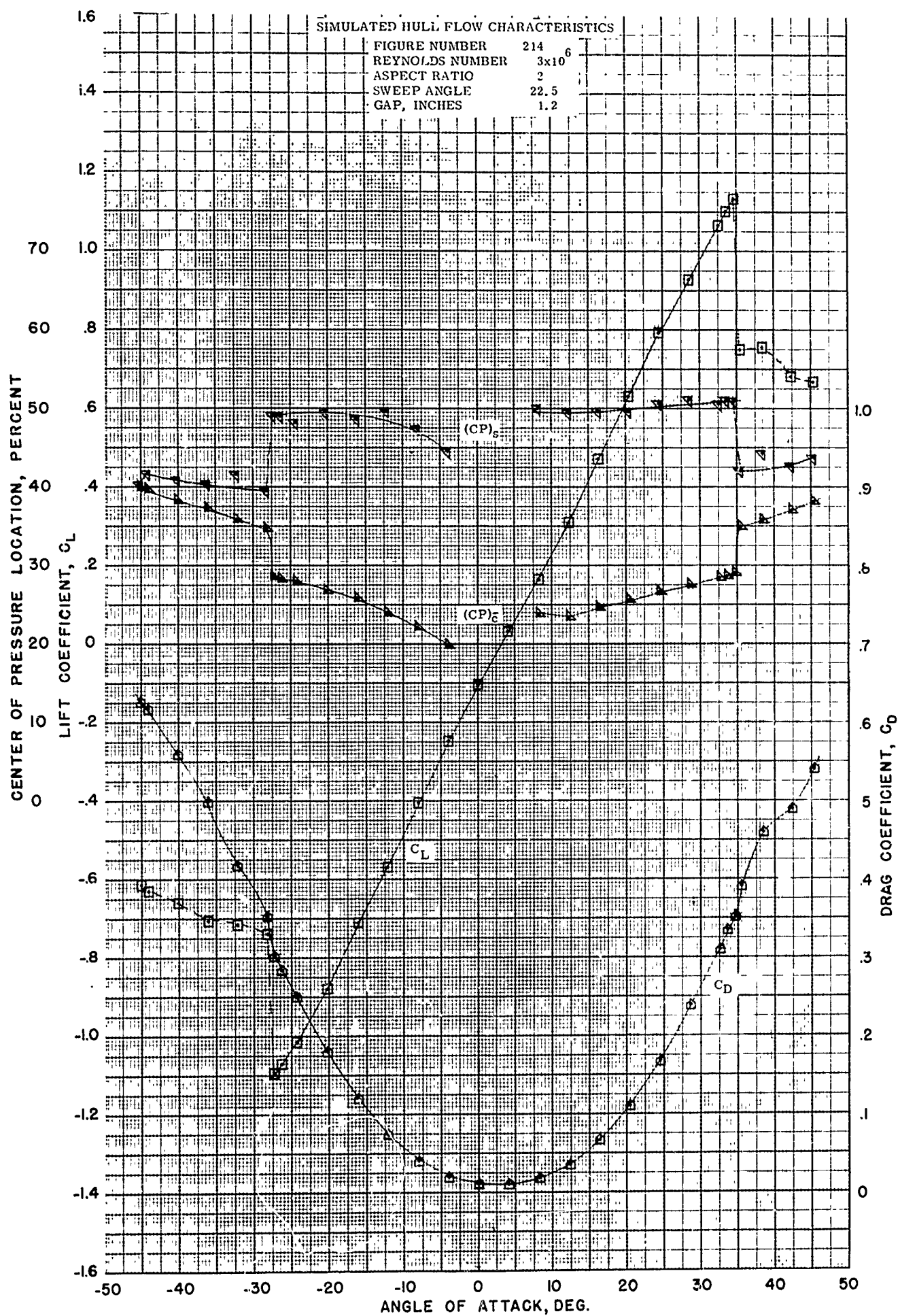


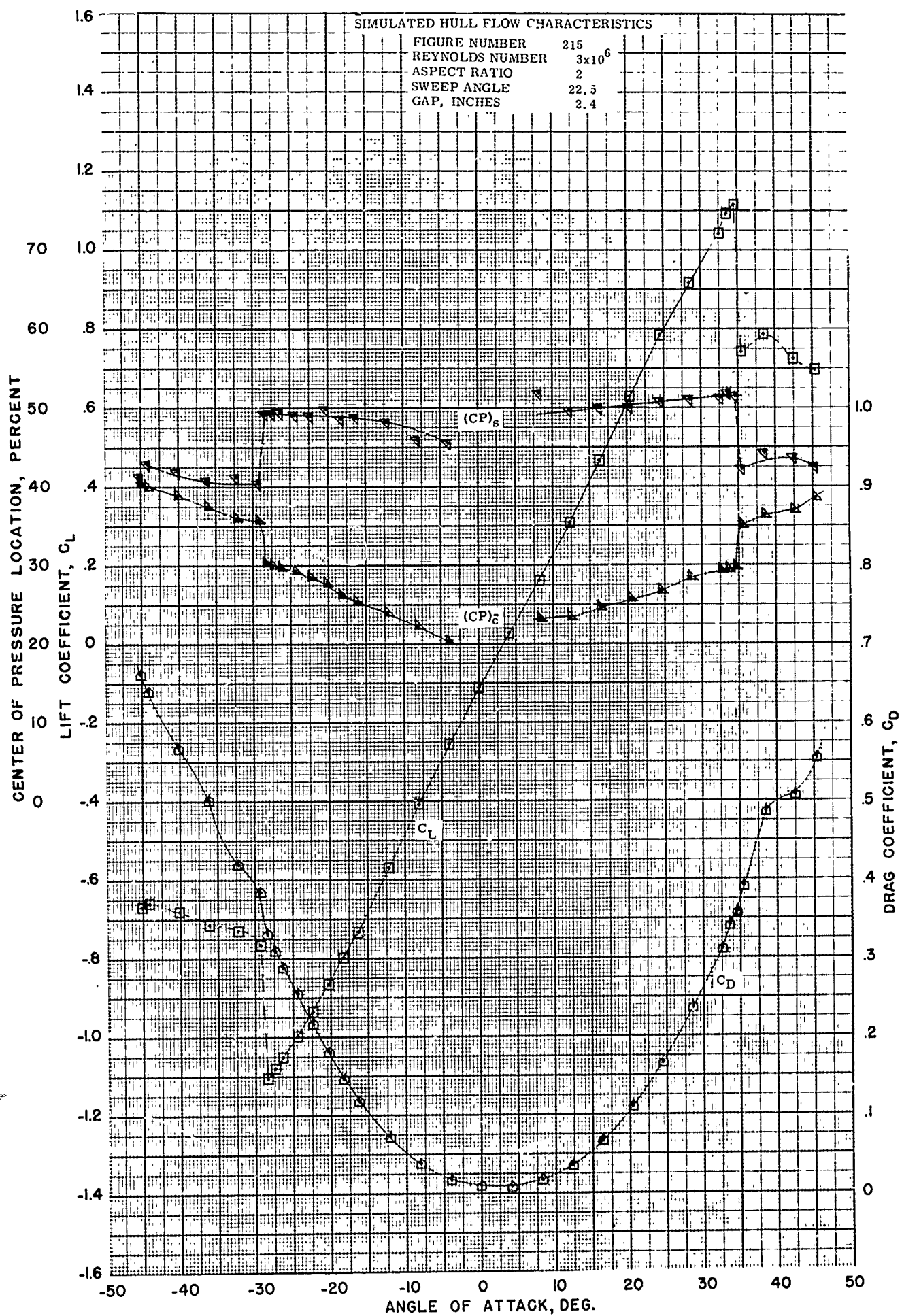


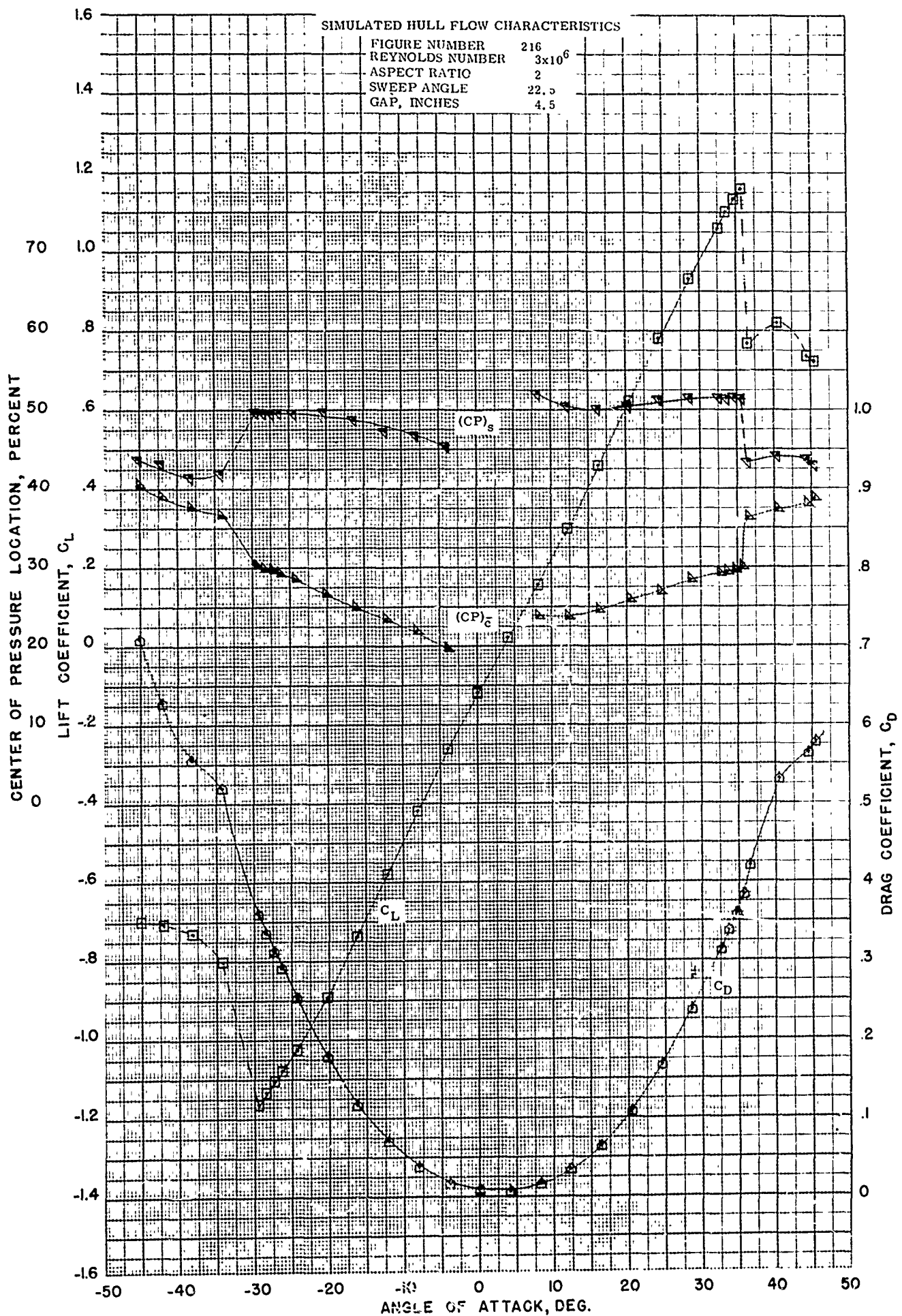


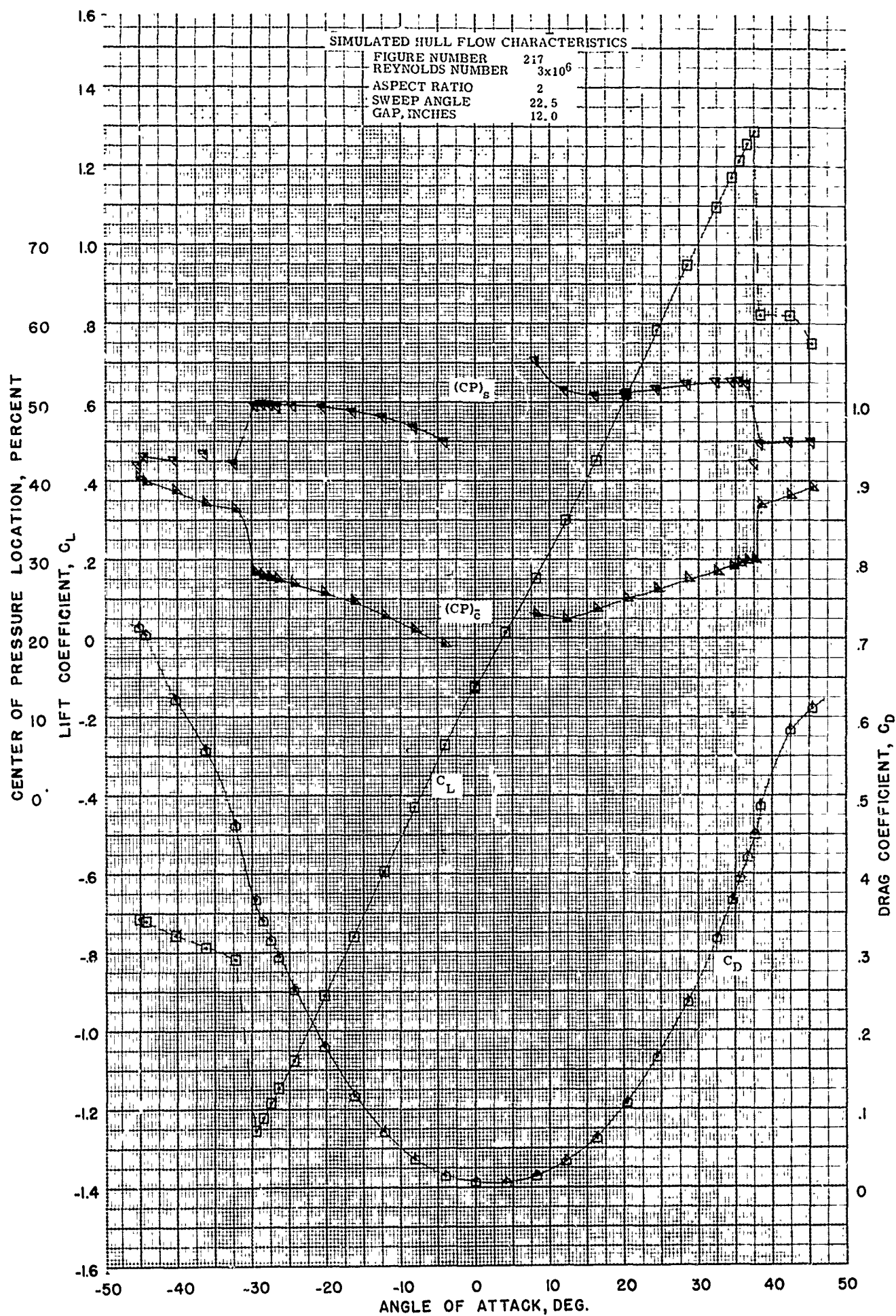


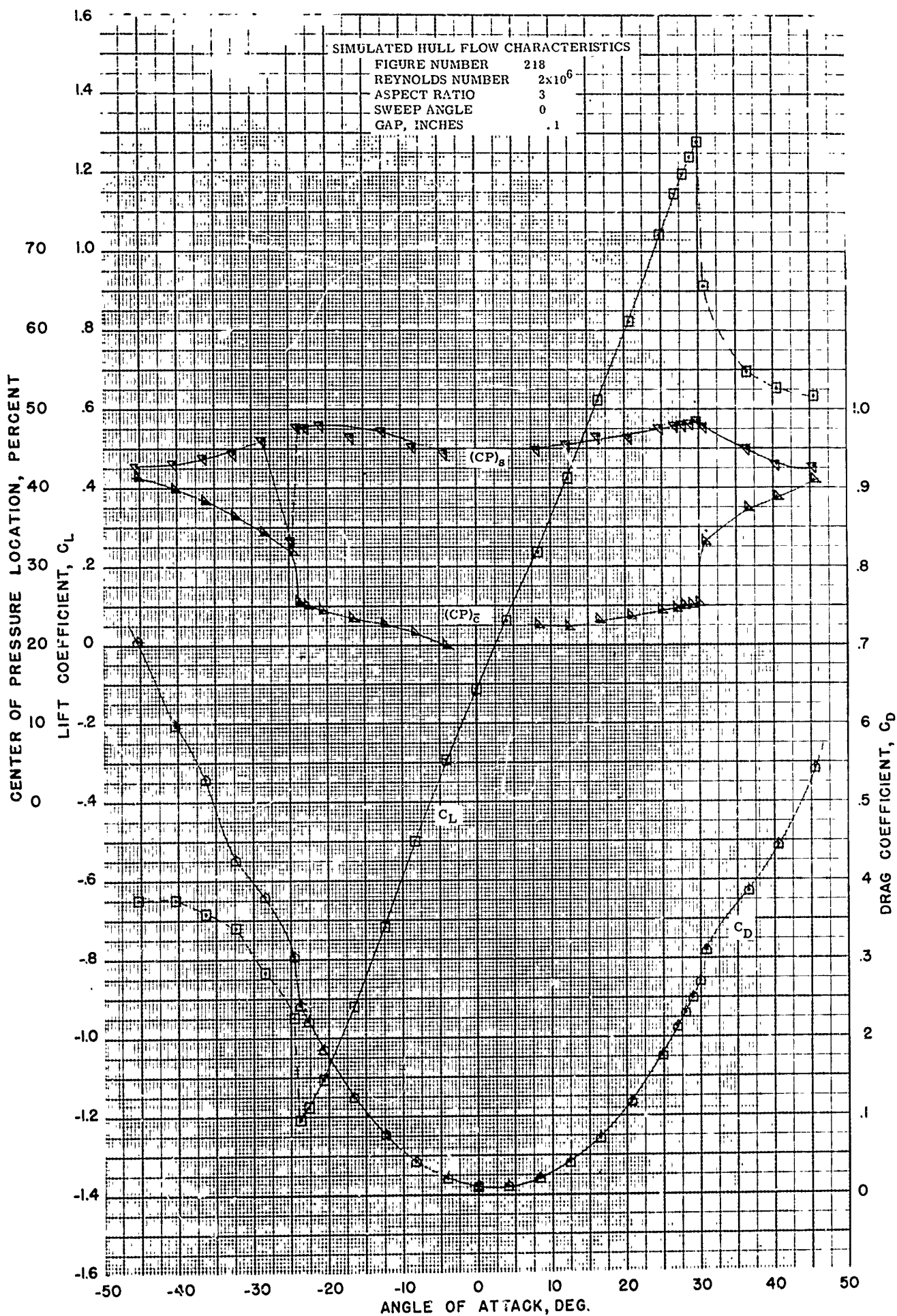


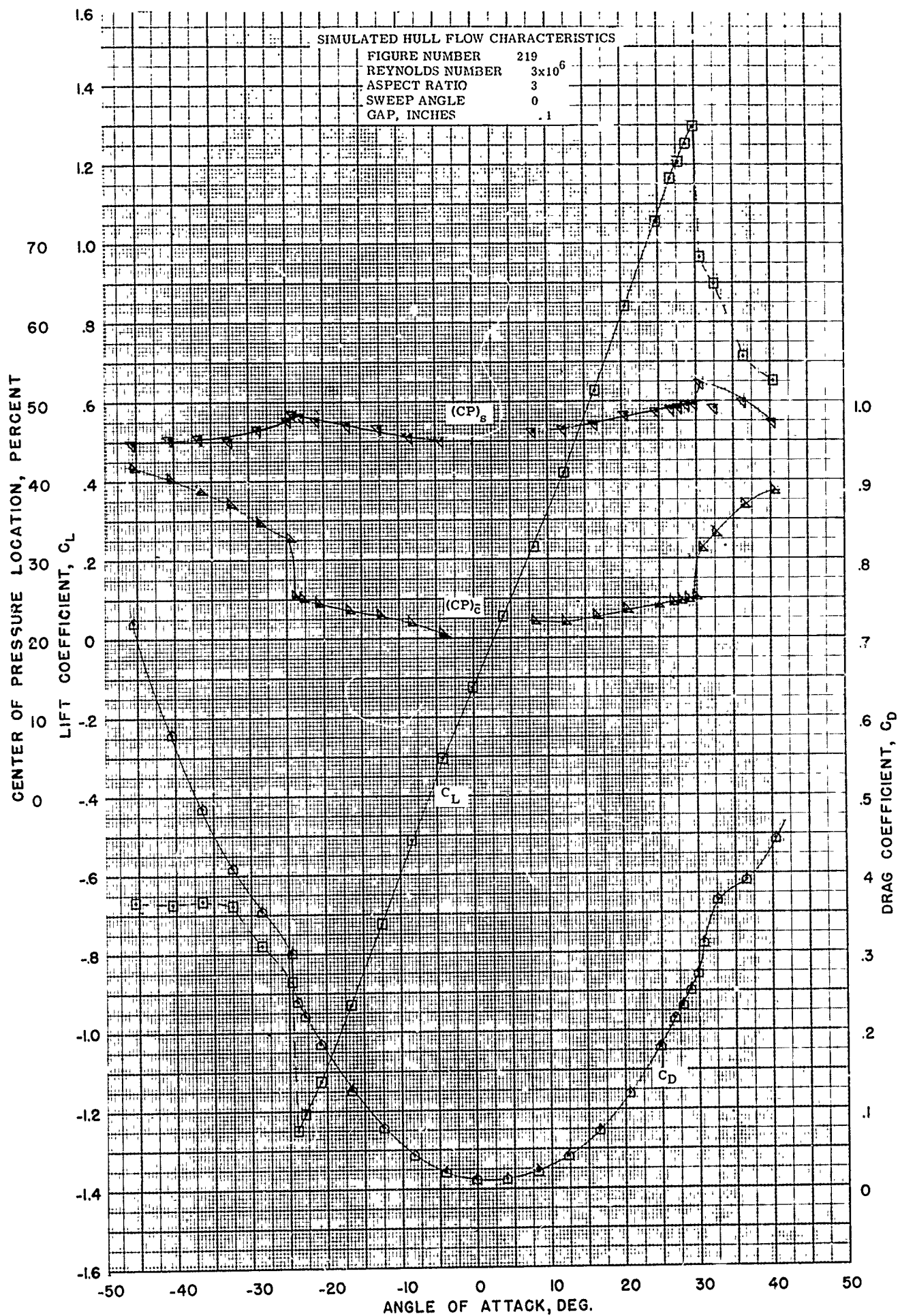


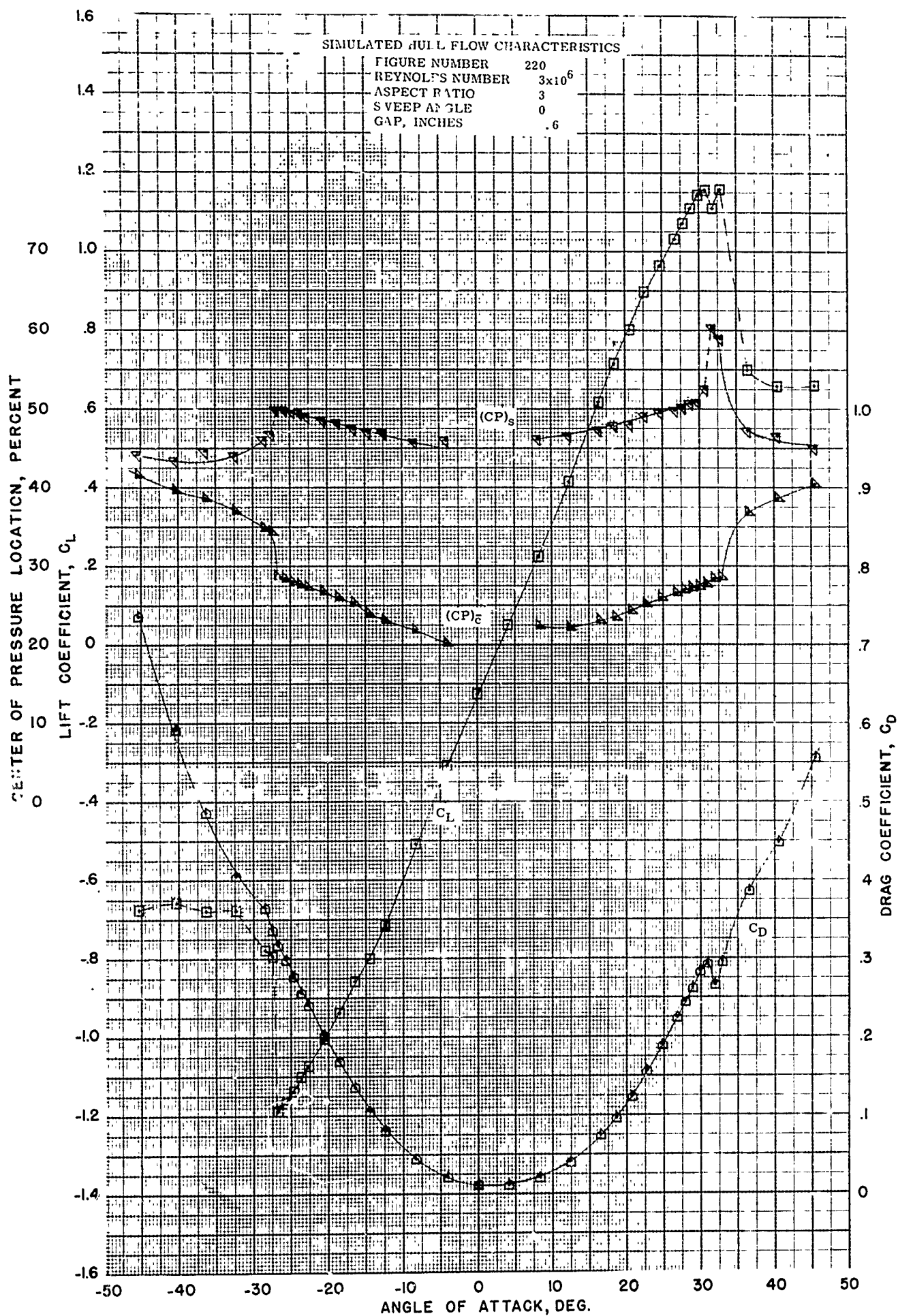


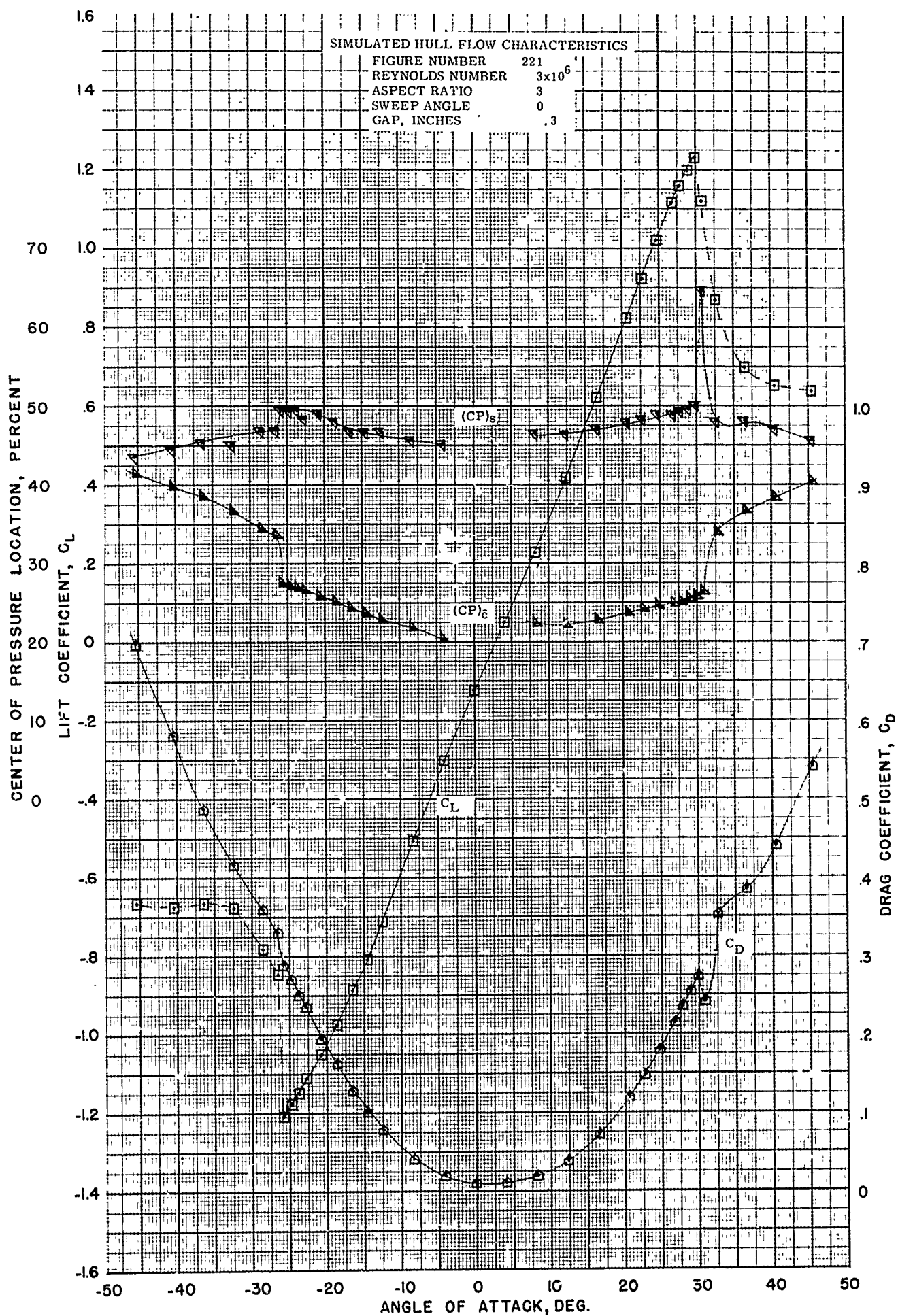


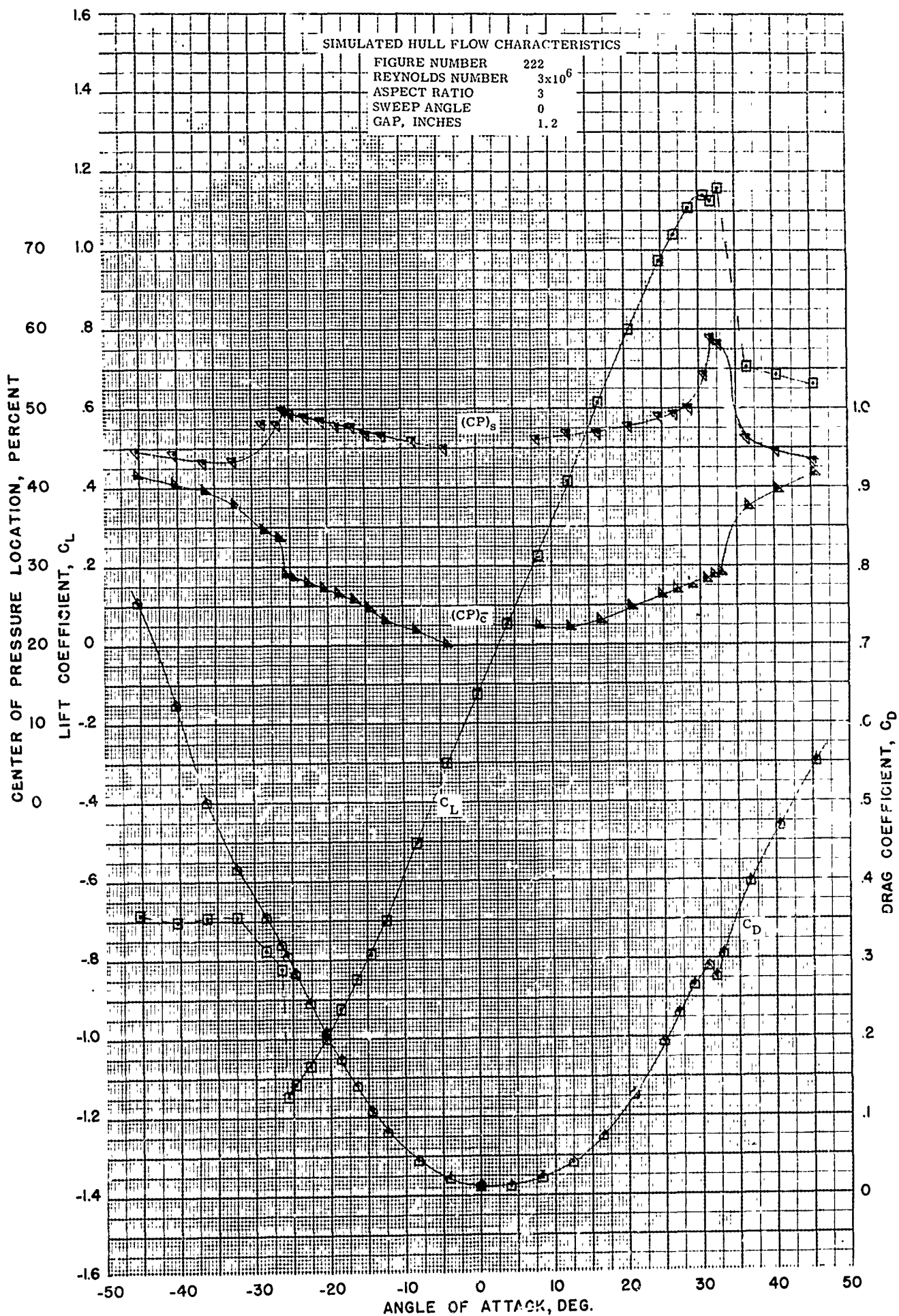


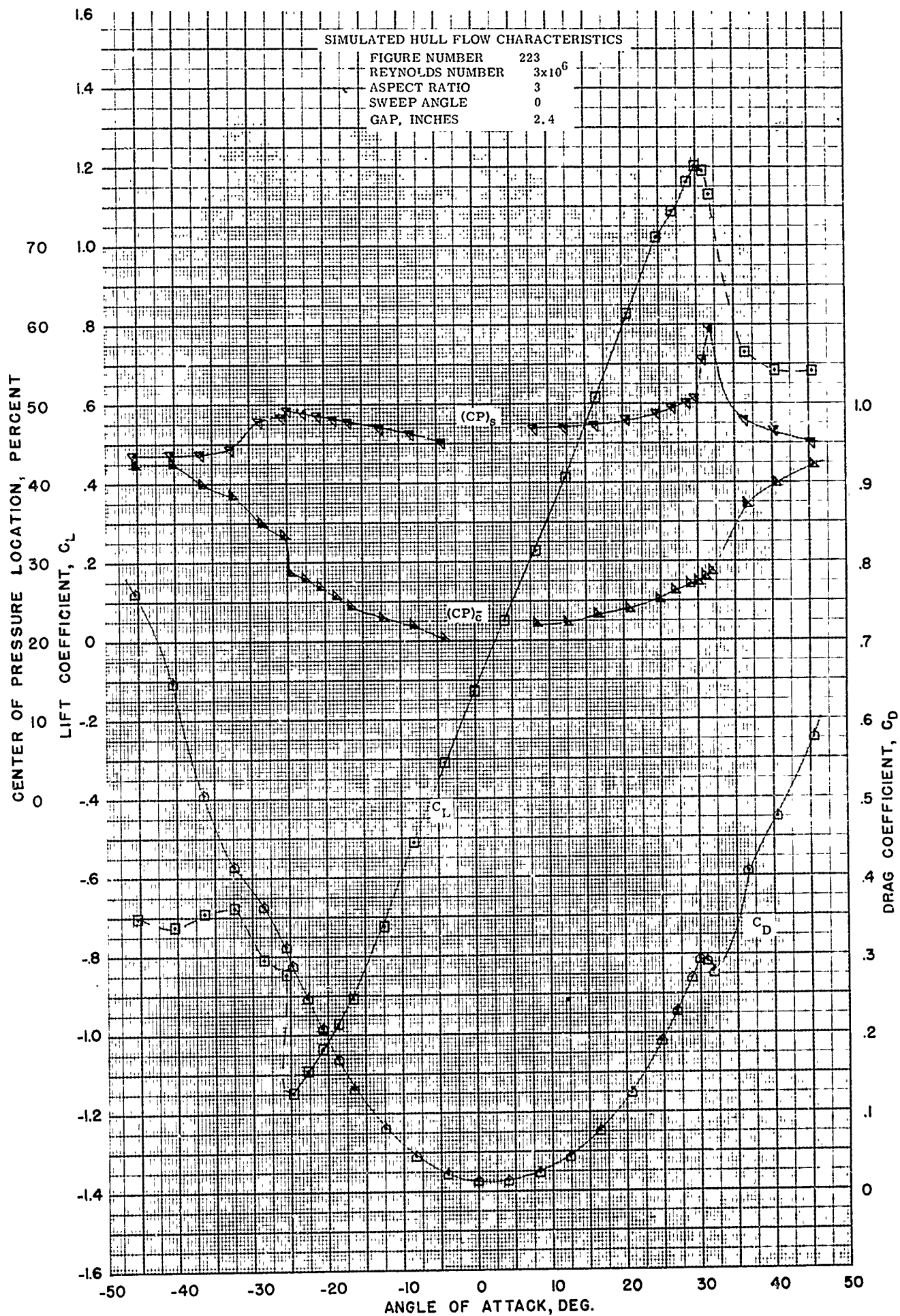


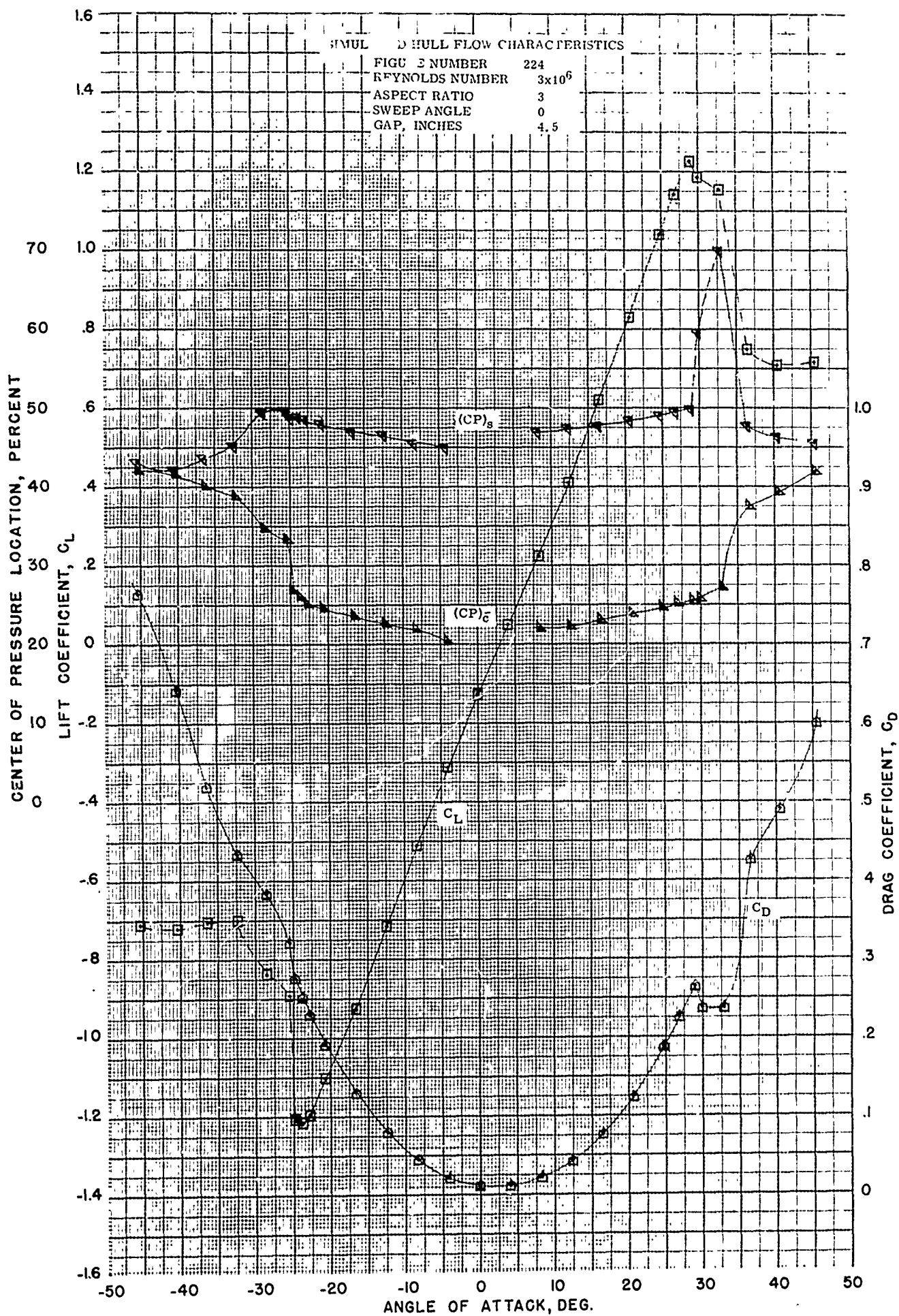


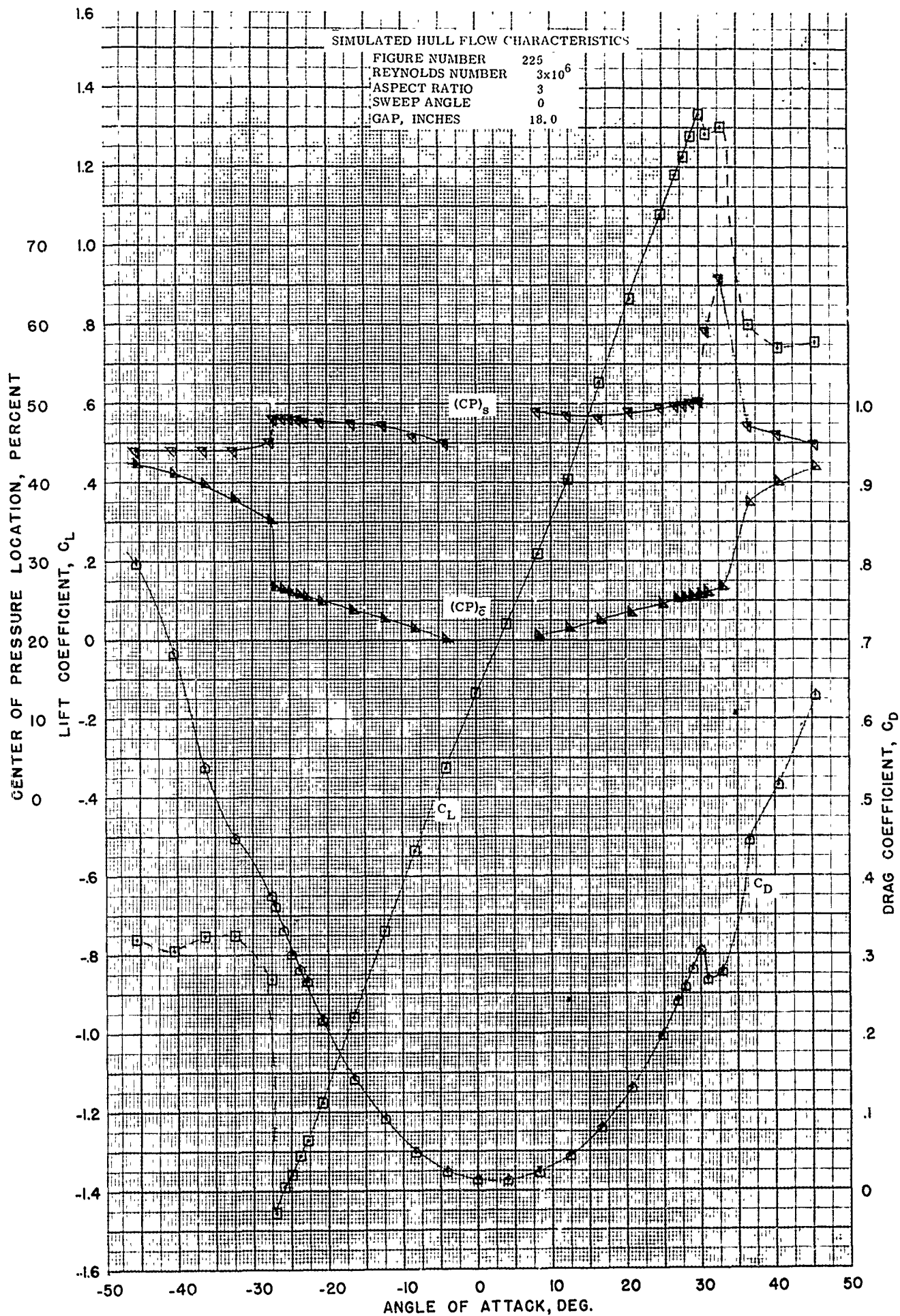


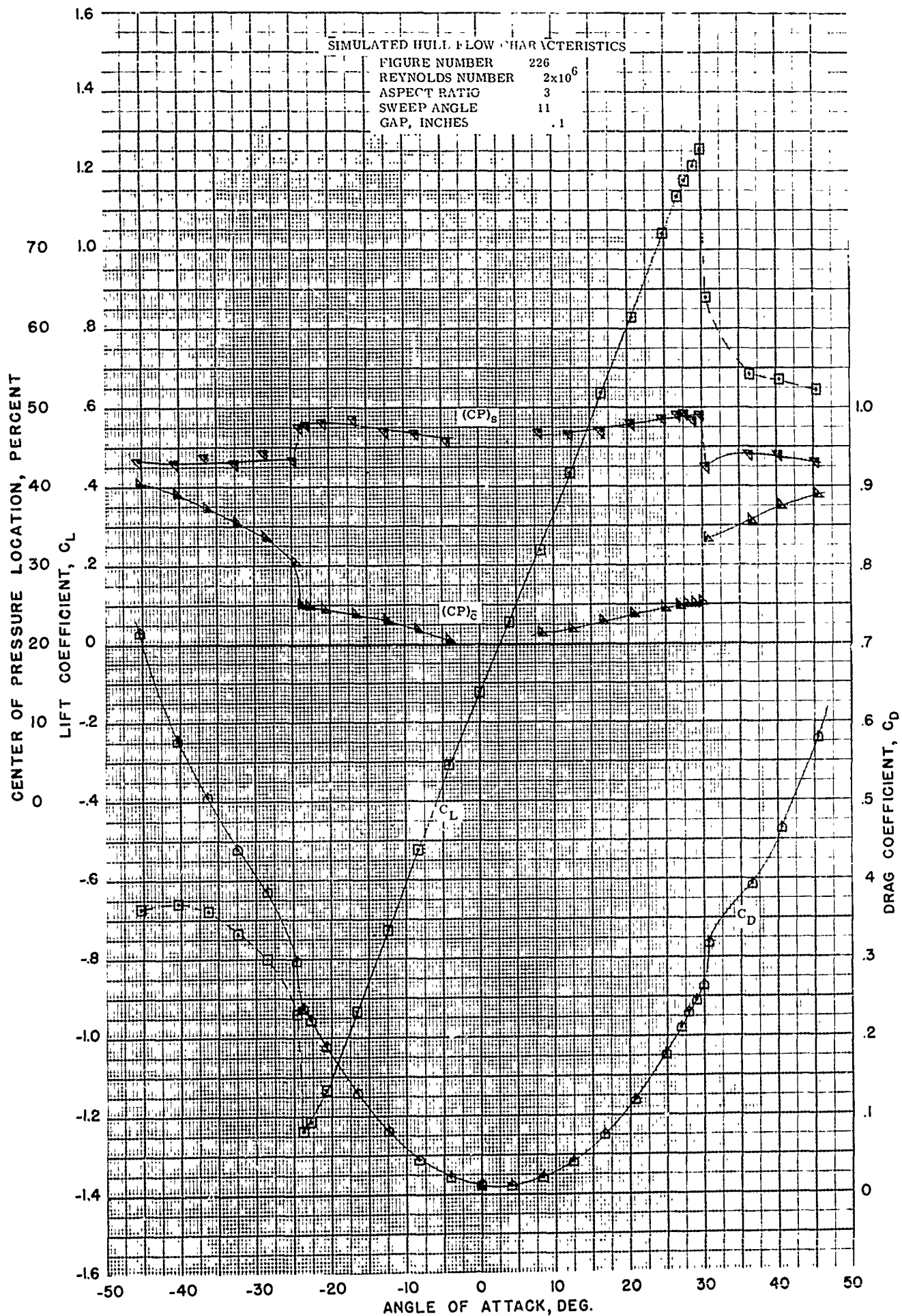


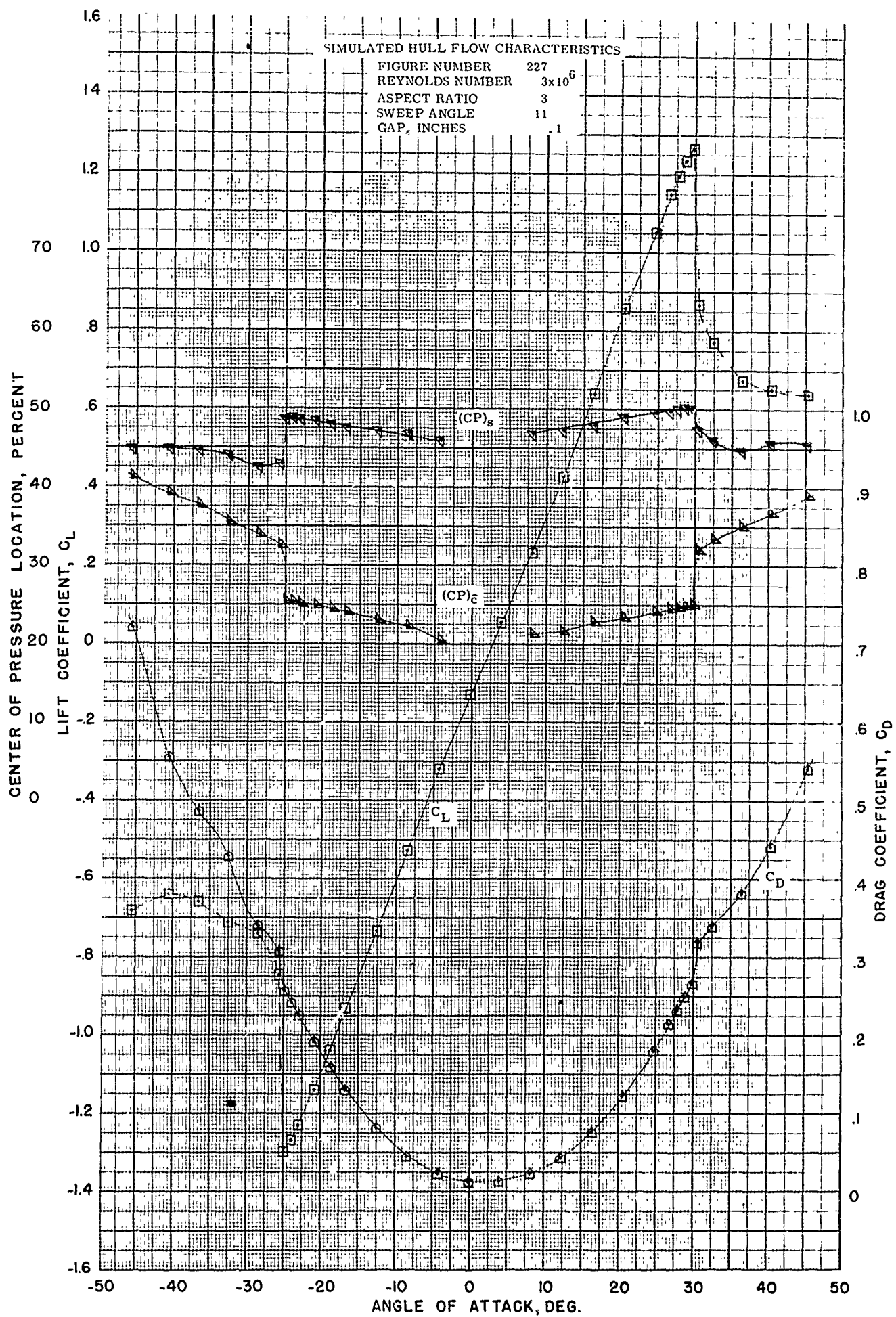


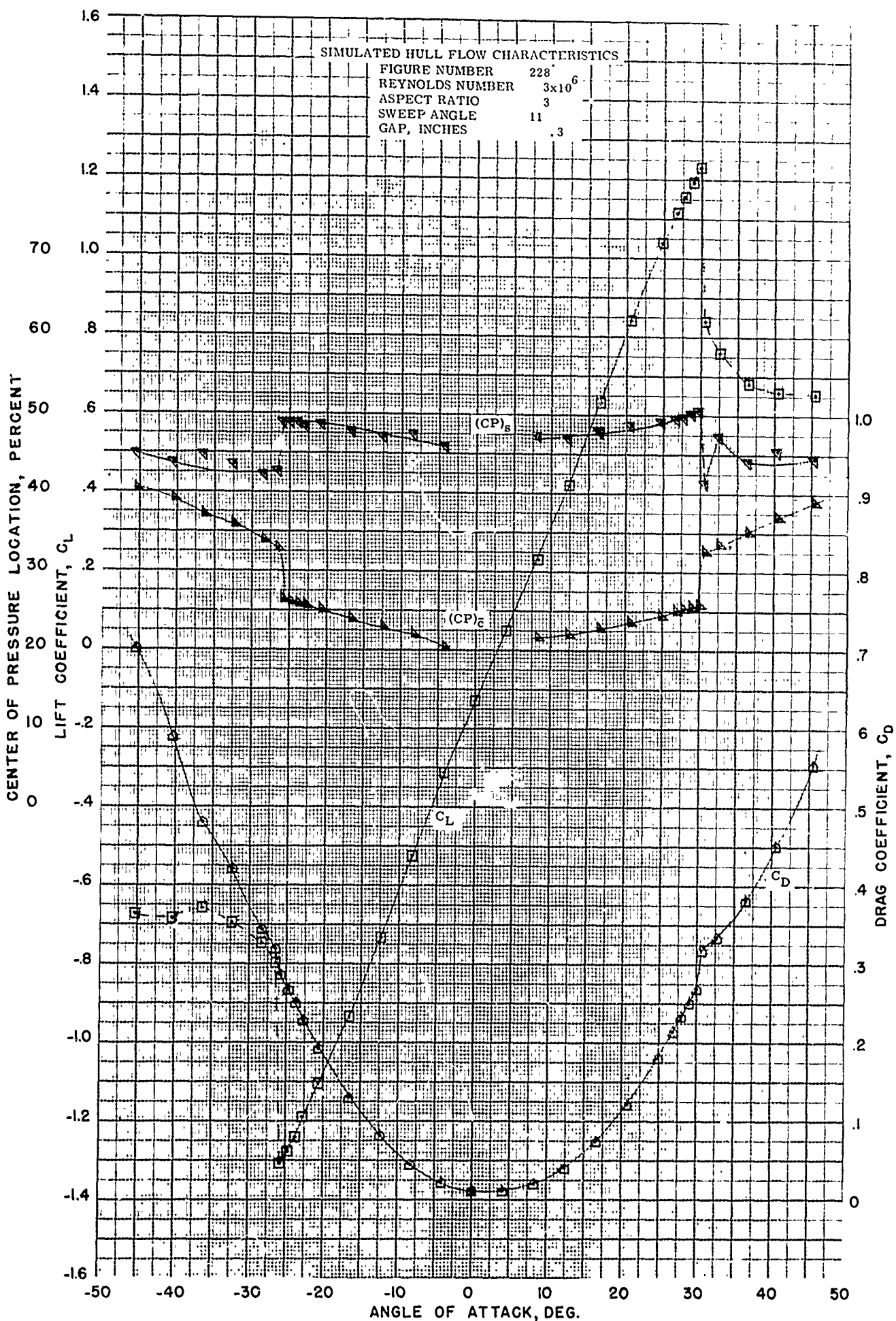


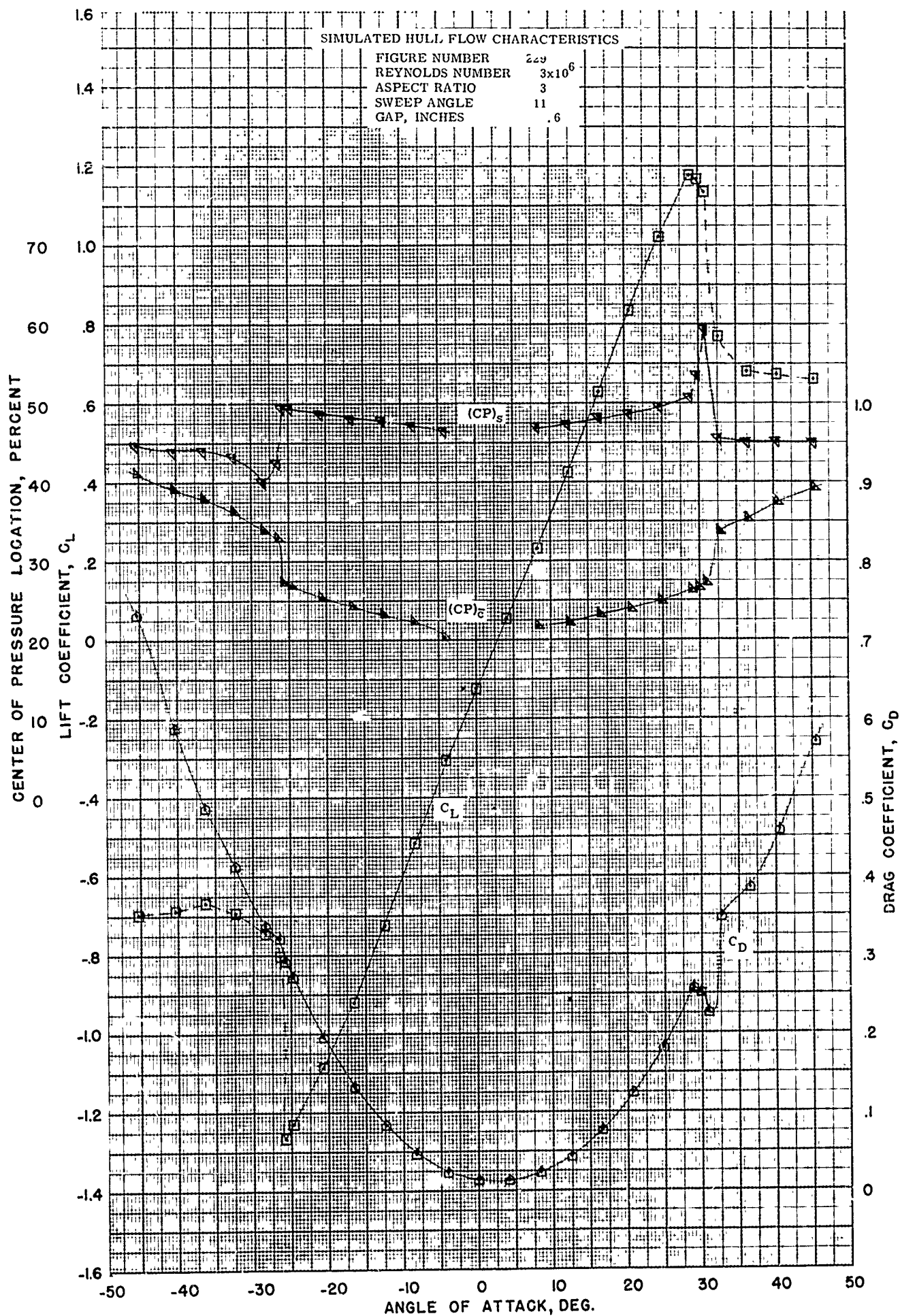


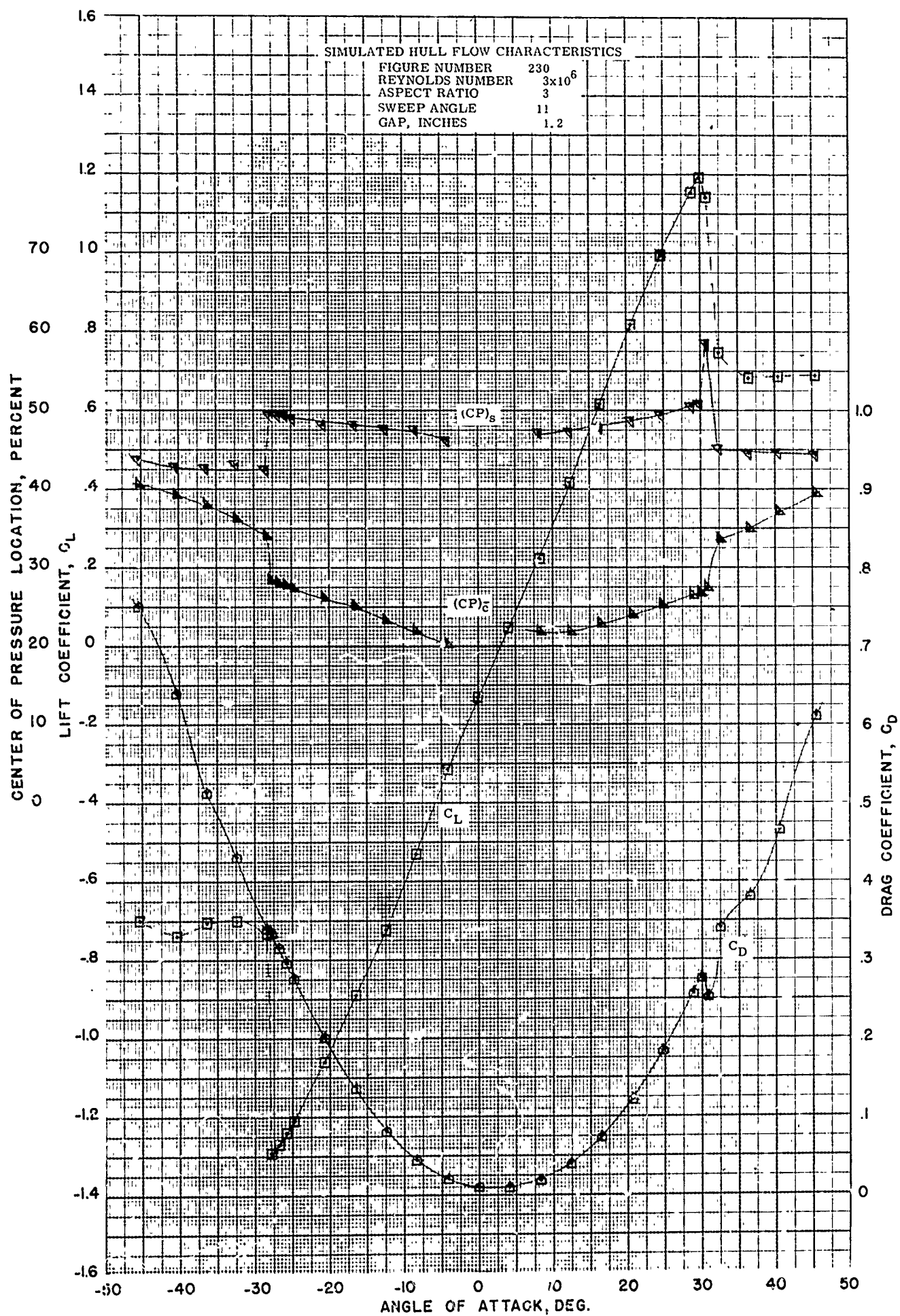


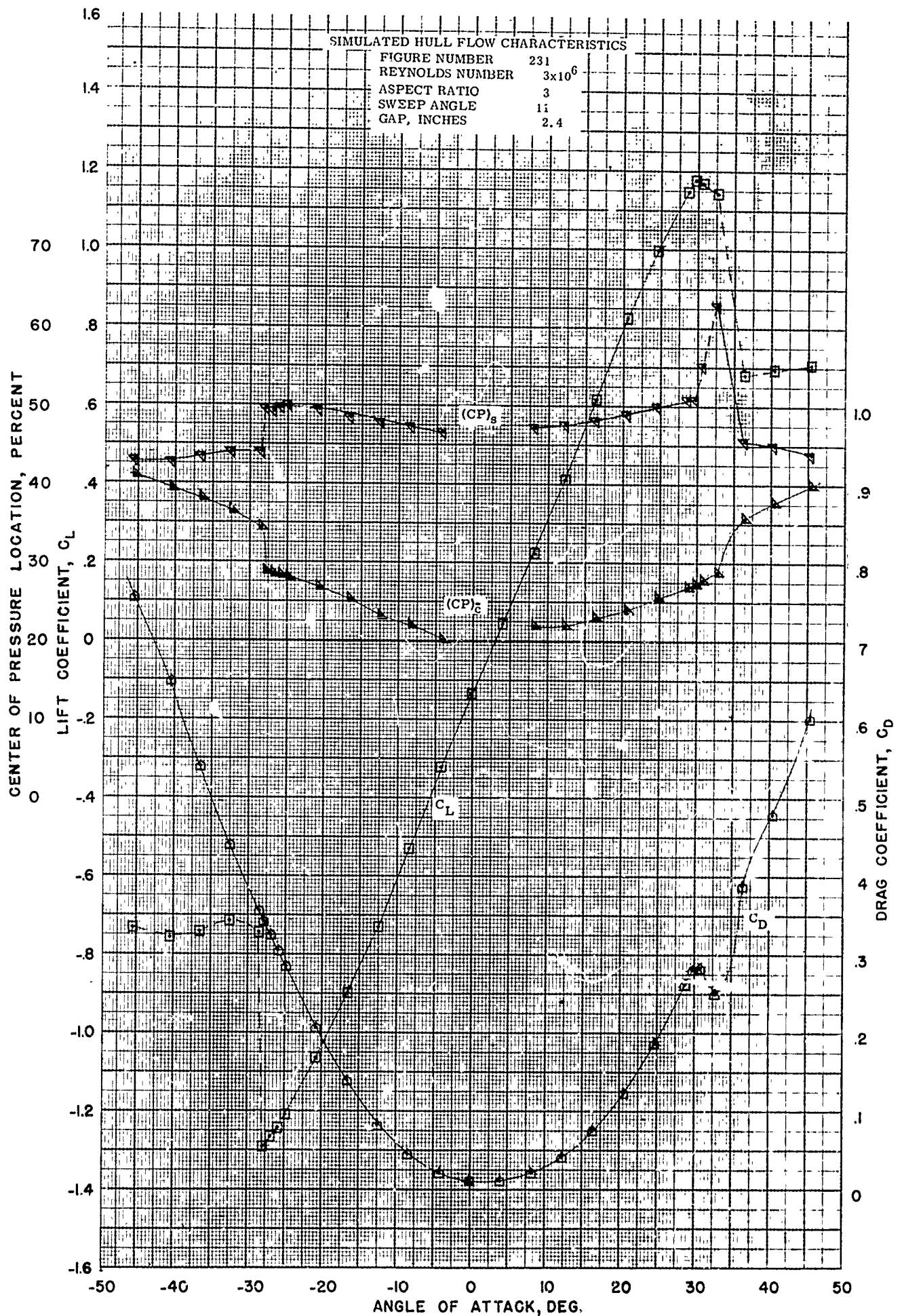


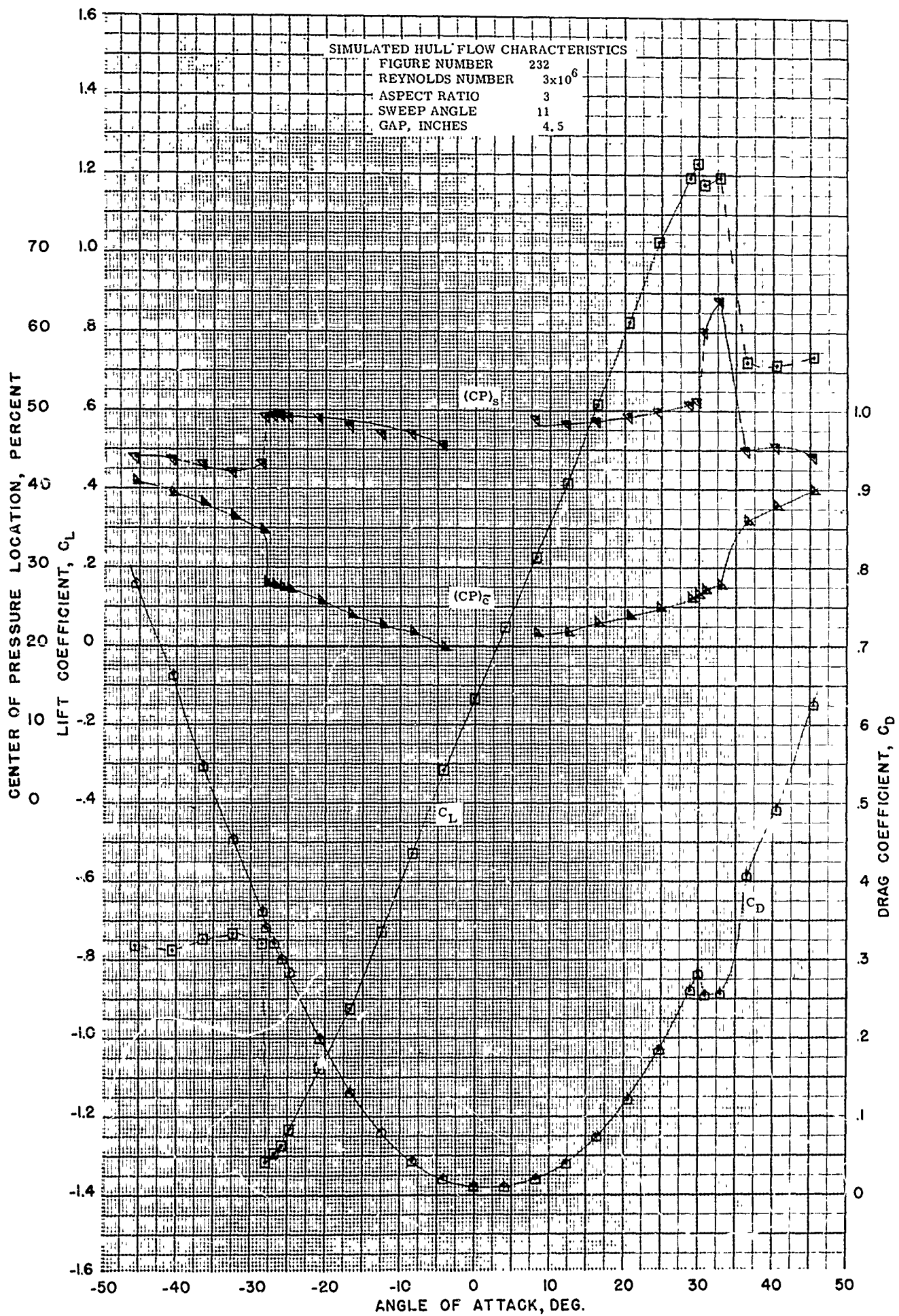


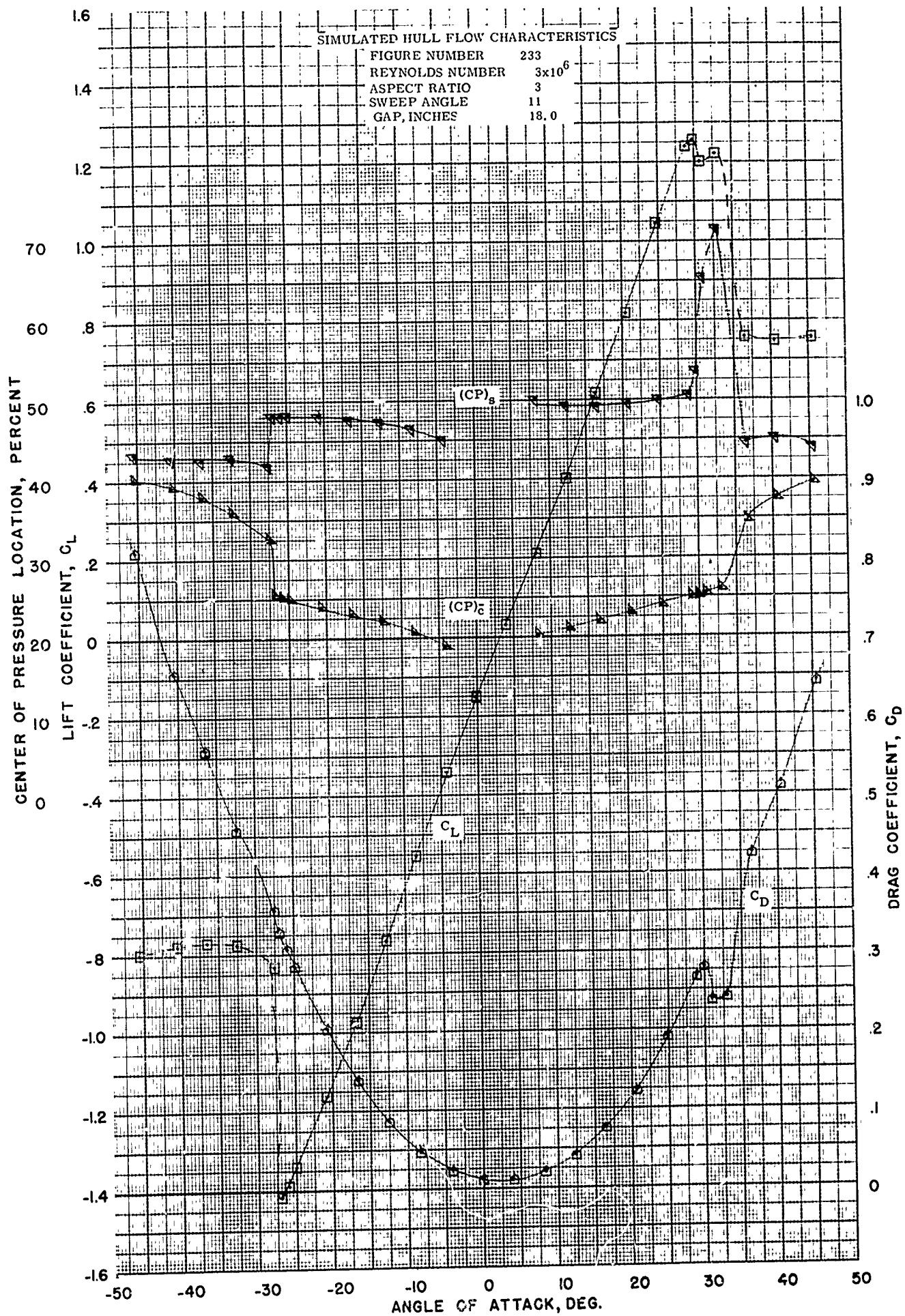


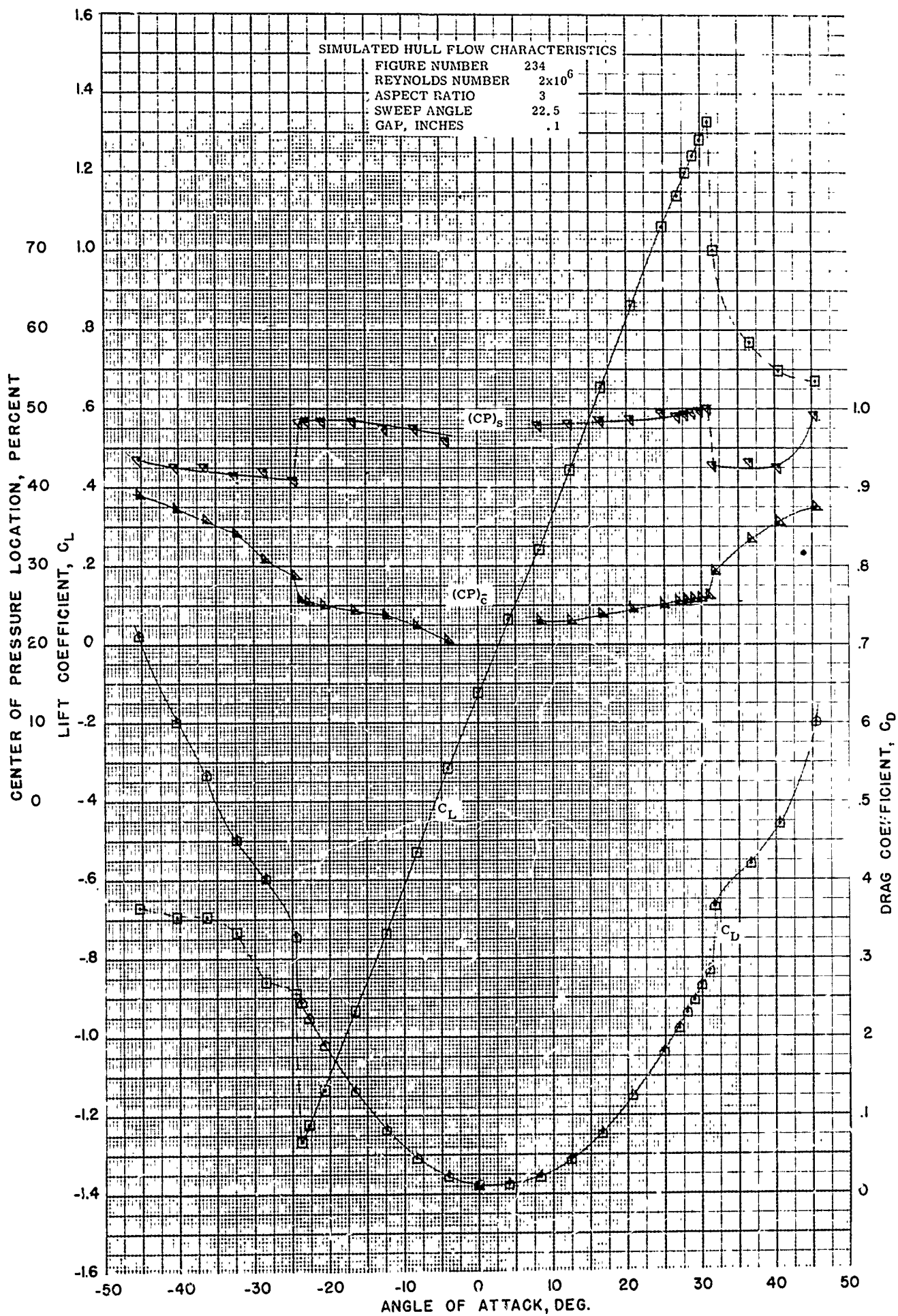


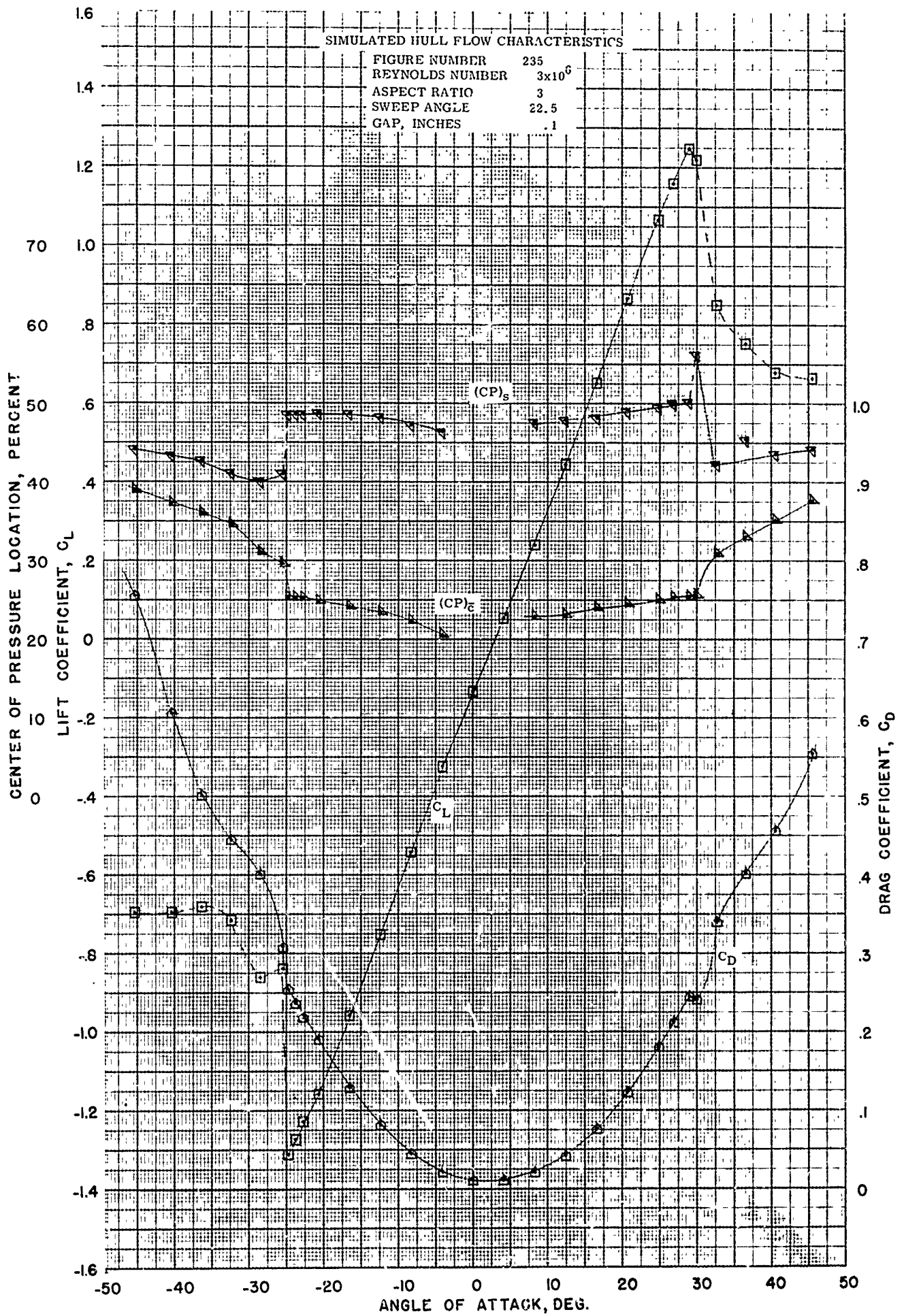


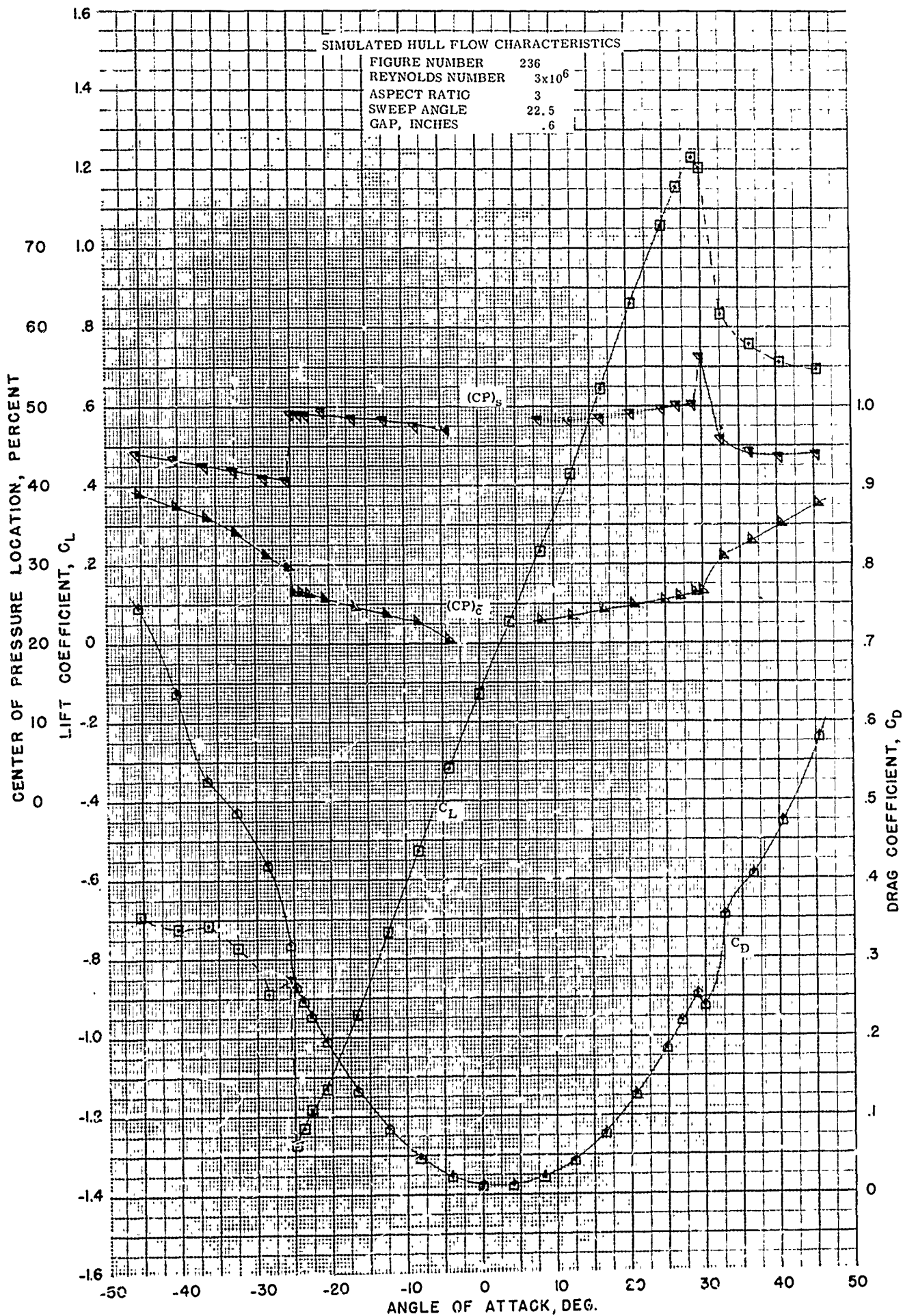


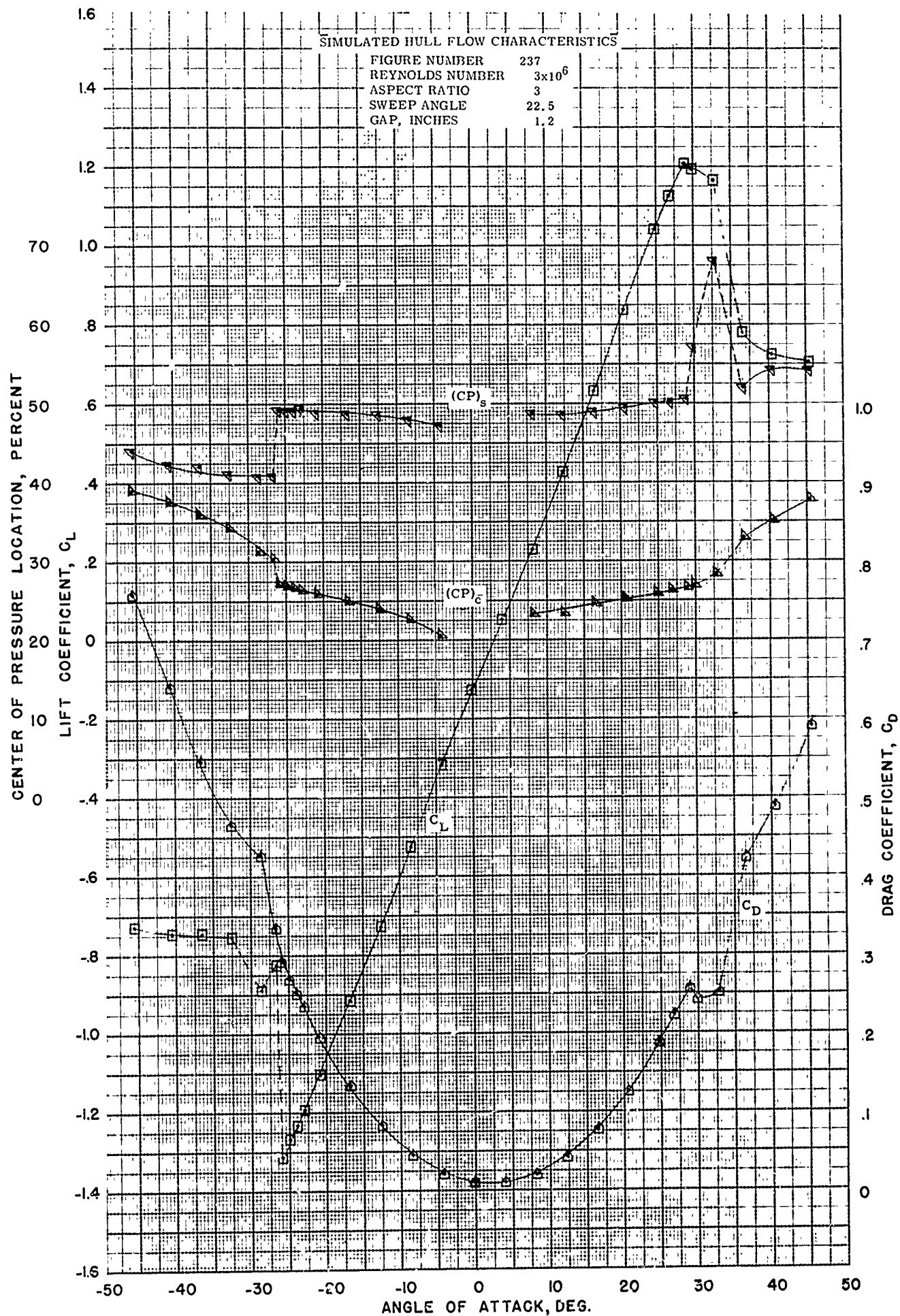


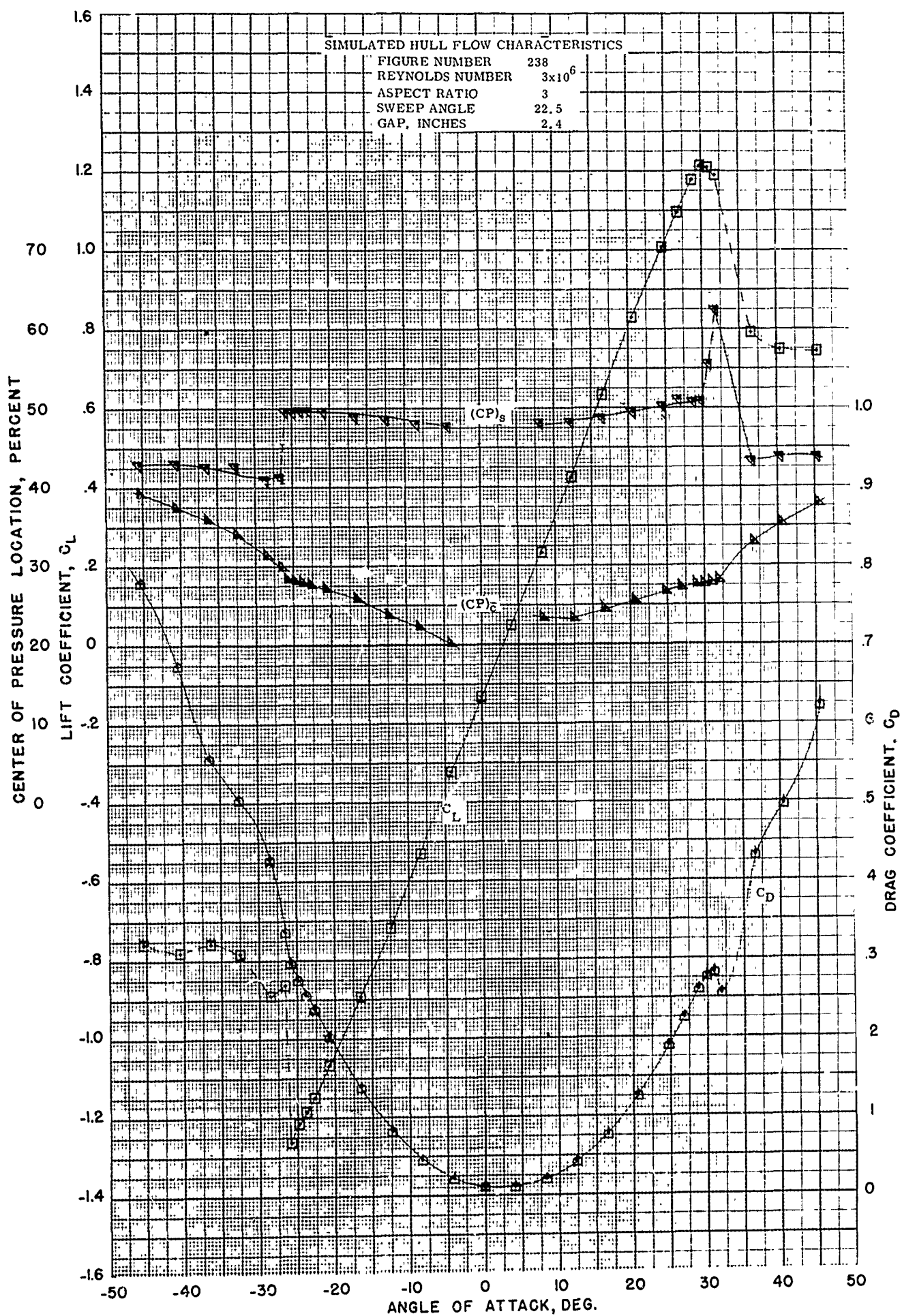


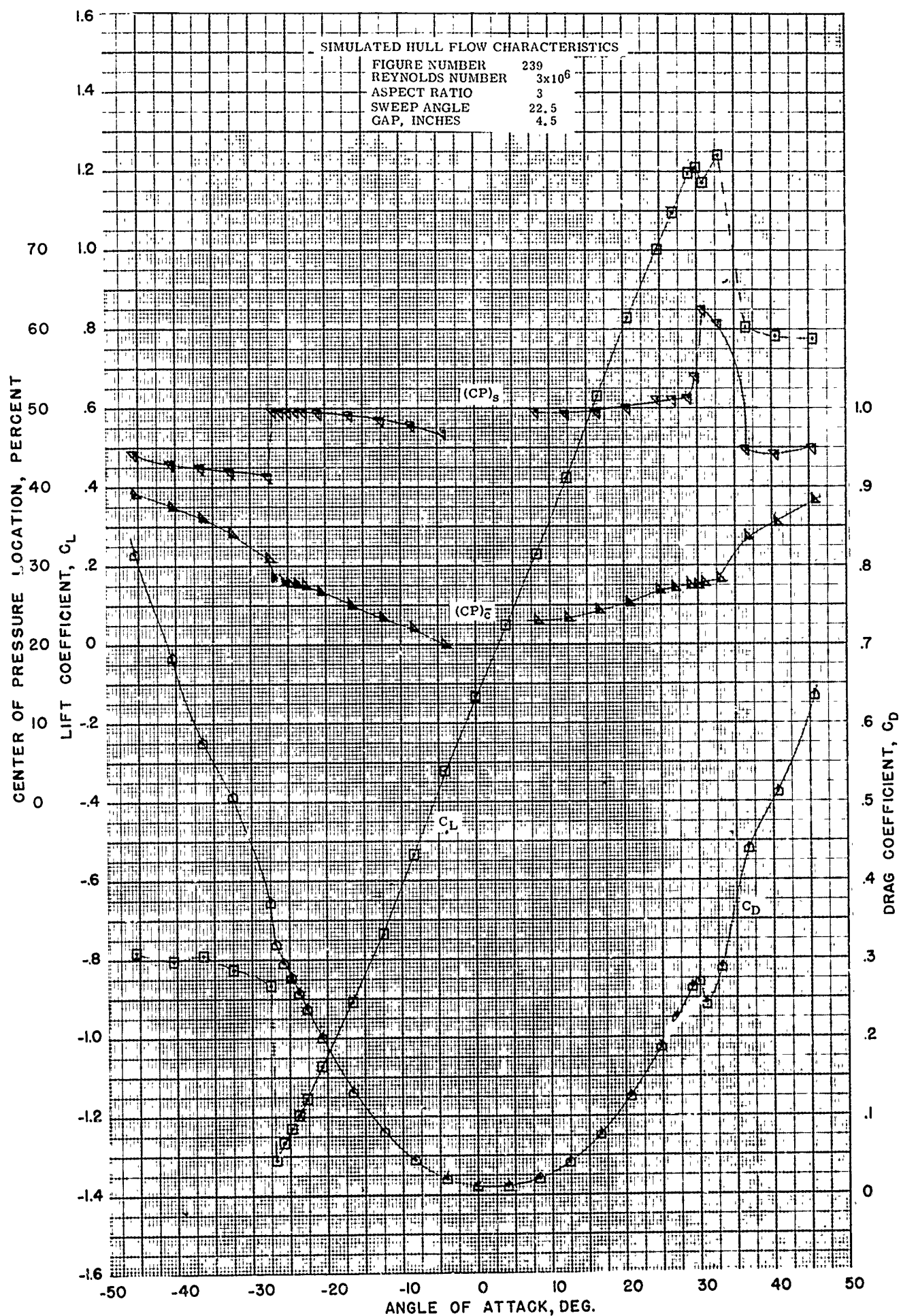


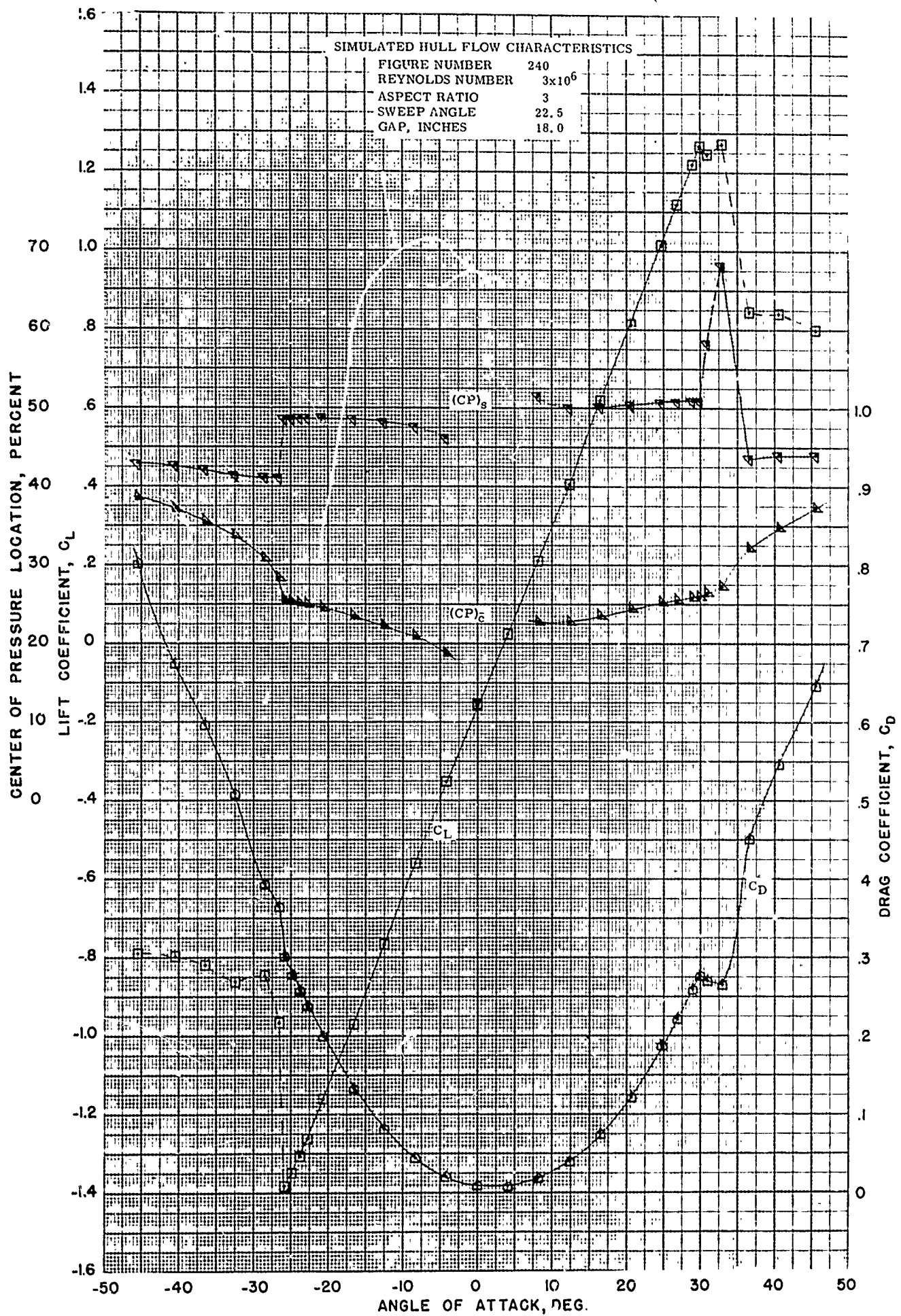






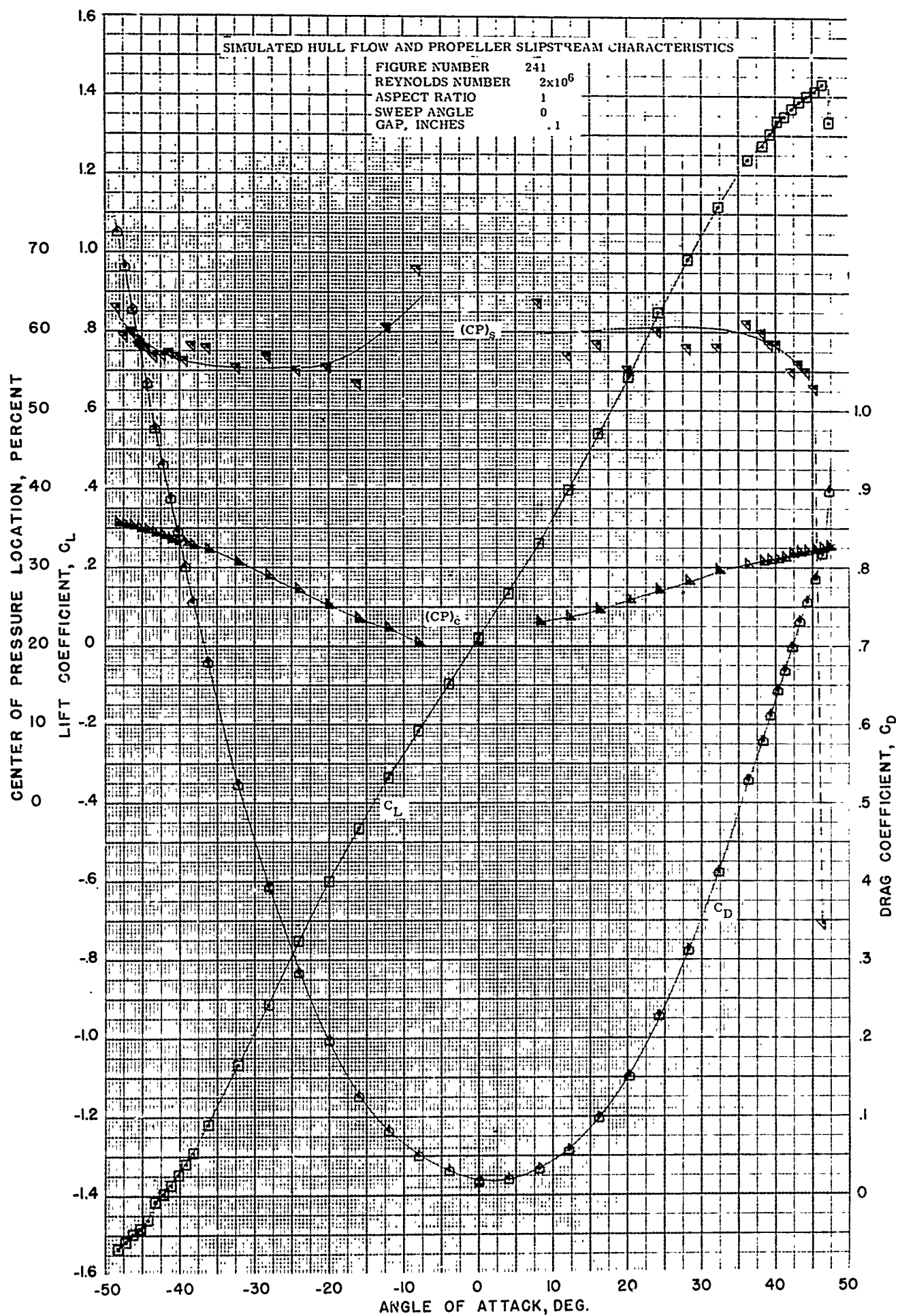


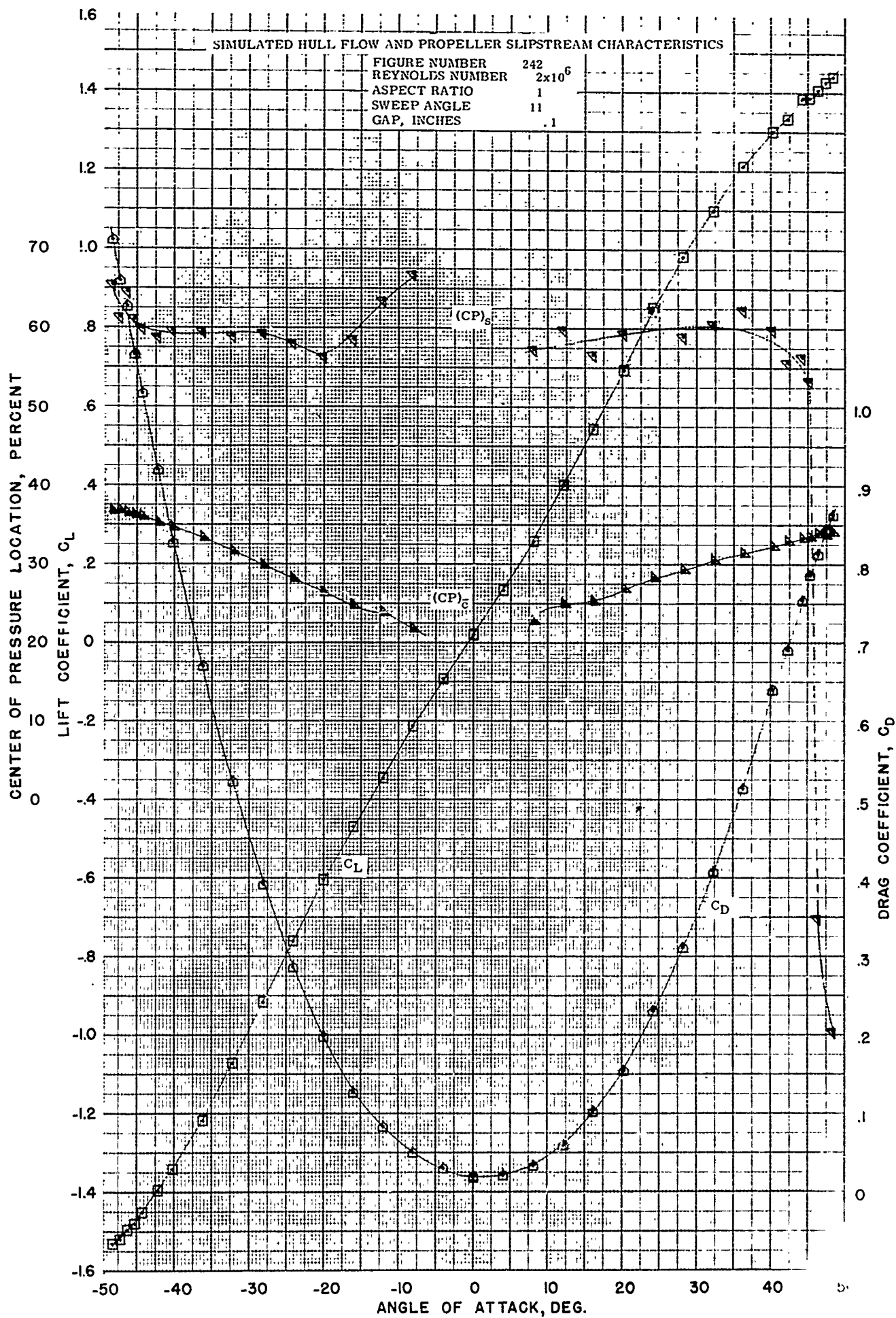


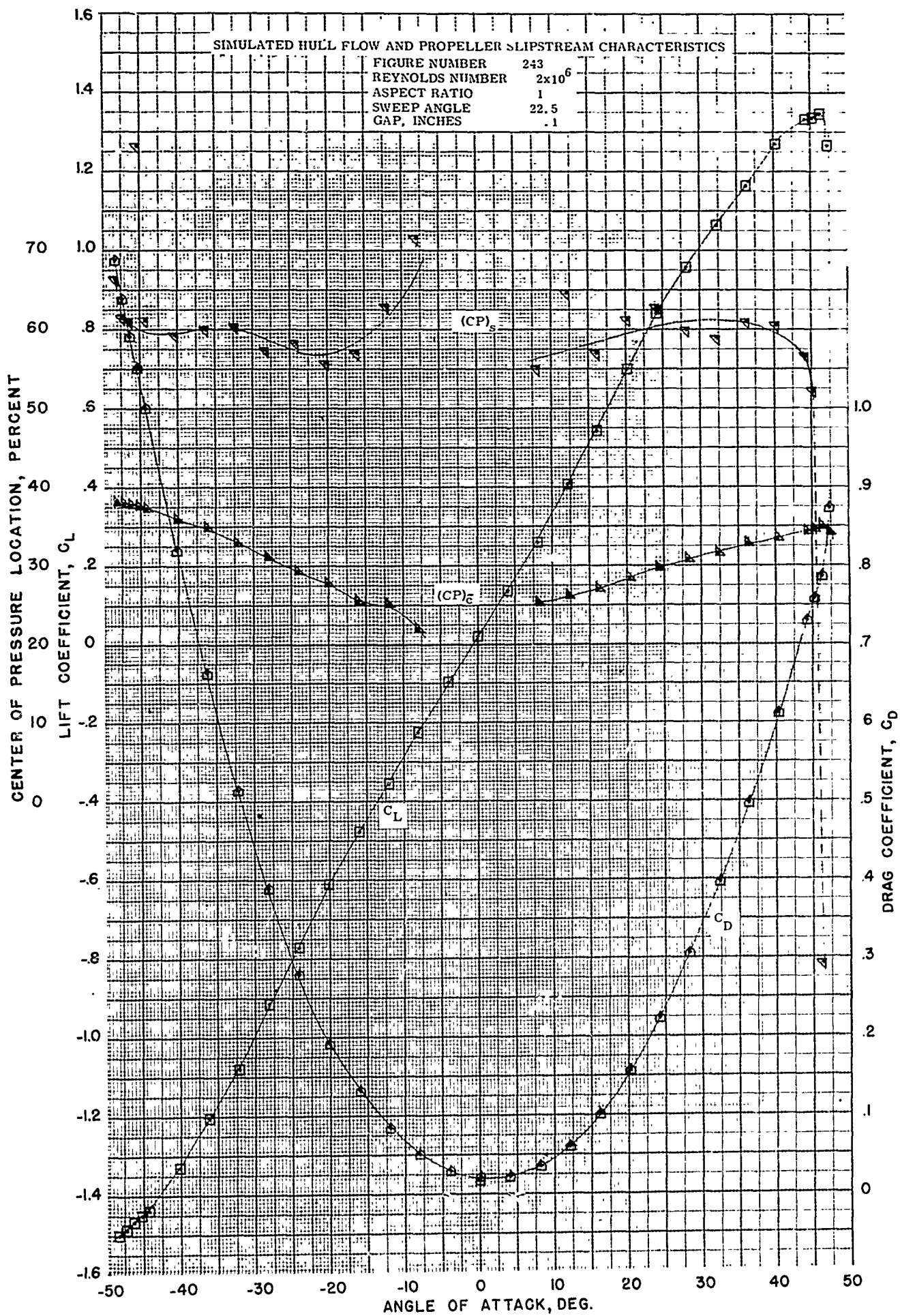


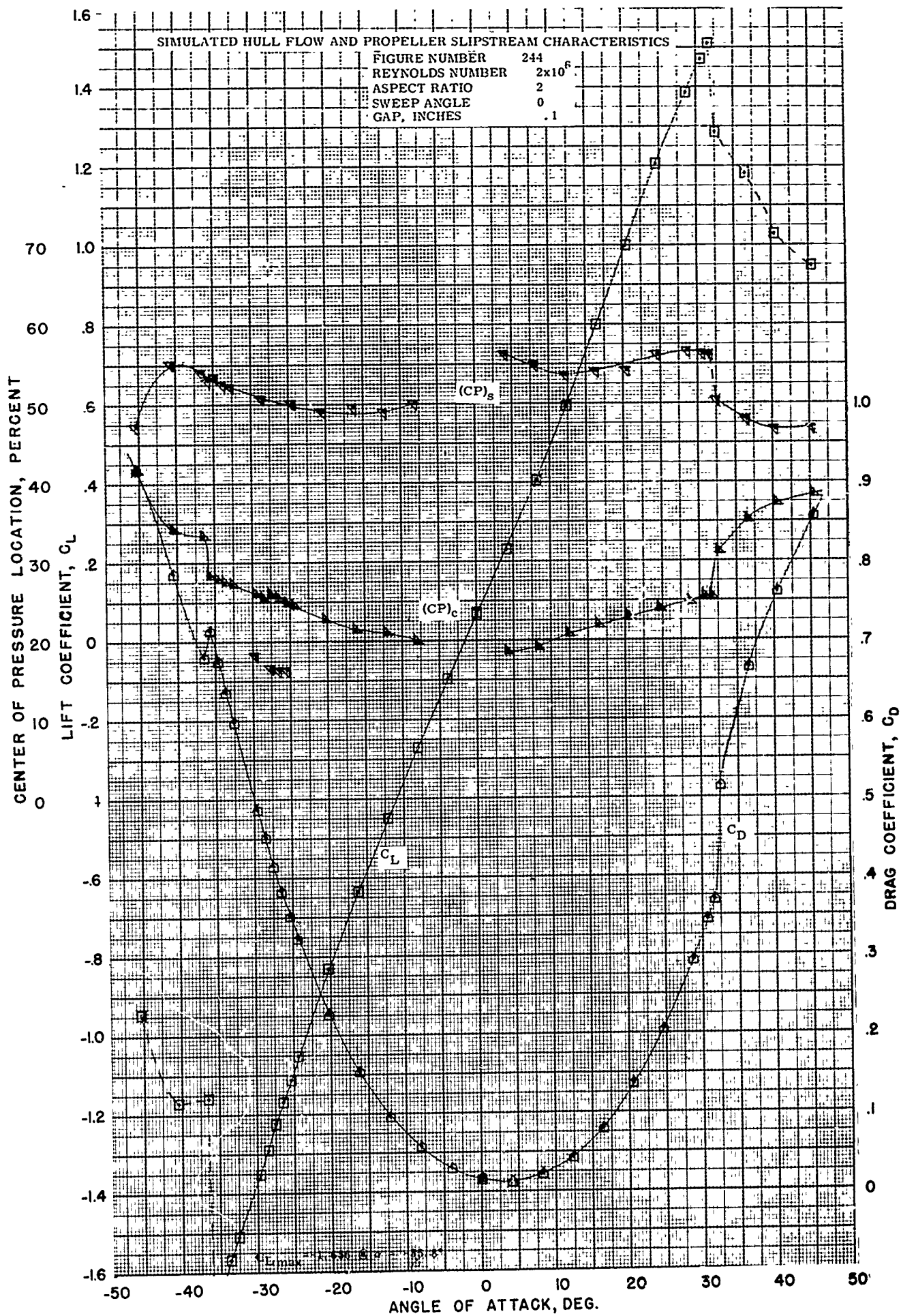
APPENDIX C

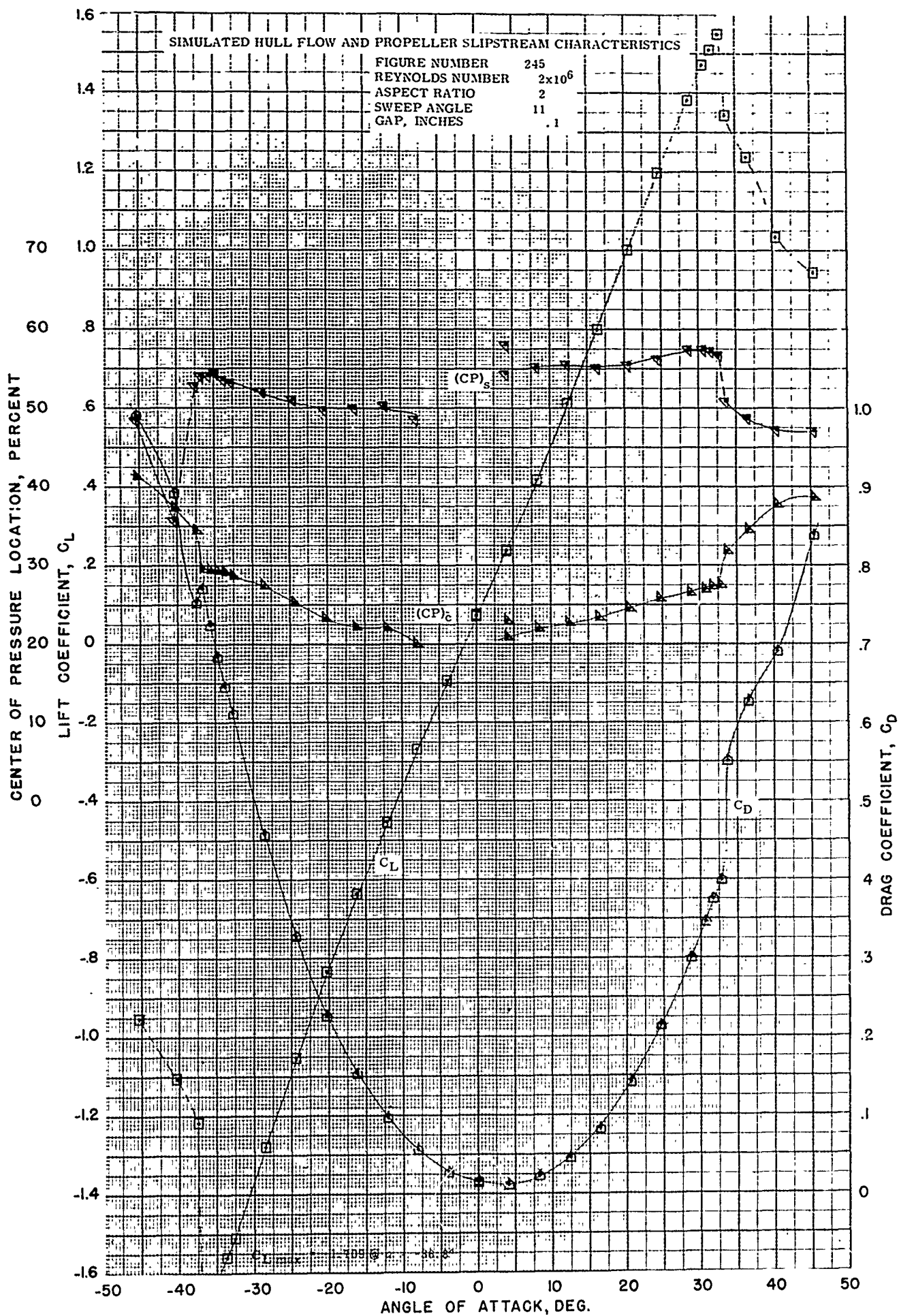
Combined Simulated Hull Flow And
Propeller Slipstream Characteristics, Minimum Gap

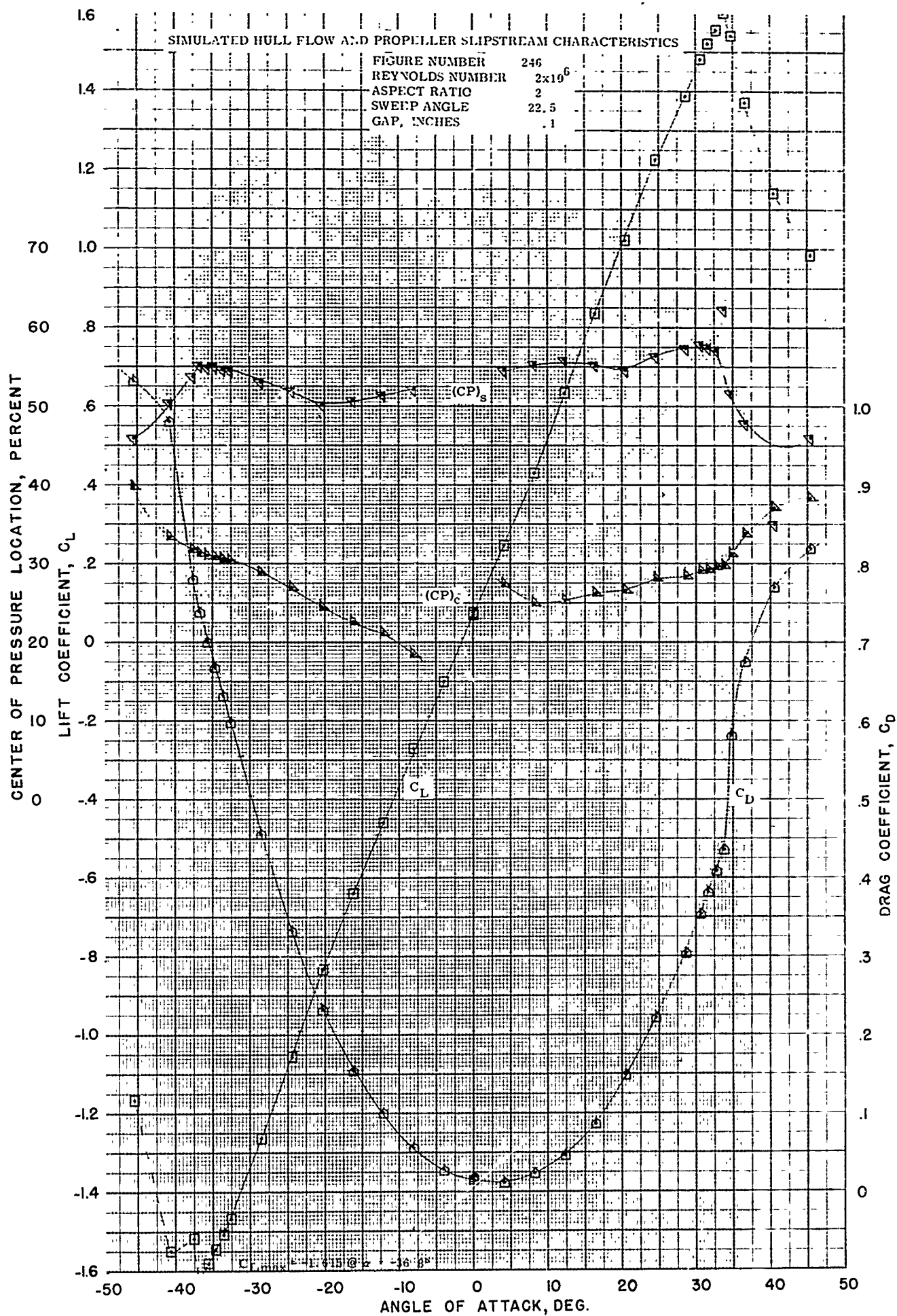


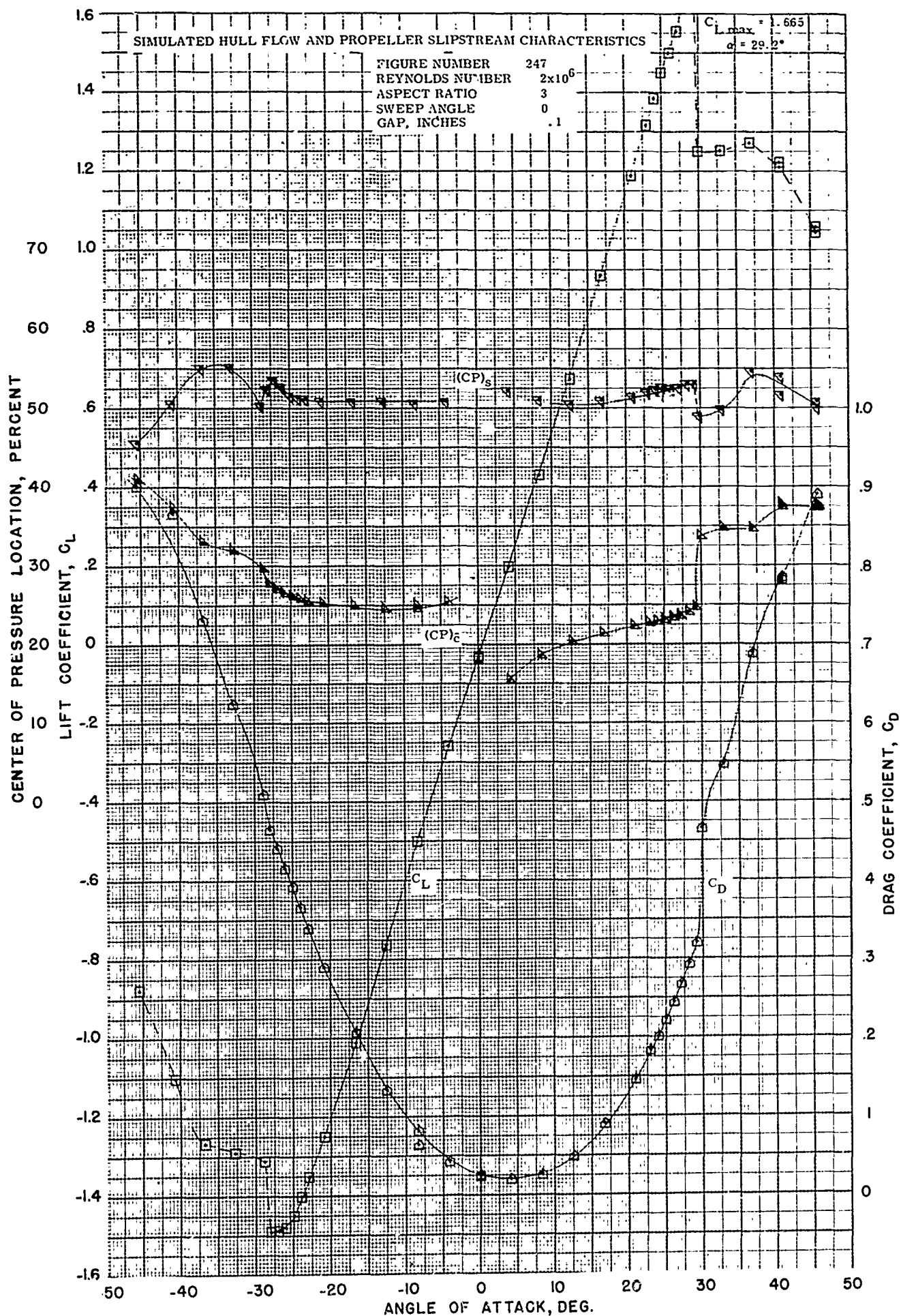


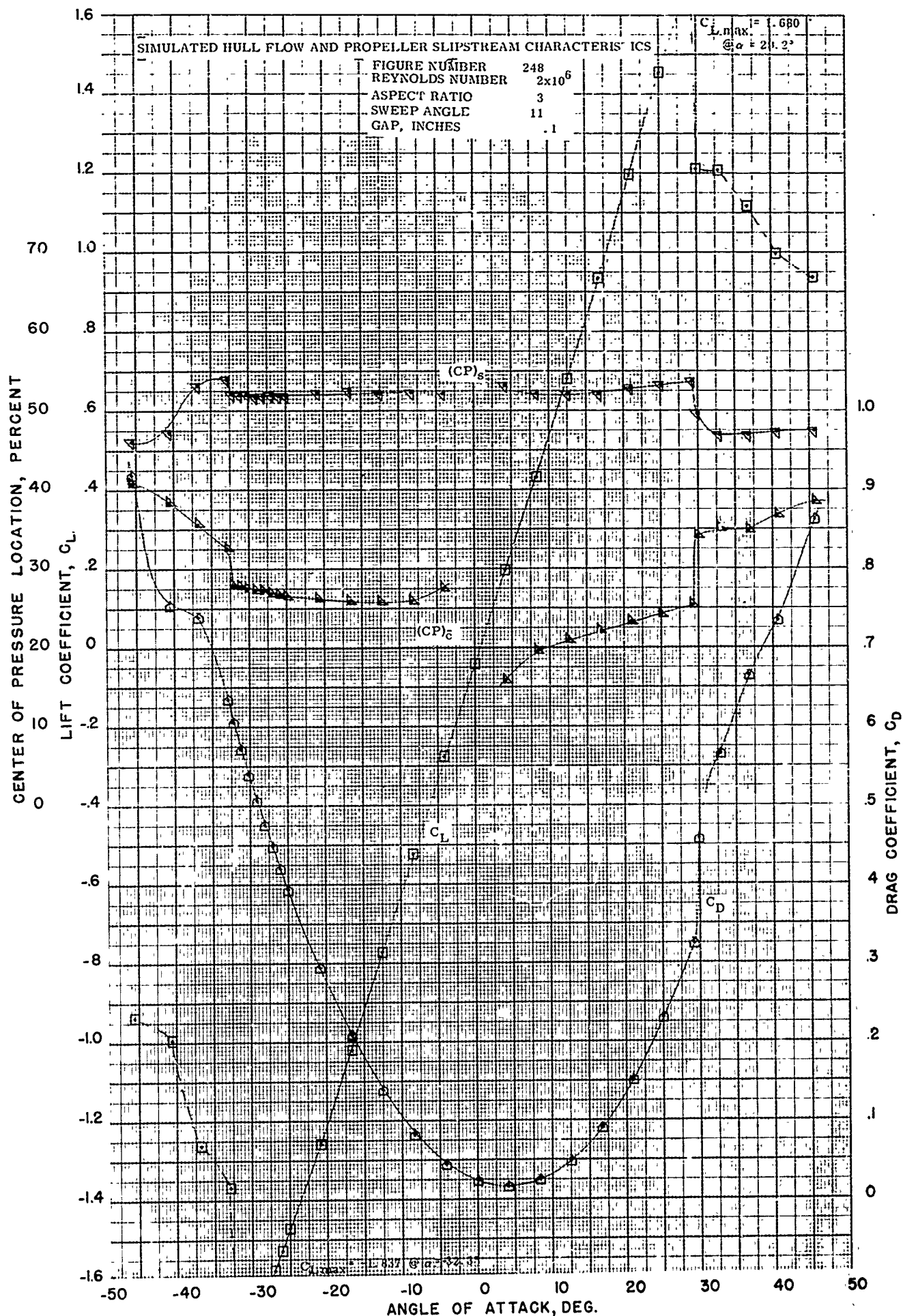


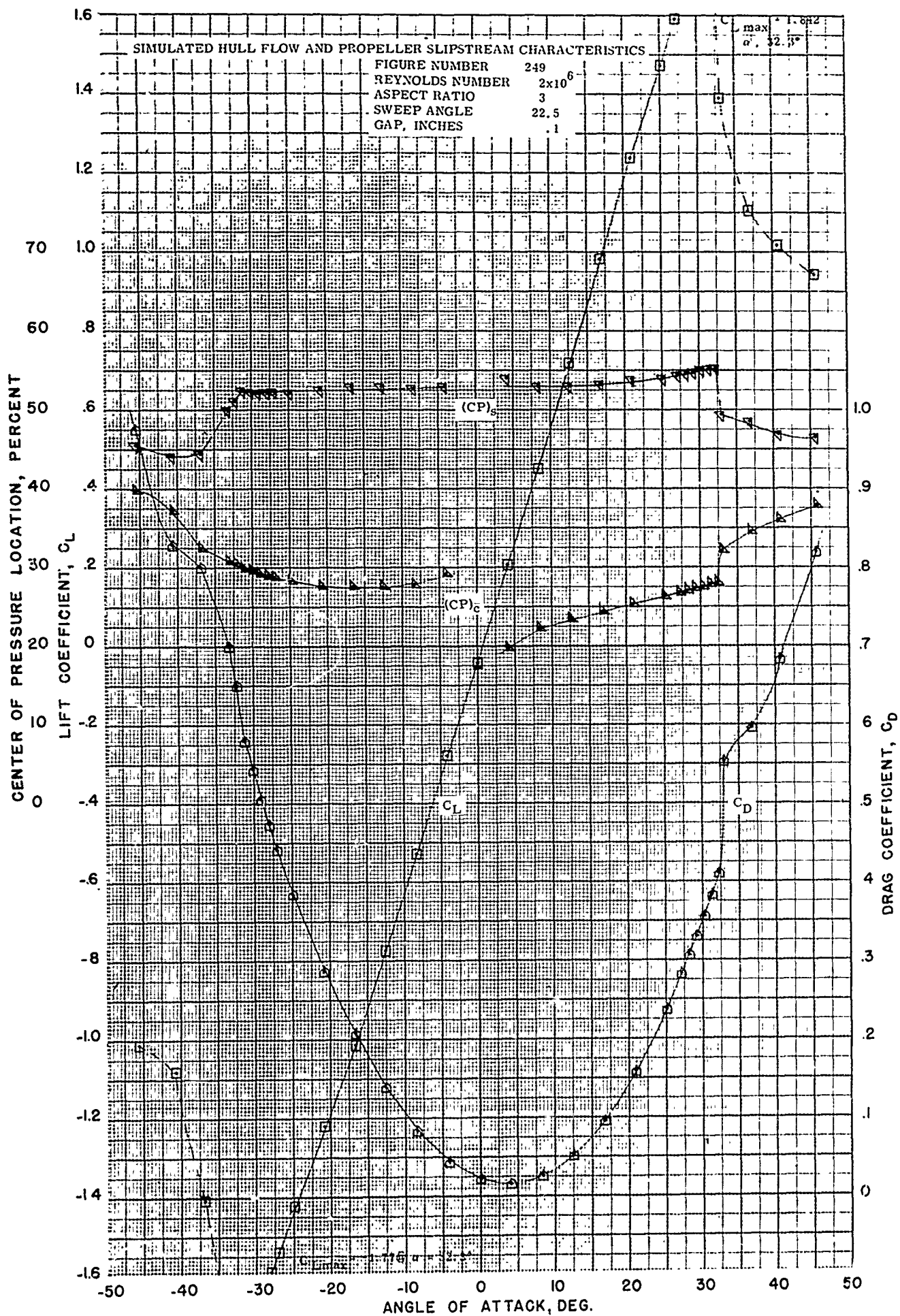












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EFFECTS OF STREAMWISE GAPS, HULL FLOW AND PROPELLER SLIPSTREAM UPON THE AERODYNAMIC CHARACTERISTICS OF A FAMILY OF LOW-ASPECT RATIO, ALL-MOVEABLE CONTROL SURFACES		
4. DESCRIPTIVE NOTES (Type of report and inclusive dates)		
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13. ABSTRACT		
<p>Effects of faired, streamwise gaps upon the free stream characteristics of a family of low-aspect-ratio, all - moveable control surfaces are presented. The family of control surfaces consisted of three aspect ratios (1, 2, and 3) and three sweep angles (0, 11, and 3) and three sweep angles (0, 11 and 22.5 degrees), each having a NACA 0015 airfoil section and a taper ratio of 0.45. Gap effects were also investigated in conjunction with simulated hull effects. Propeller slipstream effects were determined for the minimum gap condition. (1) K</p>		

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14. KEY WORDS	LINK A		LINK B		LINK C	
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